

Title:	Approval of 60% Design for 325 Blake Road Restoration and Redevelopment			
Resolution number:	22-010			
Prepared by:	(952) 641-451	Gabriel Sherman, Planner-Project Manager (952) 641-4510 gsherman@minnehahacreek.org		
Reviewed by:	Michael Haym	an, Project Planning Manager		
Recommended action:	probable cost;	al of the 60% design submittal, including plans; specifications; opinion of Operations, Maintenance, and Monitoring Plan; and design , with Board feedback to be incorporated at the 90% design phase		
Schedule:	March 2022 – Second Quarte	Authorization to execute a purchase and sales agreement with Alatus Authorization to submit Point Source Implement Grant application er 2022 – Approval of 90% design - Final design and project bidding		
Budget considerations:	N/A			
Past Board action:	Res # 20-066	Authorization to Execute a Cooperative Agreement with the City of Hopkins for Coordinated Planning, Improvements and Development for 325 Blake Road		
	Res # 20-067	Authorization to Release the Request for Proposals for Design Services for 325 Blake Road Stormwater Management and Site Restoration		
	Res # 20-083	Authorization to Contract for Site Survey for 325 Blake Road Regional Stormwater and Greenway Project		
	Res # 20-091	Authorization to Contract for Design Services for the 325 Blake Road Regional Stormwater and Greenway Project		
	Res # 21-063	Acceptance of 30% Design for 325 Blake Road Restoration and Redevelopment		
	Res # 21-075	Approval of Phase II Design Contract for 325 Blake Road Restoration and Redevelopment		
		ons listed above are specific to the design process and selection of design history of Board decisions related to the project is available.		

Summary:

<u>Background</u>

In December 2020, Minnehaha Creek Watershed District (MCWD) contracted with HDR to provide design and engineering services to advance its stormwater and greenway project at 325 Blake Road and adjacent Cottageville Park properties in Hopkins. The design process has been phased, with the Phase I contract covering project initiation through schematic design and the Phase II contract scoped to bring the project from schematics through final design. Phase I work was completed in September 2021 with Board acceptance of schematic designs, and the Phase II scope of work and contract were authorized in November 2021. At the February 24, 2022 Board meeting, staff will present the draft 60% design submittal for the Board's consideration.

Design Process

Phase I design included significant foundational technical work as well as broad stakeholder engagement, both of which built off prior work undertaken to characterize the site's water resource and societal potential. Listening sessions, surveys, and open houses in early 2021 helped re-establish and refine the specific goals the community, MCWD, and the City of Hopkins (City) held for the site. In July 2021, a design charrette was held in conjunction with MCWD's and the City's selected developer, Alatus, LLC. Findings from the stakeholder engagement process and preliminary stormwater engineering studies were used to sketch MCWD's stormwater and greenway project and demonstrate how Alatus' transit-oriented development could be merged with that design. Representatives from regional agencies with an interest in the project were invited to provide real time input on the emerging designs.

The first Phase II deliverable is 60% design, which incorporates feedback received on the schematic design from the Board and staff, as well as preferences gathered through several community engagement events. MCWD participated in a neighborhood meeting hosted by Alatus in November 2021 to collect ideas on the schematic design and hosted a 60% design virtual community meeting in January 2022. Both events included preference surveys, which were also made available online in English and Somali after the meetings. Two informational sessions and preference surveys were also conducted with students at Hopkins West Junior High to bring youth perspective to the site, a demographic that was under-represented during other community events. The designs have continued to respect the direction set at the July 2021 charrette to allow for seamless integration with the Alatus development, while independently achieving the project goals established by the Board and community.

The Board has maintained active involvement in project design through the selection of the design consultant, participation in the listening sessions and charrette, and providing feedback at Committee and Board design briefings. In between these milestones, Board liaisons appointed to the design process have provided an additional level of review and strategic guidance to project staff through regular design meetings and workshops. A separate Board liaison group has guided the developer selection process.

60% Design

Baseline and Alatus Alternatives

Two alternatives were produced as part of the schematic design: 1) a Baseline Alternative which built out MCWD's stormwater and greenway project and reserved a portion of the site for a future transit-oriented development (TOD), and 2) an Alatus Alternative which merged MCWD's stormwater and greenway project with Alatus' proposed TOD. Throughout late 2021, Alatus rapidly advanced the design of its development to secure land use entitlements by the end of 2021, which allowed MCWD's 60% design to proceed along the Alatus Alternative while maintaining the ability to easily shift to the baseline alternative if necessary.

Project Components

The major components of the project are broken out below to demonstrate that portions of the project could be prioritized or constructed in phases if necessary. Designs for the stormwater pond and associated infrastructure have currently been fast-tracked to meet critical grant deadlines, while the Nature Play Area and Gateway Plaza are proceeding at a more measured pace to allow for future collaboration with Alatus and Hopkins.

Stormwater

At the heart of MCWD's capital project is the regionalization and treatment of 270 acres of stormwater that currently empties untreated into Minnehaha Creek. This stormwater will be brought to the 325 Blake Road site through two diversion pipes (already constructed) and treated in a stormwater pond in the eastern portion of the site. The pond is designed to be functional yet aesthetically pleasing for users of the Minnehaha Creek Greenway trail extension and future residents of the private development. The pond is currently designed to tie into the Alatus development through a pump and cascade system, which offsets the volume of the pond reduced by the development footprint and provides added water quality benefits.

Greenway and Trails

Another core element of the project is the extension of the Minnehaha Creek Greenway, providing a connection through the site between the Cedar Lake LRT Regional Trail and Cottageville Park. The design includes a ten-foot bituminous trail running from the Cedar Lake LRT Regional Trail, along Minnehaha Creek and the stormwater pond, across Minnehaha Creek via a pedestrian bridge, and finally to Lake Street to connect to Cottageville Park. The Greenway will be bookended with the Trailhead at the Cedar Lake LRT Regional Trail intersection and the Gateway at the Lake Street and Blake Road intersection to welcome and orient users.

Greenway Activity Nodes

In addition to the Gateway and Trailhead, the design includes two distinct activity nodes along the Greenway trail to provide users with connections to the creek and places to gather, while protecting the integrity of the riparian corridor. The Landing is located adjacent to Minnehaha Creek on the 325 Blake Road parcel and will accommodate non-motorized watercraft users, as well as provide picnic areas and more contemplative spaces. The Nature Play Area will be located on the Cottageville parcel immediately downstream of the Lake Street bridge and will be connected to the main 325 Blake Road parcel by a pedestrian bridge across Minnehaha Creek.

60% Submittal

In addition to the drawing set, the 60% design submittal includes draft:

- Specifications: Draft construction specifications based on 60% drawings
- Opinion of Probable Cost: Refined cost estimates based on 60% drawings
- Operations, Maintenance, and Monitoring (OMM) Plan: A draft OMM plan detailing annual and long-term operations and maintenance, including an inspection plan, lifecycle expectations, and maintenance costs
- Design Memorandum: Documents technical data, studies, and community engagement supporting the design.

Each of the above documents will be updated with additional detail as design progresses through 90% and final design.

Next Steps

At the February 24, 2022 Board meeting, staff will present the 325 Blake Road Restoration and Redevelopment draft 60% design and seek Board feedback and acceptance of the proposed plans and supporting documentation. Board feedback will be combined with staff's review and used to refine the 60% design and produce the 90% design submittal.

In March, staff intends to submit plans and specifications for the regional stormwater system to the Minnesota Pollution Control Agency to be certified by June 30, 2022 for the Minnesota Public Facilities Point Source Implementation Grant Program. A purchase and sales agreement with Alatus is nearing completion and is also currently scheduled for Board consideration in March. The purchase and sales agreement will provide the framework for determining if MCWD's project (or a portion of it) could be jointly bid with the larger development to achieve cost efficiencies. In preparation for either jointly or independently bidding MCWD's project, final designs for the main 325 Blake Road parcel are schedule to be completed in Summer 2022. Interpretive and artistic elements may advance on an extended timeline to allow for maximum coordination with project partners. The following is a general timeline of the next steps:

- Authorization to submit PSIG application March 2022
- Authorization to execute purchase and sales agreement with Alatus March 2022
- Approval of 90% design Second Quarter 2022
- Final design and project bidding Summer 2022

Supporting documents:

The draft 60% design package is comprised of the following documents:

- Design Memorandum (attached)
- Opinion of Probable Cost (attached)
- 60% drawing set (attached)
- Operations, Maintenance, and Monitoring (OMM) Plan (attached)



RESOLUTION

Resolution number: 22-010

Title: Approval of 60% Design for 325 Blake Road Restoration and Redevelopment

- WHEREAS the Minnehaha Creek Watershed District (MCWD) acquired 325 Blake Road, Hopkins, MN in 2011 as a key piece of the Minnehaha Creek Greenway in St. Louis Park and Hopkins;
- WHEREAS the MCWD is implementing a regional stormwater project at 325 Blake Road to treat polluted stormwater that flows into the creek from approximately 270 acres of surrounding area and to restore more than 1,000 feet of creek frontage and is planning for this work with three accompanying Cottageville Park parcels bordering the creek, collectively the 325 Blake Road Regional Stormwater and Greenway and Cottageville Park Phase II Riparian Restoration Project. The project is commonly referenced by its shortened title "325 Blake Road Restoration and Redevelopment";
- WHEREAS as of March 2020, the construction of both the Powell Road and Lake Street stormwater diversion systems are complete, with the diversion structures remaining bulk-headed until the treatment facility at 325 Blake Road is constructed;
- WHEREAS on August 27, 2020, the MCWD Board of Managers authorized the execution of a Cooperative Agreement with the City of Hopkins for Coordinated Planning, Improvements and Development for 325 Blake Road (Res # 20-066);
- WHEREAS on August 27, 2020, the MCWD Board of Managers approved the release of a Request for Proposals for Design Services for 325 Blake Road Stormwater Management and Site Restoration (Res # 20-067), which sought landscape architecture and engineering services to complete integrated stormwater management, ecological restoration, and public open space improvements at 325 Blake Road and accompanying parcels;
- WHEREAS on December 3, 2020, the MCWD Board of Managers authorized final negotiation and execution of a contract for design and engineering services for the 325 Blake Road Restoration and Redevelopment project with HDR, Inc. (Res # 20-091);
- WHEREAS due to project complexity and uncertainty, the MCWD Board of Managers determined it was prudent to contract for a scope of services that included an additional task not solicited in the RFP to further define the public realm and potential redevelopment footprints and re-scope the later stages of the project after a schematic design (30% design) was produced;
- WHEREAS the MCWD conducted an extensive stakeholder engagement campaign to establish specific project and design goals, including a series of listening sessions with the community, MCWD Board of Managers, and Hopkins City Council (January March 2021), community open houses (June July 2021), preference surveys in English, Spanish, and Somali, and a design charrette with regional agency and development partners (July 13-14, 2021);
- WHEREASthe MCWD Board of Managers accepted the 30% design memorandum and schematic design for 325Blake Road Restoration and Redevelopment on September 23, 2021 (Res # 21-063) upon finding thatHDR had satisfactorily completed the tasks and produced the deliverables included in the contract

authorized by the MCWD Board of Managers on December 3, 2020; and that the schematic design satisfies all major project needs and accurately reflects the project goals defined in the Cooperative Agreement with the City of Hopkins for Coordinated Planning, Improvements and Development for 325 Blake Road;

- WHEREAS MCWD staff presented the schematic design to the Hopkins City Council on October 12, 2021 and the Council expressed support for the design and design direction;
- WHEREAS the MCWD Board of Managers found that it was prudent to advance all project elements from schematic design through final design and produce a construction phasing plan;
- WHEREAS on November 4, 2021, the MCWD Board of Managers authorized execution of a contract for Phase II design and engineering services for the 325 Blake Road Restoration and Redevelopment project with HDR, Inc. (Res # 21-075);
- WHEREAS the MCWD conducted further significant community engagement to inform the 60% design process, including participating in a neighborhood meeting hosted by development partner Alatus (November 15, 2021), hosting a virtual community meeting (January 24, 2022), and conducting informational session with students at Hopkins West Junior High (February 11, 2022). Surveys in English and Somali were available during the events and online for participants to express their preference for various project components;
- WHEREAS the 60% design meets MCWD's project goals and HDR has satisfied the contractual terms associated with 60% design, including the production of plans; specifications; Operations, Maintenance, and Monitory Plan; design memorandum; and opinion of probable cost;

NOW, THEREFORE, BE IT RESOLVED that the Minnehaha Creek Watershed District Board of Managers approves the 60% design submittal for the 325 Blake Road Restoration and Redevelopment project produced by HDR, Inc., with Board comments on the 60% design to be incorporated at the 90% design phase.

Resolution Number 22- 010 was moved by Manager ______, seconded by Manager ______. Motion to adopt the resolution _____ayes, _____abstentions. Date: February 24, 2022.

Date: _____

Secretary

DRAFT

Design Summary Memorandum

325 Blake Road Restoration and Redevelopment

Regional Stormwater Improvements and Greenway Enhancement

Hopkins, MN February 18, 2022

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1. Executive Summary

Located adjacent to Minnehaha Creek, the 325 Blake Road Regional Stormwater and Greenway and Cottageville Park Phase II Riparian Restoration Project is a multi-purpose project being developed to achieve key water quality and recreational goals of Minnehaha Creek Watershed District, along with several other public partners and the greater community. The project features a regional stormwater management facility that treats runoff from several hundred acres of land, the completion of the Minnehaha Creek Greenway, water-centric recreational opportunities, and is co-located with a mixed-use, transit oriented development.

Minnehaha Creek Watershed District has partnered with HDR, Inc., Damon-Farber Landscape Architects, and Inter-Fluve for the detailed design of the public realm development. Design goals include:

- Regionalizing stormwater runoff to improve the water quality of Minnehaha Creek and downstream waterbodies;
- Providing visual and physical access to a previously hidden portion of the creek;
- Increasing recreational opportunities associated with the creek;
- Completing the Minnehaha Creek Greenway by providing improved trail connections for watercraft, pedestrians, and cyclists.

The regional stormwater management facility consists of two stormwater detention ponds separated by a weir wall, located between the Minnehaha Creek Greenway Trail to the east, and a mixed-use private development to the west. The detention ponds are controlled by a multi-stage outlet structure that includes a low-flow orifice and a high-flow weir, with a box culvert located underneath the adjacent trail serving as an auxiliary overflow device. Through coordination with the developer, *Alatus, LLC*, the detention ponds also feature a wet well and pump that discharges stormwater to a cascade on the west side of the mixed-use development. The cascade provides additional stormwater treatment, ultimately discharging back into the detention ponds for recirculation and further water quality enhancement.

Visual and physical access to the creek and recreational opportunities are provided by several aspects of the project design. The Minnehaha Creek Regional Trail is situated between the regional stormwater management ponds and the creek. Key design features include a trailhead and overlook off the Cedar Lake LRT trail, a landing for watercraft using Minnehaha Creek that incorporates picnic areas and hammock poles, a pedestrian bridge to a nature-based play area in the triangular lot north of the creek and adjacent to Lake Street, and a gateway plaza to the Minnehaha Creek Greenway situated at the greenway's hinge point at Blake Road and Lake Street.

2. Project Introduction

Minnehaha Creek Watershed District (MCWD or the District), in partnership with the City of Hopkins (City) and several other public and private partners, is leading an effort to coordinate the planning, design, and redevelopment of the almost 17-acre parcel at 325 Blake Road and three accompanying smaller parcels at 415 Blake Road, 1308 Lake Street, and 1312 Lake Street in Hopkins, Minnesota.

Previously developed as industrial, commercial, or residential properties, these parcels are currently vacant. Adjoining each other, they form a combined site of nearly 18 acres (collectively known as the site). The parcel at 325 Blake Road formerly housed a large cold storage facility with extensive outdoor parking for tractor-trailer trucks. The parcel was purchased by MCWD in 2011 and the cold storage facility and parking lots were demolished in 2018. Situated across the creek from Cottageville Park, the other parcel on Blake Road is wedged between the creek, Blake Road, and Lake Street. It had formerly contained a commercial structure which hindered access and obscured views of the creek as thoroughly as the adjacent cold storage facility. The two parcels on Lake Street are also adjacent to the creek and were occupied by single-family residences before they were purchased and removed by the District. Consequently, access to the creek and public enjoyment of the waterway had been inhibited by their former adjacent land uses. All four parcels have now been cleared with only remnant vegetation remaining, creating the potential for unfettered access to the creek. In addition to these platted parcels, there is also one very small outlot sandwiched between the Lake Street bridge and the former residential properties that is included as part of the site.

Officially known as the 325 Blake Road Regional Stormwater and Greenway and Cottageville Park Phase II Riparian Restoration Project (the project), the District's is creating a transformative, water-centric development on this site adjacent to Minnehaha Creek premised on its vision of Balanced Urban Ecology. This process includes:

- Regionalizing stormwater runoff to improve the water quality of Minnehaha Creek and downstream waterbodies;
- Providing visual and physical access to a previously hidden portion of the creek;
- Increasing recreational opportunities associated with the creek;
- Completing the Minnehaha Creek Greenway by providing improved trail connections for watercraft, pedestrians, and cyclists.

Complementing the District's goals were additional goals of the City, including the desire to develop the site as a relatively high-density transit-oriented residential and commercial development.

This report documents the detailed design phase of the project which builds on the schematic design phase completed in 2021. The detailed design involves advancing the "Alatus alternative" from schematic design. This option includes full build out of the development, recreational/preservation features in the riparian corridor and two detention ponds separated by

a weir wall, which receive regional stormwater runoff from the Powell Road and Lake Street subwatersheds adjacent to the site. The project adopted a goal of treating stormwater from the first flush of pollutants, associated with the 1.25-inch storm event. The stormwater ponds were originally designed with sufficient water quality volume available to meet this objective; however the proposed development schematic encroached on the ponds as originally designed. In partnership with the developer, MCWD negotiated an alternative stormwater treatment process, which pumps and treats stormwater from the ponds to a location within the development where further water quality treatment occurs, compensating for pond encroachments.

In addition to the regional stormwater management, the project incorporates several key design elements adding to the recreational opportunities of the site. The design includes a trailhead and overlook off the Cedar Lake LRT, a landing for watercraft using Minnehaha Creek that incorporates picnic areas and hammock poles, a pedestrian bridge to a nature-based play area in the triangular lot north of the creek and adjacent to Lake Street, and a gateway plaza to the Minnehaha Creek Greenway situated at the greenway's hinge point at Blake Road and Lake Street. Elements of project design, construction, long-term operation, maintenance, and monitoring are detailed within this memorandum or the references cited.

Further information related to project planning and early stages of project coordination, outreach, and conceptual design are contained in the *Schematic Design Memorandum*, dated September 3, 2021. Community engagement and outreach has continued to occur throughout detailed design; the process and findings of which is summarized in separate deliverables submitted to MCWD.

3. Site Information

325 Blake Road is located at the southeast quadrant of the Blake Road North (CSAH 20) and Lake Street Northeast intersection; less than ¼-mile from both State Highway 7 to the north and Excelsior Boulevard (CSAH 3) to the south, and within one mile east of State Highway 169. The property is bounded by approximately 1,100-feet of Minnehaha Creek, 1,100-feet of Blake Road, and 1,200-feet of the Cedar Lake LRT Regional Trail and the future Southwest Light Rail Transit (SWLRT) corridor.

The Project is situated in the lower Minnehaha Creek watershed, approximately 7.3 river miles downstream of Grays Bay dam on Lake Minnetonka where the headwaters of Minnehaha Creek are formed, and approximately 11.5 river miles upstream of Lake Hiawatha. Minnehaha Creek's confluence with the Mississippi River is located roughly 13.9 river miles downstream of the project site. Six key influences define the character of the site and its potential for redevelopment. As detailed below, the key influences are: context, parcelization, land use, land cover, transportation, and utilities.

3.1 Context

The factor most influencing the character and development potential of the site is its context as defined by three regional patterns—patterns of nature, mobility, and development. Three corridors generated by these patterns converge on the site, forming the boundaries of the site's triangular shape (see *Figure 3.1: Regional Patterns.*)



Figure 3.1: Regional Patterns. Three regional patterns exert strong influences on the character of the site and its potential for development.

The dominant pattern that underlies the other two is the natural pattern created by the topography and hydrography of the Minnehaha Creek Watershed. Minnehaha Creek forms the site's northern and eastern edge, creating a strong, not easily crossed barrier. Only the Lake Street and Blake Road bridges offer access between the site and properties to its north and east. The site sits along a segment of Minnehaha Creek that is being ecologically restored to become a recreational attraction, including conservation efforts as part of this project's design. As the mid-point of the greenway, the site could become an ideal gateway to the greenway and the creek's recreational amenities. As Minnehaha Creek drains the surrounding landscape, it makes the site an ideal location for regional stormwater management.

Regionally, the site is situated in the City of Hopkins, a near western suburb of Minneapolis. The southern edge of the site is mostly impenetrable, defined by the existing Cedar Lake LRT Regional Trail and an existing freight rail line that funnel any crossing to properties south of the site to Blake Road. The new double-track Southwest LRT line will parallel the trail and rail lines, reinforcing the barrier. Despite the barrier, the trail and the LRT facilitate regional mobility. Geographically defined by its location as an attractive midpoint between the residential and commercial opportunities located in the expanding western suburbs and the inviting commercial center of the state, downtown Minneapolis, with its bustling business and vibrant residential districts. Consequently, the LRT station proposed at Blake Road will promote access to the site, creating a destination for residential, commercial, and recreational development.

The site's western edge is formed by Blake Road, a busy four-lane collector with access to the site only at 2nd Street, where it is controlled by a signalized intersection and semaphore, and Lake Street which controls access to Blake Road only with a 2-way stop sign on Lake Street. The site's western edge is semi-permeable, providing access to the larger pattern of urban development that will influence the character of the site's own development.

Since the beginning of the project, it was anticipated that the confluence of the three regional patterns on the site would affect the layout and character of the site's design. As the development process continued, and as the initial phase culminated during the Design Charrette, it became increasingly obvious that the influence of regional natural patterns as represented by Minnehaha Creek would create an edge along the creek that would be dominated by natural features. Similarly, the edge influenced by regional patterns of mobility would create an edge responsive to the Cedar Lake LRT Regional Trail and the Blake Road LRT Station. The edge adjacent to Blake Road would be most influenced by existing and proposed urban development resulting in the concentration of buildings along that western edge of the site. (See *Figure 3.2: Site Influences.*)

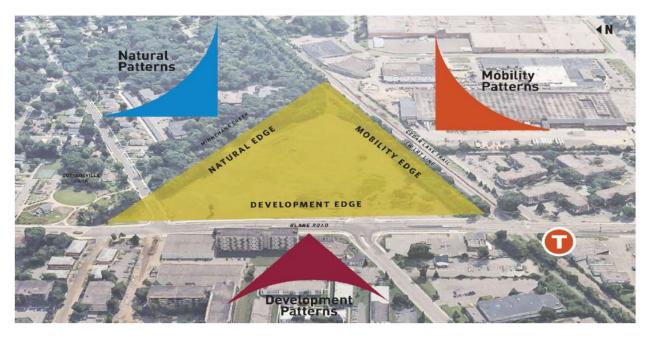


Figure 3.2: Site Influences. The layout and character of each edge of the site will be heavily and distinctly influenced by one of the regional patterns.

3.2 Parcelization

The project site is comprised of 4 parcels and one outlot that total 17.81 acres (see *Figure 3.3: Site Parcels*).

- Parcel A: 325 Blake Road N consists of 16.84 acres, including nearly 1.5 acres of riparian woodland buffer along 1,100 feet of Minnehaha Creek.
- Parcel B: 415 Blake Road N consists of approximately 0.48 acres of an open site wedged between the creek, Blake Road, and Lake Street. The parcel slopes to 150 feet of Minnehaha Creek frontage.
- Parcel C: Outlot. A small 0.16-acre outlot, located across Minnehaha Creek from the primary parcel with a narrow riparian woodland buffer has approximately 100 feet of creek frontage.
- Parcel D: 1308 Lake Street NE consists of 0.14 acres, located across Minnehaha Creek from the primary parcel, a mostly open, former residential, parcel with a narrow riparian woodland buffer along 50 feet of Minnehaha Creek.
- Parcel E: 1312 Lake Street NE consists of 0.19 acres, located across Minnehaha Creek from the primary parcel, a mostly open, former residential property with a narrow riparian woodland buffer along 50 feet of Minnehaha Creek.

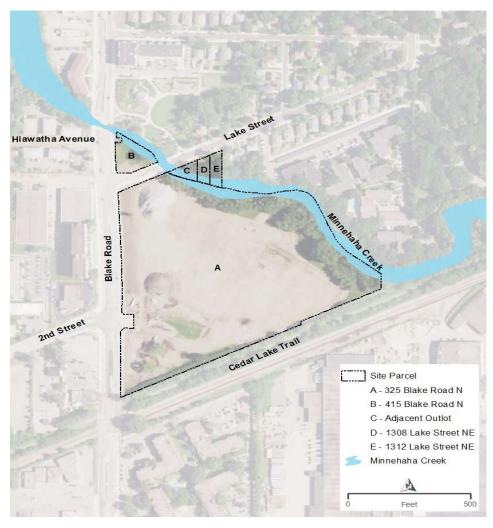


Figure 3.3: Site Parcels. The site is composed of five adjoining, mostly vacant, parcels.

3.3 Land Use

The site is located near the middle of the Minnehaha Creek Greenway; a restored and revitalized ecological and recreational corridor of Minnehaha Creek that meanders through portions of Hopkins and St. Louis Park. Nearby land use includes residential, commercial, industrial, institutional, and transportation infrastructure all of which complement the proposed mixed-use development envisioned by the City. Existing significant landmarks and attractions nearby, including Downtown Hopkins (1.5 miles southwest), Knollwood Mall (0.5 miles north), Cottageville Park (located across the creek from the site), Minnehaha Preserve (0.75 miles east), and Methodist Hospital (1.0 miles east), make the location particularly attractive to commercial and residential development.

3.4 Land Cover

Before the site was cleared for stormwater management and redevelopment, the primary site had been occupied by a cold storage facility. The demolition of that facility in 2018 provided the opportunity to repurpose the parcel in accordance with the vision of MCWD and the City. The cold storage facility consisted of a 6.3-acre building and 5.7 acres of adjacent parking and

driving surfaces, which combined to cover 12 acres of land with impervious surface. The majority of the current site is vacant with aggregate surfacing and sparse vegetation with a wooded riparian buffer covering roughly 1.5 acres along Minnehaha Creek. The district is also storing two large stockpiles of crushed concrete/pavement in the northwest corner of the site. This material will be sold to a local contractor or sourced by the developer's contractor during development. Remaining outlot parcels are also vacant covered with mostly grass and scattered older trees. With the exception of maintaining a vegetative buffer along the creek, the prior impervious landcover will allow redevelopment to proceed with more flexible design and performance criteria to meet regulatory requirements than if the site were previously undeveloped.

3.5 Transportation

Providing transportation access and mobility is key to the successful redevelopment of the site. Two of the site's three sides are flanked by transportation corridors, providing it with excellent access and mobility. To the west is Blake Road. Classified as a Major Collector by the City of Hopkins' 2040 Comprehensive Plan, it has an average annual daily traffic (AADT) of approximately 12,200 vehicles. It operates as a significant north-south corridor for local vehicular traffic and active transportation connecting the site to the metropolitan region and locally to destinations along Blake Road, Excelsior Boulevard to the south, and Minnesota Highway 7 to the north. It supports bus routes and its sidewalks will provide the "last mile" for pedestrians walking between the site and the future Blake Road LRT Station.

The south edge of the site is flanked by a multimodal transportation corridor. The corridor is comprised of three parallel facilities. The closest to the site is Cedar Lake LRT Regional Trail. It is an active transportation facility managed by Three Rivers Park District to promote walking, bicycling, skating, and—as allowed by law—selected forms of electrically powered mobility. It promises to be a significant commuting and recreational connection drawing bicyclists and other active transportation users to and from the site. The trail extends west to downtown Hopkins where it connects to several other trails that serve the western suburbs. Similarly, it extends east into Minneapolis and that city's extensive trail system. Consequently, the Cedar Lake LRT Regional Trail provides a level of service for active transportation users similar to that which Blake Road provides motorists—access to the larger metropolitan region.

Offset south approximately 70 feet and parallel to the trail is an active single track freight railroad. It acts primarily as a barrier, blocking access between the site and locations south of the train tracks and funneling any crossing to Blake Road.

Parallel to the railroad and offset an additional 50 feet south will be the location of the doubletrack Southwest Light Rail Transit (SWLRT) line. Like the tracks for freight trains, the rails for the SWLRT line will hinder access and mobility, relegating crossings to Blake Road. Currently under construction, the SWLRT will include a transit station in the southwest quadrant of the intersection of the LRT tracks and Blake Road. With the addition of a tunnel under Blake Road and traffic signals at 2nd Street, pedestrian access between the site and the Blake Road Station will be excellent, making the site a prime location for Transit Oriented Development (TOD). Minnehaha Creek borders the east side of the 325 Blake Road parcel. Although not a traditional transportation corridor, the creek is considered a water trail for recreational watercraft. As a water trail, it provides people with an alternative to safely crossing the bicycle trail, the freight railroad, and LRT tracks that impede travel to destinations south of the site. Between Louisiana Avenue and Blake Road, this creek crossing is the only opportunity to safely cross the transportation facilities that flank the south side of the site.

3.6 Utilities

According to a survey performed in January 2020, utilities associated with the 325 Blake Road parcel include inactive sanitary sewer and natural gas utility lines located near the north edge of the site, which connect to utility mains under Lake Street. Storm sewers from Lake Street and Powell Road are currently bulkheaded, but designed to discharge onto the site from the north and southeast edges of the site, respectively. Two sampling wells are located within the main parcel. Public utilities, including overhead electric lines, underground electric lines, underground communication lines, and similar utilities are located along Blake Road, Lake Street, and near the Cedar Lake LRT Regional Trail. Overhead utilities adjacent to the site currently detract from the site's visual quality. It is anticipated that all overhead utilities will be buried during the site's redevelopment. The survey does not show any utilities within the proposed stormwater management area except the monitoring wells, which will be removed or abandoned during construction.

4. Existing Information

4.1 Prior Studies and Information

Since the Project's initiation in 2013, several studies, models, and reports have been developed that assess and document key findings related to stormwater management at the Project. *Table 4.1* contains a list of major items referenced throughout the project design.

Data Description	Data Source	Date of Record
Assessment of pollutant loading, biology, and habitat	DRAFT Stormwater Management Feasibility Study for 325 Blake Road North, Hopkins, MN	July 2013
Summary of pollutant loading estimates	325 Blake Road Market Analysis Pollutant Loading Study	Nov. 2013
Groundwater and geotechnical parameters	Baseflow Restoration in Minnehaha Creek Watershed with Stormwater Infiltration report	2013
Hopkins Lift Station L27 storm sewer design update memo	Hopkins Lift Station L27 Storm Sewer Design Update Memo	Aug. 2015
Powell Road storm sewer diversion record drawings	Powell Road Storm Sewer Diversion Project Record Plans	Nov. 2015
Runoff volume estimates and groundwater elevations	Storm Water Treatment Concepts at 325 Blake Road Technical Memorandum	Jan. 2016
Regulatory floodplains	Flood Insurance Rate Map (FIRM) Panel 342	Nov. 2016
Soil boring records	DRAFT Phase I Environmental Site Assessment, Appendix H	Aug. 2017
Water quality monitoring results	Powell Rd. and Lake St. Water Quality Analysis Technical Memorandum	Aug. 2018
Prior Utility Demolition	Hopkins Cold Storage Demolition Project	Jul. 2018
Runoff volume estimates and modeled pollutant loading	325 Blake Water Resources Concept Analysis	Oct. 2019
Tree survey	STN Tree Survey	Jan. 2020
Topographic survey	ALTA/NSPS Land Title Survey	Jan. 2020
Lake Street storm sewer diversion record drawings	HIS Contract D – Lift Station L27, Meters M123A & M123B	Mar. 2020
Wetland Delineation	Stantec Consulting Services 325 Blake Road Site Wetland Delineation Report	Nov. 2021
Minnehaha Creek hydrology and hydraulics	Lower Watershed 100-year XP-SWMM Model	
Powell Road subwatershed hydrologic and hydraulics	Powell Road Diversion HydroCAD Model	

Table 4.1: Summary of Data Acquired. Studies, models, reports, record plans, models, and other data are critical to project planning and design.

The studies and information included evaluations of regional subwatershed sizes and land covers, surface water and groundwater characteristics, potential for pollutant reduction via regional stormwater management BMPs, potential stormwater BMP schematics, and estimated Project costs. Consideration was given to these studies, and the results leveraged as appropriate in context with current discussion and knowledge of the site.

4.2 Stormwater Drainage

The regional stormwater that will be treated by the project's proposed stormwater management facility is largely driven by two storm sewer diversion structures that direct water towards the Site. The stormwater diversion was first initiated by the District in 2013 and includes the diversion of two regional drainage areas to the Site:

- Powell Road subwatershed, which primarily consists of impervious industrial land use with nearby residential and ball fields. The Powell Road subwatershed drains 226 acres of regional stormwater runoff to the Site.
- Lake Street subwatershed, which primarily consists of impervious transportation land use. The Lake Street subwatershed drains 30.3 acres of regional stormwater runoff to the Site.

The Powell Road and Lake Street diversions are first-flush diversions. As such, they were constructed to divert runoff from smaller storms as well as the first flush from larger storms, which contain the majority of pollutants (see *Figure 4.1: Storm Sewer Diversions*). When the diversions reach capacity, the remaining overflow continues downstream in the mainline storm sewer piping and does not flow to the Site.

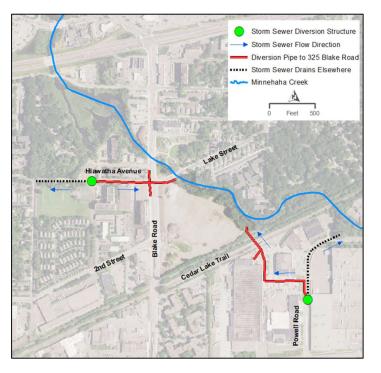


Figure 4.1: Storm Sewer Diversions. Stormwater collected from Powell Road and Lake Street is diverted to the site. When the diversions reach capacity, excess runoff discharges to separate locations.

Site stormwater runoff originates from local high points at the property's border with Lake Street, Blake Road, and the Cedar Lake LRT Regional Trail. These boundaries' conditions range from approximate elevations between 909' to 912' at Lake Street, 912' to 919' along Blake Road, and 911' to 919' along the Cedar Lake LRT Regional Trail. Each site boundary begins with a relatively steep slope down to the property, which transitions to a relatively flat (approximately 1 to 3 percent) grade across the majority of the site, sloping gradually toward Minnehaha Creek.

The importance of stormwater management associated with the Project is emphasized by the regional drainage systems described above, along with the close proximity of the Project to Minnehaha Creek. As an integral part of the regional greenway, the Project offers a unique opportunity to showcase stormwater management, provide visual access to Minnehaha Creek, and develop Balanced Urban Ecology.

4.2.1 POWELL ROAD DIVERSION

According to the District's HydroCAD model and review of record drawings, the Powell Road Diversion consists of a series of storm sewer pipes that drain approximately 226 acres of land. The HydroCAD model was modified by HDR to reflect the diversion condition shown in the Powell Road Diversion construction record drawings (Wenck, 2015). The Powell Road subwatershed is predominantly characterized by developed industrial and residential land use, with minor areas of developed turf grasses (e.g., baseball fields, parks, and landscaped areas).

The Powell Road Diversion structure consists of a 10-ft diameter drainage structure with a 48" reinforced concrete pipe (RCP) inlet. A series of stoplogs function as a weir, diverting stormwater runoff from the inlet pipe toward the Project. The top of the stoplogs is located at elevation 903.5', where water will spill over and travel directly to Minnehaha Creek via the original Powell Road storm pipe. A 6" PVC drain is located at elevation 895.01'. The structure features a sump with an invert elevation 891.96, allowing approximately 3.05' of sediment storage below the PVC drain at full storage capacity. The pipe outlet that diverts water to the Project from the diversion structure is situated at elevation 901.06'. The pipe outlet from the most downstream pipe discharging onto the property is situated at invert elevation 898.40'.

4.2.2 LAKE STREET DIVERSION

The Lake Diversion consists of a series of storm sewer pipes that drain approximately 30.3 acres of land, according to the District's HydroCAD model. The Lake Street subwatershed is predominantly characterized by developed commercial and high-density residential land uses with minimal pervious surfaces.

According to the Lake Street Diversion Record Drawings, the diversion structure consists of an 8-ft diameter drainage structure with a 30" RCP inlet. A concrete weir constructed inside the structure diverts water from the inlet pipe toward the Project (*to be verified by HDR; design will be incorporated into the project plans*). The top of the concrete weir is located at elevation 902.4'. Stormwater would potentially reverse flow over the weir and into the other drainage system at this elevation. The Lake Street Diversion storm sewer drains toward the Site, into a 6-ft diameter manhole with a floor elevation slightly below 897.85 according to the as-built drawings, although the floor elevation is not explicitly recorded. A 12" RC weeper pipe (currently bulkheaded) was constructed from this manhole to allow drainage to daylight onto the Site at

elevation 897.25'. The as-built drawings indicate that the downstream pipes and structures were under water at the time of construction, and standing water was present in the upstream pipes. The storm sewer pipes downstream of the diversion structure feature slopes as low as 0.06% which may result in sedimentation in the pipes regardless of the outlet configuration.

4.3 Minnehaha Creek

The Project is bound to the northeast by a reach of Minnehaha Creek that is relatively stable, featuring a wooded riparian buffer along the creek corridor. This reach of Minnehaha Creek is impaired for Chloride, Fecal Coliform (*E. Coli*), Dissolved Oxygen (DO), Macroinvertebrates Bioassessments, and Fish Bioassessments. A TMDL report is approved for Chlorides and Fecal Coliform, while the remaining impairments have a target TMDL completion year of 2024, according to MPCA's 2020 approved impaired waters list and MPCA's draft 2022 impaired waters list.

Minnehaha Creek originates from Gray's Bay Dam and meanders throughout the watershed to the stream's confluence with the Mississippi River. Flow in Minnehaha Creek is highly variable and subject to rapid fluctuations, which can exacerbate flow-related impairments and stream stability challenges. Stormwater management at the Project considered this variability, assuming that it would not be uncommon for flow rates through this reach to be as low as 10 cubic feet per second (cfs) or to exceed flows up to and above 300 cfs.

Two stream gages were consulted to determine flow characteristics within Minnehaha Creek. One of the stream gages, located upstream of the Project at Gray's Bay Dam, is owned by the United States Geological Survey (USGS) and operated in cooperation with the District. The other stream gage, located downstream of the Project at Hiawatha Avenue, is operated by the USGS. Information obtained from stream gage observations confirmed the assumptions that flows in the creek can range from lower than 10 cfs, to higher than 300 cfs, as demonstrated during the historic flooding that occurred in 2014.

A warm season duration analysis was performed to further evaluate flow rates in Minnehaha Creek. The average daily flows at 50% exceedance during warm seasons range from approximately 34 cfs to 93 cfs. The latter value (93 cfs) provides an estimate for the seasonally high peak flow rate in the creek that is exceeded 50% of the time.

Minnehaha Creek's floodway features regulatory floodplains in the vicinity of the Project. Near the midpoint of the Site, a narrow floodplain exists on the inside of a stream meander. Near the downstream end of the Project, a larger floodplain exists adjacent to the Powell Road diversion's outlet pipe. This floodplain specifically is a critical design and planning feature, located adjacent to a programmed area of the Project. The regulatory flood elevation in this area is estimated to be slightly lower than elevation 899'.

4.4 Geotechnical Investigations

4.4.1 SOIL PROFILE AND GROUNDWATER

According to soil borings obtained in a 1997 soil investigation, soils on the property primarily consist of medium to coarse sand and gravel, with trace amounts of silt and clay. In some

locations, soils near the ground surface are comprised of fill, consisting of topsoil and organic sandy silt. The dominant sand and gravel soil texture is typical to depths of 3 to 6 feet or deeper, which is underlain by 2 to 4 feet of soft clay before transitioning back to sand and gravel at lower depths. This investigation encountered moist soils throughout the boring, except in areas where fill soils were placed. Wet or saturated soils occurred approximately 13 to 14 feet below the ground surface.

Additional soil borings were obtained in May 2013 and May 2014. In May 2013, the groundwater elevation was observed between elevations 889.0 and 891.5 in locations near the proposed stormwater pond. In May 2014, the groundwater elevation was observed at elevation 897.9 near the proposed stormwater pond. The dates of these soil borings were compared to precipitation and stream stage obtained from the stream gages discussed above. The data indicates that groundwater at the site is subject to significant fluctuation in response to precipitation, much like the flow and stage of Minnehaha Creek. Although the soil textures are conducive to infiltration practices, the highly variable depth to groundwater would limit the performance of infiltration BMPs near the elevation of Minnehaha Creek.

A study performed by the University of Minnesota indicates potential for reverse flow from Minnehaha Creek into the riparian groundwater system, although the flow reversals would have minimal impact to the groundwater system. Soil cores indicate that the surficial aquifer in the Project area is overlain by 7 to 12 feet of sandy clay fill material. The aquifer consists of sandy glacial outwash with silt, interspersed with gravel.

4.5 Related Projects

Design of the mixed-use development of the Site is ongoing; performed concurrently with the District's public realm design. This approach allows for collaborative planning, design, construction, and long-term operation and maintenance (O&M).

The design adjacent to the Site's public realm provides for residential and commercial development in response to the construction of the Southwest LRT line and the location of a transit station near the southwest corner of the site. The design currently includes As proposed, the Alatus Alternative included an iconic 10+ story building, several midrise buildings, and townhomes. The taller structures flank Blake Road, with one mid-rise structure extending along the Cedar Lake LRT Regional Trail.

The main roadway through the development forms an arc and coupled with a cascading water feature running from the junction of 2nd Street and Blake Road, it draws people—residents and visitors—to ponds, a skating rink, and restaurants. In addition to the road, there are several pedestrian arteries that open the site up and encourage movement between structures. A boathouse is situated as a terminal view down one of these pedestrian arteries off of Blake Road. Another off of the Cedar Lake LRT Regional Trail turns into a woonerf, or shared street, inviting children to play on its hard surface while pedestrian, bicycles, scooters, and cars all mingle. All of the development's off-street parking is hidden inside occupied buildings. Although parking is extensive, the design intends to minimize the presence of active traffic within the development. Buildings and the open spaces between them will dominate the landscape.

The mixed-use development adjoins the public realm at the restaurants and surrounding areas. The interface between the developments features a vertical wall, maximizing space for both the public realm and the mixed-use development. The restaurant design includes balconies that overlook the ponds, providing another opportunity for water-centric experience. A boat house is proposed near the restaurants, adjacent to the north stormwater pond. The boat house will include a wet well and a stormwater pump, which intakes stormwater from the pond and discharges into the cascading water feature near the west edge of the Site. The pumped stormwater (first treated by the stormwater ponds) would be filtered by natural or cartridge filters to further improve the water quality prior to public exposure. The filtered runoff would then traverse the cascade, ultimately discharging back into the stormwater ponds for additional treatment and recirculation.

5. Design Approach and Analysis

5.1 Stormwater

5.1.1 REGULATORY CRITERIA

Stormwater management and design considerations are governed by various local and state agencies. The primary regulatory criteria influencing design of the Project includes:

- MCWD Rules
- City of Hopkins Code and Ordinances
- Minnesota Pollution Control Agency's National Pollutant Discharge Elimination System (NPDES) Regulations
- Lake Hiawatha Total Maximum Daily Load (TMDL) Report

Regulatory criteria for the developed portion of the Site will be adhered to as part of the Site's development process. For regulatory purposes, the Site is considered redevelopment rather than new development, as the 6.3-acre cold storage facility and 5.3-acre parking area previously occupied the Site.

MCWD's volume control rules vary depending not only on the status of development or redevelopment, but based on the size of the site, the amount of disturbance, and the reduction in impervious surface. Because this project size is greater than 5 acres and disturbs more than 40% of the site, the stormwater management plan must meet the volume control requirements in subsection 3(c) of the volume control rule, requiring abstraction of the first one inch of rainfall from the site's impervious surface.

5.1.2 WATER QUALITY GOALS

In addition to the regulatory design criteria, non-regulatory design goals or objectives to provide regional stormwater treatment have been identified that apply to Project planning, programming, and design. The treatment objectives are based on water quality monitoring results, prior studies, regional plans, and industry best practices.

This reach of Minnehaha Creek is impaired for Chlorides, Fecal Coliform, Dissolved Oxygen (DO), Macroinvertebrates Bioassessments, and Fish Bioassessments. A TMDL report is approved for Chlorides and Fecal Coliform, while the remaining impairments have a target TMDL completion year of 2024, according to MPCA's draft 2020 impaired waters list.

Downstream of the Site is Lake Hiawatha, which has an approved TMDL for nutrients. The Lake Hiawatha TMDL indicates that the average growing season total phosphorus (TP) cumulative watershed load delivered from Minnehaha Creek to Lake Hiawatha is approximately 6,463 pounds. A reduction of 1,907 pounds (29.5% reduction) would be required to achieve the target loading capacity of 4,556 pounds from Minnehaha Creek to Lake Hiawatha.

The 325 Blake Road Restoration and Redevelopment Project has been cited as an opportunity to reduce phosphorus loading to Lake Hiawatha. Estimated pollutant loads to the Site are

summarized in *Table 5.1: Modeled Pollutant Loading* as calculated in the study *Blake Water Resources Concept Analysis (Wenck, 2019).*

Parameter	Lake Street Diversion	Powell Road Diversion	325 Blake Road North	Total
Total Phosphorus (lbs/yr)	48	151	10	209
Total Suspended Solids (Ibs/yr)	8,738	27,618	1,834	38,190

Table 5.1: Pollutant Loading. Of the estimated 209 pounds of TP and 38,190 pounds of TSS delivered to the site, the Powell Road Diversion accounts for approximately 72% of the total pollutant loading.

Prior to this study, the District performed pollutant monitoring in 2016 and 2017, summarized in the *Powell Rd. and Lake St. Water Quality Analysis Technical Memorandum (MCWD, 2018)*. The memorandum describes a TP load of 6.2 lbs/yr from the Lake Street Diversion and 207 lbs/yr from the Powell Road Diversion, although the measured TP loads only occurred between April and October in 2016, potentially underestimating the annual total. The report concludes that particulate phosphorus concentrations are higher than expected from the Powell Road subwatershed, and lower than expected from the Lake Street subwatershed, though the combined annual TP load was greater than expected.

The monitoring results also show that the particulate phosphorus load from the Powell Road subwatershed comprises 90% of the TP on an average annual basis. Stormwater BMPs, including those designed for the project, are typically more effective at removing particulate phosphorus than dissolved phosphorus.

5.1.3 KEY SITE STORMWATER ELEVATIONS

The elevations of Minnehaha Creek, groundwater, and stormwater inflows are key factors in approach to stormwater design. Existing grade for the majority of the site is between elevation 907' to 910'. Within roughly 100 feet of the creek, the site features a more gentle grade towards the creek which steepens at the creek bank.

The Powell Road diversion storm sewer enters the site at elevation 898.40' and the Lake Street diversion storm sewer enters the site at elevation 897.25', roughly 10 feet below the majority of the site's existing grade. Backflow from these diversion storm sewers into mainline storm sewer systems would occur near elevation 901'. Groundwater elevations have been recorded between elevations 889.0' to 898.0'. The creek water surface varies along the site but can vary between elevations 893' to 899', depending on creek flow (see *Figure 5.1: Key Elevations*).

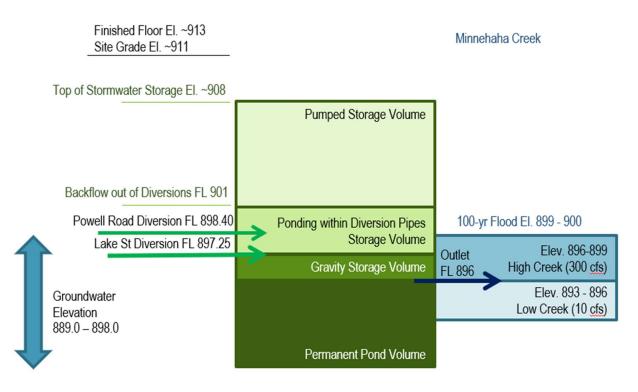


Figure 5.1: Key Elevations. A conceptual sketch of the site elevations demonstrates their significance to stormwater treatment limitations, opportunities, and storage considerations.

Because the storm sewer diversion outfalls are situated in close proximity to groundwater and creek water surface elevations, infiltration as a potential stormwater treatment option was eliminated. The site water elevations are favorable for a stormwater pond, which would have its normal water surface at approximately elevation 896' (north pond) and 897' (south pond), and be partially sustained by groundwater.

5.1.4 STORM SEWER DESIGN

The existing Powell Road Diversion storm sewer drains onto the property through a 36-inch RCP, which enters a manhole and redirects flow toward Minnehaha Creek. The proposed design removes the manhole and extends the 36" RCP, redirecting the pipe away from the creek and toward the south stormwater pond using 36" RCPs to maintain the storm sewer capacity. Prior to discharging runoff into the stormwater pond, the storm sewer drains through a 6' x 12' Nutrient Separating Baffle Box (NSBB) hydrodynamic separator to provide pre-treatment. The NSBB is designed to reduce nitrogen, phosphorus, total suspended solids, and to capture trash and floatables. The storm sewer design flows through the NSBB, discharging into the south stormwater pond at invert elevation 897.0. The outlet consists of a concrete flared end section surrounded by riprap to prevent scour and erosion.

The existing Lake Street Diversion storm sewer drains onto the property through a 42-inch RCP, which drains through a 12" RC weeper pipe which is currently bulkheaded. The proposed design for this project ties into an existing manhole, routing stormwater through a series of 42-inch pipes to maintain drainage capacity. The storm sewer network draining the Lake Street subwatershed directs runoff between the mixed-use development and the proposed trail, draining runoff toward the north pond. Prior to discharging runoff into the stormwater pond, this storm sewer drains through a 8' x 16' NSBB and ultimately discharges into the north pond at invert elevation 896.0. The outlet consists of another concrete flared end section surrounded by riprap to prevent scour and erosion.

5.1.5 STORMWATER POND DESIGN

Prior studies, regulatory requirements, and District goals were considered as factors guiding stormwater management design goals. Best practices published in the Minnesota Stormwater Manual as well as other local regulatory programs were followed and resulted in the preliminary design of a regional stormwater pond. The size of the pond, including surface area, depth, and water quality volume, were optimized to achieve regional water quality goals to the extent practicable. A summary of the design goals used in the layout, sizing and design of a regional stormwater treatment pond with no pumped or upland stormwater treatment is presented below in *Table 5.2: Stormwater Pond Design and Performance Goals*.

Parameter	Design Goal	Status		
Location	Avoid wetlands, floodplains, and buffers ✓ Goal Achiev			
	Volume 1,800 cubic feet per acre of drainage area	x Maximum Extent Practicable ¹		
Permanent Pool	Depth between 3 and 10 feet	🗸 Goal Achieved		
	Install a liner for contamination, karst, or other flow restriction	x Not Applicable		
Water Quality Pool	Volume equal to 1" times impervious surfaces	x Maximum Extent Practicable ²		
Inlets	Provide stabilized inlet areas for high flow conditions	🗸 Goal Achieved		
	Discharge < 5.66 cfs per acre of pond surface area	🗸 Goal Achieved		
	Provide energy dissipation	✓ Goal Achieved		
Outlets	Provide emergency spillway	🗸 Goal Achieved		
	Located to prevent short-circuiting	✓ Goal Achieved		
	Prevent discharge of floating debris	✓ Goal Achieved		
	Maintain or reduce stormwater volume	🗸 Goal Achieved		
Performance	Maintain or reduce peak flow rates	🗸 Goal Achieved		
	Reduce TP and TSS loading	✓ Goal Achieved		
Maintenance	Provide maintenance access bench	🗸 Goal Achieved		
Table continued on the next page				

Safety	Provide 35' offset between pond and water supply wells	✓ Goal Achieved
	Incorporate public safety features (e.g., wetland safety bench)	✓ Goal Achieved

Table 5.2: Stormwater Pond Design and Performance Goals. This table will continue to be reviewed as detailed design is developed to meet these design and performance goals.

¹ Permanent pool volume goal is maximized based on the selected development scenario. Achieving the explicit numerical goal would require over 50% of the property be occupied by a single pond.

² On-site and regional impervious surfaces are pre-developed. Spatial constraints limit the ability to achieve this explicit numerical goal. The proposed design provides water quality treatment equal to the runoff discharged to the site associated with a the 1.25" rainfall event, which exceeds the water quality (first flush) storm event of 1.1" based on water quality monitoring results.

The project uses two stormwater ponds separated by a sheet pile concrete-capped weir wall with the top of the wall designed at invert elevation 897.0. The weir wall creates two separate cells for the stormwater pond, with the south cell receiving runoff from the Powell Road subwatershed, and the north cell receiving runoff from the Lake Street subwatershed. The south pond is designed with a permanent pool elevation of 897.0, and the north pond is designed with a permanent pool elevation of 896.0. When runoff from Powell Road subwatershed occurs, stormwater will flow through the south pond and drain over the top of the weir wall. As the pond reaches and exceeds elevation 897.0, the water surface elevation will overtop the weir wall and the two ponds will have a combined water surface.

The pond outlet structure adjoins the weir wall and is designed as a 40' (L) x 10' (W) concrete structure, allowing for multi-stage (low- and high-flow control) outlets. The objective of the outlet structure is to restrict "first-flush" outflow from the ponds sufficiently to allow settlement of sediments and pollutants and then provide overflow capacity for larger magnitude storm events without engaging the auxiliary overflow culvert. The outlet structure is designed with galvanized steel grating located above the outlets, surrounded by a safety railing. This allows the District to maintain and access the structure but also provides pedestrian access from the trail to the outlet structure where they can safely overlook the stormwater ponds and weir wall.

The outlet structure is designed to intake water from the north pond using a submerged 24-in orifice, located at invert elevation 893.5'. The submerged orifice allows water to enter the structure without being blocked by floating debris at the permanent pool elevation. Inside the structure, a concrete wall with a series of stoplogs is proposed to provide control of the permanent pool elevation. A 4-in diameter orifice is designed in one of the stoplogs, which functions as the low-flow outlet control. As the pond receives runoff and the water surface increases, the 4-in diameter orifice continues to control discharge until the water surface reaches elevation 900.25'. At this elevation, a series of weir openings are designed near the top of the concrete outlet structure. The weir openings are located within both cells of the stormwater pond and each opening is 1.75' (H) x 10' (W). Two weir openings are proposed at the outlet structure's interface with the north pond to provide overflow discharge when the capacity of the 4-in orifice is exceeded. The weir openings provide high-flow outlet control for storm events approaching the 100-year, 24-hour storm. Incorporating several weir openings reduces

the risk of the openings becoming clogged and allows the outlet structure to be supported by concrete walls on the interior to enhance structural integrity. For extreme storm events, an auxiliary overflow culvert is set to the north of the outlet structure to provide additional discharge capacity prior to the pond being overtopped.

A 4' (H) x 6' (W) box culvert conveys outflow from the drainage structure and is sized to accommodate potential outflow from the overflow weirs. The design of the outflow channel into the creek continues to be detailed. A riprap apron is proposed at the downstream end of the culvert to dissipate energy and reduce risk of scour. Given the size of the outlet culvert, the design team is reviewing methods to minimize its visual impact. The channel and culvert will be excavated into the bank and potential plantings or boulder installations will be reviewed to further screen the outlet. Safety bars will be installed on the downstream end to prevent access into the culvert from the downstream side.

5.1.6 ALATUS STORMWATER OFFSET

The stormwater ponds interact with the upland mixed-use development via a wet well and pump located in a boat house (designed by Alatus) located adjacent to the north pond. The pumped stormwater design allows for the mixed-use development to occupy sufficient space on site to meet development goals, while compensating for reductions of water quality volume in the stormwater ponds.

The wet well in the boat house is designed to screen and intake stormwater, pumping it through a ductile iron forcemain to the west edge of the property where the developer's "stormwater cascade" feature begins. The "stormwater cascade" features being designed by the Alatus development will include upland aeration, filtration, and transpiration of stormwater that would not be possible within the stormwater pond. Preliminary filtration concepts include but are not limited to cartridge filters, iron-enhanced sand filters, and similar measures, which are capable of removal up to 85% TSS and 80% TP depending on the design and the pollutant loading parameters. After this additional stormwater treatment is achieved, cleaner stormwater meanders through the cascade, ultimately returning to the south stormwater pond for additional detention and recirculation.

5.2 Stormwater Modeling Results

5.2.1 SITE HYDROLOGY AND HYDRAULICS

The District's Powell Road Diversion HydroCAD model was modified to account for as-built conditions, and to incorporate the design and construction of the Lake Street Diversion, and the proposed design of the Site. The HydroCAD model determines peak flow rates and stormwater runoff volumes discharged to the Site from regional storm sewer diversion networks, and from the proposed stormwater ponds. Design storm depths used in the model are summarized in *Table 5.3: Modeled Design Storm Depths*. These rainfall depths were used for the site hydrologic and hydraulic modeling described throughout this section.

Design Storm ¹	Modeled Rainfall Depth
1.25-in, 24-hour	1.25"
2-year, 24-hour	2.86"
10-year, 24-hour	4.30"
100-year, 24-hour	5.90"

Table 5.3: Modeled Design Storm Depths. Rainfall depths from the Powell Road Subwatershed model were assumed for this analysis.

Peak flow and runoff volume modeling results are documented for various design storms (see *Table 5.4: Regional Subwatershed HydroCAD Modeling Results*). The model hydrology (rainfall depths, distributions) and storm sewer diversion hydraulics will continue to be validated during detailed design.

	Lake Street Diversion		Powell Road Diversion	
Design Storm	Runoff Volume (ac-ft)	Peak Flow Rate (cfs)	Runoff Volume (ac-ft)	Peak Flow Rate (cfs)
1.25-in, 24-hour	1.8	23.2	6.2	19.5
2-year, 24-hour	4.7	37.6	13.8	31.5
10-year, 24-hour	7.1	42.0	22.8	35.5
100-year, 24-hour	9.5	43.4	29.3	36.8

Table 5.4: Regional Subwatershed HydroCAD Modeling Results. Peak flow rates and stormwater runoff volumes were modeled for the regional storm sewers draining onto the site.

The existing and proposed conditions summary compares runoff characteristics from the combined regional subwatersheds and the pre-development site were modeled to determine benefits of the project. Peak flow and runoff volume modeling results between existing and proposed conditions are documented for design storms as shown in *Table 5.5: Existing vs. Proposed HydroCAD Modeling Results*. This analysis indicates that stormwater runoff volumes to Minnehaha Creek are generally decreased by 7 to 9%, and peak flow rates are decreased by approximately 49 to 99% based on the design storm event. This analysis does not account for groundwater flow patterns, which can have an influence on site hydrology and hydraulics. Site hydrologic and hydraulic model outputs are contained in *Appendix A*

	Existing Conditions ¹		Proposed Conditions	
Design Storm	Runoff Volume (ac-ft)	Peak Flow Rate (cfs)	Runoff Volume (ac-ft)	Peak Flow Rate (cfs)
1.25-in, 24-hour	8.7	45.3	8.1	3.5
2-year, 24-hour	22.3	123.0	21.4	30.9
10-year, 24-hour	36.3	169.7	31.9	67.3
100-year, 24-hour	48.3	214.1	42.4	109.5

Table 5.5: Existing vs. Proposed HydroCAD Modeling Results. Peak flow rates and stormwater runoff volumes were modeled for the regional storm sewers draining onto the site.

¹ Existing conditions assume that both regional diversions are constructed, operable, and online without any downstream stormwater BMPs.

Peak flow rates and stormwater runoff volumes are significantly reduced by the stormwater BMPs designed for the project. The stormwater pond's water surface elevations associated with the design storms will impact features of the project and the surrounding environment, including regional storm sewers, Minnehaha Creek, building floor and basement elevations, trail grades, etc. Water surface elevations are influenced by inflows to the stormwater ponds and the multi-stage outlet structure. The water surface elevations associated with the modeled design storms are tabulated in *Table 5.6: Stormwater Pond Water Surface Elevations*.

Design Storm	Peak Water Surface Elevation ¹
1.25-in, 24-hour	900.20'
2-year, 24-hour	900.60'
10-year, 24-hour	900.86'
100-year, 24-hour	901.13'

Table 5.6: Stormwater Pond Water Surface Elevations. The pond's water surface elevation ranges from 900.20' (fully controlled by the low-flow orifice) to 901.13'.

¹ Peak elevation assumes all outlets are fully functional without clogs or reduced capacity, and the pump to developer's cascade feature is operating at 1,200 gpm.

5.2.2 MINNEHAHA CREEK HYDROLOGY AND HYDRAULICS

The District's Lower Watershed XP-SWMM model was run to determine water surface elevations (WSEs) corresponding to the Minnehaha Creek flow rates documented above. The WSEs were reviewed near the upstream end of Project, near the Project's midpoint, and near the downstream end of the Project. WSEs reported by the model are tabulated below (see *Table 5.7: Minnehaha Creek Modeled Water Surface Elevations*).

Flow Scenario	Upstream End	Midpoint	Downstream End
Low (WSE at 10 cfs)	897.2'	895.5'	893.6'
Average (WSE at 93 cfs)	898.0'	896.5'	894.8'
High (WSE at 300 cfs)	899.2'	897.6'	896.2'

Table 5.7: Minnehaha Creek Modeled Water Surface Elevations. Variations between low flows, average daily flows, and high flows provide context for the design of recreational opportunities, bridges, and pond outlets.

Inter-Fluve collected survey data of the Minnehaha Creek floodplain, banks, and bed during project design. A preliminary HEC-RAS model was developed to support hydraulic modeling of the creek to evaluate impacts of the design. The results of preliminary modeling are provided in *Appendix B* and will replace XP-SWMM results in final design for establishing the range of potential creek water surface elevations and velocities for flood magnitude events.

5.2.3 SITE WATER QUALITY MODELING

The Project has a water quality volume design goal of treating 8.0 ac-ft of stormwater runoff from regional storm sewer diversions in accordance with planning and schematic design objectives. *Table 5.8: Water Quality Volume Tracker* on the following page shows stormwater runoff parameters from the development, the compensatory runoff volume required for encroachment on the stormwater ponds, and the water quality provided by the cascade used to compensate for decreased storage in the stormwater ponds. The table summarizes volumetric water quality assessments but does not include results of detailed water quality modeling.

DEVELOPMENT	Impervious Surface		Required Stormwater Abstraction Volume ¹		Provided Stormwater Abstraction Volume ²		Compensatory Volume Managed by Cascade ³	
RUNOFF ANALYSIS	sf	ac	cf	ac-ft	cf	ac-ft	cf	ac-ft
	398,574	9.15	33,215	0.76	35,763	0.82	-2,548	-0.06

1 Equals 1 inch times the impervious surface created by the project

2 Refer to MCWD Stormwater Management Rule, Appendix A, for credit calculation

3 Compensatory Volume = Volume Required - Volume Provided. Negative value indicates the required abstraction value has been met.

POND WATER QUALITY ANALYSIS	Design Volume Goal ¹		Baseline Alternative		Design Volume Provided		Compensatory Pond Volume Required ²	
	cf	ac-ft	cf	ac-ft	cf	ac-ft	cf	ac-ft
	348,480	8.00	368,193	8.45	248,081	5.70	100,399	2.30

1 Based on the Lake Street and Powell Road subwatershed runoff volumes, associated with the 1.25" storm event

2 Compensatory Volume = Volume Goal - Volume Provided

POND/CASCADE WATER QUALITY	Total Design BMP Volume Required ¹		Pond Treatment Volume Provided		Cascade Treatment Volume ²		Treatment Volume Check ³	
SUMMARY	cf	ac-ft	cf	ac-ft	cf	ac-ft	cf	ac-ft
	345,932	7.94	248,081	5.70	287,932	6.61	190,081	4.36

1 Total Volume = Pond Design Volume Goal + Compensatory Volume Managed by Cascade

2 Cascade Volume provided by HydroCAD model during the 1.25" storm event, assuming 1,200 gpm pump rate. Pump design in progress by Alatus.

3 Treatment Volume Check = Pond and Cascade Volume Provided - Design BMP Volume Required. Positive value indicates the goal has been achieved.

Table 5.8: Water Quality Volume Tracker. The pond's water surface elevation ranges from 900.20'

Water quality modeling is currently underway using P8 water quality modeling software, assuming the 60% design moves forward without significant changes to the project concept. The water quality modeling and associated results are moderately dependent upon developer features, as a significant amount of stormwater runoff will be pumped from the ponds filtration BMPs for additional water quality treatment and recirculation. As such, water quality models will be finalized and preliminary results documented when developer BMPs are selected.

Several stormwater management practices selected for the project have published pollutant removal efficiencies that can be considered for preliminary water quality planning, as shown in *Table 5.9: Preliminary Water Quality Estimates*. Site water quality model is underway; model outputs will be contained in *Appendix C* when available.

Stormwater BMP	TSS Removal (%)	TP Removal (%)	TN Removal (%)	Metals Removal (%)	Bacteria Removal (%)
Nutrient Separating Baffle Box ¹	90	19	20	4	4
Constructed Pond ²	60	34	30	70	60
Hydrodynamic Separator ³	80	75	⁴	4	4

Table 5.9: Preliminary Water Quality Estimates. Water quality will be improved by several BMPs that receive flow from the regional storm sewer diversions. The BMPs listed in this table are presented in order of their treatment train location; a Nutrient Separating Baffle Box drains into a constructed pond, which is pumped to the top of the Site's cascade feature before discharging filtered water back into the constructed pond.

¹ Nutrient Separating Baffle Boxes are located between each regional storm sewer diversion and the constructed ponds, providing pre-treatment before runoff enters each pond. The pollutant removal efficiencies listed are according to Oldcastle Infrastructure's publicly available data.

² Constructed pond removal efficiencies are listed in accordance with Minnesota Stormwater Manual's estimates for Design Level 1. These values do not account for recirculated runoff that is pumped from and returned to the ponds.
 ³ The selection and design of a hydrodynamic separator, cartridge filter, sand filter, or other BMP at the top of the Cascade is in progress by the Developer's engineering team. This assessment assumes that a Contech Jellyfish Filter (cartridge filter) or equivalent is used for treatment of pumped stormwater.
 ⁴ Values net published

⁴ Values not published.

5.3 Geotechnical Analysis

A geotechnical analysis was performed to evaluate the slope stability and seepage gradients of the pond embankment and foundation soils. The analysis also included evaluation of the foundation conditions at the pedestrian bridge, weir wall, and outlet structure. To support the geotechnical analysis, a subsurface investigation was completed to gather site-specific geotechnical data. This investigation was completed in January 2022 and results from this investigation were not available at the time of the report. To complete preliminary design, the geotechnical analysis reviewed subsurface stratigraphy and soil parameters of the Site based on available regional data and soil descriptions from the following reports:

- Surficial Geology of Minnesota
- Wenck 2017 Borehole Logs
- Wenck 2017 Monitoring Well Logs

• Piezometer information from *Baseflow Restoration in Minnehaha Creek Watershed with Stormwater Infiltration* report (University of Minnesota, 2013)

Preliminary findings of the geotechnical analysis are summarized in a technical memorandum in *Appendix D*.

5.3.1 GEOTECHNICAL SITE INVESTIGATION

A geotechnical site investigation was completed in American Engineering Testing in early 2022. Preliminary results from the investigation are available, however, lab and in-situ test results are pending.

The objectives of this investigation were to:

- Determine soil and rock stratigraphy across the project site as well as the characteristics of the typical soils encountered.
- Determine a better knowledge of groundwater conditions.
- Determine soil material parameters based on field and laboratory testing for use in final design.
- Assess the degree of variability of the encountered soils based on field and laboratory testing.

The scope of the geotechnical investigation included:

- One standard penetration test (SPT) boring drilled to a depth of 35 feet below ground surface (BGS)
 - Installation of a two-inch diameter PVC cased well with 5-foot screen, located at the depth interval from 30 to 35 feet BGS
 - Development of the well
 - Slug test completed within the well
- Two SPT borings at the proposed edge of the ponds drilled to 50 feet BGS.
- Two SPT borings drilled to bedrock (assumed to be 80 feet) near the proposed bridge abutments.
- Perform laboratory testing on representative soil samples collected from the investigation.

5.4 Structural Analysis and Design

Structural analysis and design is being completed for the:

- Weir Wall
- Outlet Structure
- Pedestrian Bridge Foundation

5.4.1 CODES AND STANDARDS

The following codes and standards were used in the structural analysis and design:

• International Building Code 2018

- Minnesota Building Code 2020
- Reinforced Concrete ACI318-14 & ACI350-06
- Minimum Design Loads for Buildings and Other Structures ASCE7-16
- American Institute of Steel Construction AISC
 - Manual of Steel Construction, 14th Ed.
- American Welding Society D1.4

5.4.2 MATERIAL STRENGTH

The following material strengths are used in the structural design:

- Structural steel: 50 ksi
- Reinforcing steel: 60 ksi
- Concrete: 4,000 psi at 28 days
- Steel sheet pile (pz-22): 50 ksi
- Steel h-piles: 50 ksi

5.5 Trailhead and Overlook

To pull regional trail users into the site, to explore it and its recreational opportunities, Cottageville Park, and the City of Hopkins, an inviting trailhead and overlook is designed as a transition from the Cedar Lake LRT Regional Trail. The trailhead design includes raised planters, block seating, a drinking fountain, bicycle storage and repair areas, and an interpretive kiosk. The trailhead is finished with permeable pavers to differentiate it from the rest of the trail and, and is set among trees to provide shade and wind protection.

5.6 Trail Design

A bituminous trail is designed between Minnehaha Creek and the proposed stormwater ponds, providing a connections between the Cedar Lake LRT Regional Trail, the Minnehaha Creek Greenway, Cottageville Park, and recreational features of the project. The trail consists of a 10-foot wide bituminous surface with 2 feet of aggregate shoulder on each side. The cross slope of the trail is 1.5%, with maximum slopes of 3:1 (H:V) outside of the 2-foot shoulders. The trail alignment is designed to fit the existing topography and conserve the creek's riparian corridor, including mature trees, to the extent practical.

The trail features a graded path that transitions to a constructed ramp over the east slope of the north pond, connecting to the traversable outlet structure overlooking the stormwater ponds. As discussed above. Near the north edge of the property, the trail includes a pedestrian bridge over Minnehaha Creek, connecting the trail to a nature-based play area across the creek and offering pedestrians a place to spend time overlooking the creek. The pedestrian bridge with a steel frame and wood planks, restricting access to pedestrians and light vehicles.

5.7 The Landing

The Landing is designed as a stop for people venturing along the creek and the greenway trails, located along a south bank of Minnehaha Creek. Finished with beach surfacing, this area can

serve as a transfer location between land and water recreation. The Landing includes a picnic area, canoe storage, informal seating, and creek access.

5.8 Nature-Based Play Area

A project outlot is designed as a nature-based play area, which provides a connection between the regional trail and Cottageville Park. This location effectively ties the development with the larger community, and the community with the development. The play area features log stacks, play boulders, precast concrete acorns, benches, tables, and seating areas. Wood fiber surfacing gives the ground a soft finish, while short trails of crushed stone offer access to seating areas closer to the creek.

5.9 Gateway to Greenway

A gateway plaza to the Minnehaha Creek Greenway is designed on a parcel located at the greenway's hinge point at Blake Road and Lake Street. The gateway design includes a sheltering plaza to obscure the sound of traffic, surrounded by a pergola. A water feature is proposed in the center of the plaza, with seating areas located nearby. The plaza is finished with decorative concrete paving, and non-decorative concrete paving allows controlled pedestrian access down to benches in close proximity to the creek.

6. Opinion of Probable Cost

The design elements from the proposed design were tabulated into distinct construction elements and quantities for preliminary construction costing. The AutoCAD-based linework, grading and surfacing models, and pipe network models were used to estimate quantities for most major construction features within the main site parcel (pond, trailhead, landing). The Nature Play Area and Gateway to Greenway areas continued to be a lump sum estimate due to the preliminary nature of some of the design elements

Costs were estimated using several sources, including recent MnDOT average bid prices, RSMeans cost heavy construction cost reference (localized for the metro area), vendor pricing, and prior design/construction experience/references.

The estimate continues to carry two cost contingencies. The design contingency was reduced from 25% to 20%. The 10% construction contingency continues to be included to account for the non-standard construction elements, as well as work near the creek and groundwater table which can increase contractor pricing for construction risk.

A cost summary based on major construction features is provided on the following page (see *Table 6.1: Opinion of Probable Costs*). A more detailed cost estimate table is provided as *Appendix E*.

Construction Item	Cost
Mobilization	\$171,244
Erosion and Sediment Control	\$102,747
Site Preparation	\$95,372
Demolition	\$33,868
Earthwork	\$748,306
Stormwater Piping/Structures	\$257,795
Outlet Structure	\$169,510
Weir Wall	\$288,320
Pedestrian Bridge (over creek)	\$235,500
Pond Site Finishing/Surfacing	\$110,213
Signage/Wayfinding/Interpretation	\$100,000
Site Lighting	\$80,000
Trailhead	\$199,436
The Landing	\$48,390
Picnic Areas	\$58,180
Nature Play Area	\$300,000
Greenway/Gateway Plaza	\$700,000
Contractor Administration/Incidentals	\$369,888
Design Contingency (20%)	\$813,754
Construction Contingency (10%)	\$488,252
Total Construction Estimate	\$5,370,774

Table 6.1: Opinion of Probable Costs. Construction items and associated costs associated with the Baseline Alternative.

The schematic design cost estimate was \$5.48M compared to the current estimate of \$5.37 for detailed design/60%. Several addition features were further detailed such as the outlet structure, weir wall, stormwater system, and the trailhead, landing, and picnic areas. No major design changes were involved in 60%, just additional detailing and with the design advanced, the project construction cost has stayed at a similar level.

Additional cost considerations for project construction are summarized as follows:

• The costs are reflective of the construction areas shown within the work limits on the project drawings (attached separately).

- It is assumed the stockpiles of crushed concrete/pavement will be sold by the District or sourced by the development contractor – no costs were included for handling that material.
- The pedestrian bridge would be a steel frame with wood planks pedestrian and light vehicle access only.
- Pond/stormwater costs versus public realm costs were approximately 50%/50%. This breakdown is provided in the detailed cost estimate in Appendix F.
- Construction costs are fluctuating significantly due to several factors including labor shortages, supply chain issues, COVID-19, etc. These factors could impact the cost of this project, so the use of bid options is recommended to allow the District the ability to stay within construction budget under these conditions.
- The entire western pond edge is comprised of walls, which are assumed to be solely an Alatus cost.
- Construction of the stormwater pond and the Alatus walls/buildings on the west side of the pond at different times or by different contractors simultaneously would be complex and could increase costs. The District should continue discussion with Alatus on shared construction of at least the pond excavation with the Alatus walls/buildings.



Appendix A

Site Hydrology and Hydraulics Model Outputs

(H&H model outputs available separately; to be included with final report)



Appendix B

Existing Conditions Hydraulic Model Technical Memorandum

TECHNICAL MEMORANDUM



То:	Andrew Judd, PE (HDR)	
From:	Briana Drake, PE; Nick Jordan, PE; and	Maren Hancock, PE (Inter-Fluve)
Date:	February 14, 2022	Project: 325 Blake Road Stormwater and Greenway
Re:	Existing Conditions Hydraulic Modelin	g of Minnehaha Creek adjacent to 325 Blake Road

This memorandum summarizes Inter-Fluve's data collection and hydraulic modeling of Minnehaha Creek in the vicinity of 325 Blake Road in Hopkins, Minnesota. The ultimate purpose of the hydraulic model is to evaluate the impacts of HDR's proposed design within the Minnehaha Creek corridor for the 325 Blake Road project. To date, Inter-Fluve has collected survey data and prepared an existing conditions hydraulic model for the project. This memo provides background on the hydrology used, and documentation of model construction.

SURVEY

Inter-Fluve collected survey data of the Minnehaha Creek floodplain, banks, and bed on December 8 and 15, 2021. Data was collected using RTK-GPS equipment. Survey data was collected at bridge crossings, the channel bed, banks, and floodplain surfaces. Large obstructions in the floodplain such as downed trees were also surveyed. Survey data was collected in the State Plane Minnesota South coordinate system referenced to the NAD83 datum. Elevations are referenced to the North American Vertical Datum of 1988 (NAVD88).

HYDRAULIC MODEL CONSTRUCTION

Hydrology

Flows in Minnehaha Creek are controlled by releases at Gray's Bay Dam at the outlet of Lake Minnetonka, impacting creek hydrology. For the purposes of this modeling effort, flow data was reviewed from the following sources and is shown in Table 1 below.

- Peak flow data from the USGS StreamStats application
- Flood flow data from the FEMA Flood Insurance Study flood flows
- Output from the Minnehaha Creek Watershed District's XP-SWMM model

Annual Exceedance Probability	Average Recurrence Interval (years)	USGS StreamStats Flow (cfs)	XP-SWMM Flow (cfs)	FEMA Flow (cfs)
67%	1.5	111	233	
50%	2	144	273	
20%	5	244	393	
10%	10	329	469	544
4%	25	454	512	
2%	50	560	546	543
1%	100	683	684	641
0.2%	500	1,000		949

Table 1. Comparison of Reviewed Hydrology Data

Based on the comparison of available data, in the model we included the series of XP-SWMM flows, the 100-year FEMA flow, and a series of low flows (30 cfs and 60 cfs) presumed to be frequent flows within the regulated creek system.

Model Development

A one-dimensional steady state hydraulic model was created in the U.S. Army Corps of Engineers Hydraulic Engineering Center River Analysis System (HEC-RAS) software version 6.1.0. The existing conditions model geometry was developed using survey data merged with LiDAR digital terrain models in AutoCAD Civil 3D to create a combined topographic and bathymetric surface. The model extends from approximately 150 feet upstream of Blake Road to downstream of Meadowbrook Road.

All cross-section overbanks were cut from the LiDAR surface. Where model cross sections closely aligned with survey data, the surveyed points were used to create the cross-section geometry. Where the survey data was further away from the cross sections, the channel geometry was cut from the combined surface which created an interpolated geometry between bounding surveyed cross sections. Bridge data was manually added into the model based on Inter-Fluve's survey data and asbuilt drawings received from Minnehaha Creek Watershed District. Bridges were included for the crossings at Blake Road, Lake Street North East, the water main crossing, and Meadowbrook Road. The bridge decks for the Cedar Lake Trail and SWLRT bridge crossings were not included in the model geometry at this time because no survey data was collected due to the southern side of the crossing was under construction during the survey. Flood flows do not exceed the elevations of the low chord of the bridges based on reviewed bridge design drawings. Cross sections were included to represent the retaining walls and overbank characteristics in this section.

Computational Parameters

Manning's "n" values were assigned based on observed channel substrate and floodplain vegetation conditions. Table summarizes the Manning's "n" values used along the reach.

Table 2. Manning's "n" values used in the hydraulic model.

Location	Manning's "n"	Typical Descriptions	Notes
Channel	0.035	Channel with sand/gravel substrates and little woody debris.	Used throughout the reach
Channel	0.050	Channel with gravel/cobble substrate and some woody debris.	Used for areas with log jams or significant woody debris
Overbank	0.050	Turf, scattered brush and heavy weeds	Lawn type overbank.
Overbank	0.080	Medium to dense brush, in winter (i.e., without foliage)	Shrub type overbank.
Overbank	0.100	Dense brush	Forest type overbank.

A normal depth boundary condition was applied to the upstream and downstream model boundaries. The average bed slope in these locations was used to estimate normal depth conditions. The boundaries were located sufficiently far from the area of interest such that the selection of boundary condition does not influence hydraulic model results near the area of interest.



Appendix C

Site Water Quality Model Outputs

(Water quality modeling underway; to be included with final report)



Appendix D

Geotechnical Findings Technical Memorandum

Technical Memorandum

Date:	Friday, February 18, 2022
Project:	325 Blake Road Regional Stormwater and Greenway/Cottageville Park Phase II Riparian Restoration Project, Hopkins, MN Project No. 10268112
To:	File
From:	Kerrie Berg, PE, HDR Engineering Inc. Greta Backman, PE, HDR Engineering Inc. Erica Bley, EIT, HDR Engineering Inc.
Subject:	Geotechnical Findings

Introduction

This technical memorandum presents the results of the geotechnical analyses and engineering evaluation of the proposed regional stormwater treatment pond to be located at 325 Blake Road in Hopkins, Minnesota. This parcel was purchased by Minnehaha Creek Watershed District (MCWD) in 2011 with the intent to create a transformative, water-centric development on this site adjacent to Minnehaha Creek premised on its vision of Balanced Urban Ecology (MCWD 2021).

This memorandum presents findings, conclusions, and recommendations regarding:

- Evaluation of pond embankment exit gradients
- Evaluation of the slope stability of the pond embankment and foundation soils
- Evaluation of the foundation conditions at the pedestrian bridge, weir wall, and outlet structure.

Project Description

Figure 1 shows the location of the proposed two-pond concept stormwater design, which is located to the west of Minnehaha Creek. The proposed normal water surface of the north pond is elevation 896 feet, and the south pond is elevation 897 feet. The proposed overflow elevation is 901 feet. The pond will be excavated into existing ground.

The proposed footprint is approximately 1.7 acres. There is approximately 8 acre-feet of storage at the ponds normal water surface elevations. The top of the pond embankment would be at an elevation of 901 feet, or higher depending on surrounding ground surface elevations. The bottom elevation of the south pond will be excavated to an elevation of 890 feet and the north pond to 889 feet. This results in a maximum pond slope height of approximately 20 feet based on the maximum ground elevation at the pond footprint of approximately 910 feet.

Sections SL-2 (STA 103+50, typical cross section of the north pond) and SL-3 (STA 105+00, typical cross section of the south pond) from Figure 1 are shown in Figure 2. These embankment cross sections have interior side slopes ranging from 3H:1V to 10H:1V.

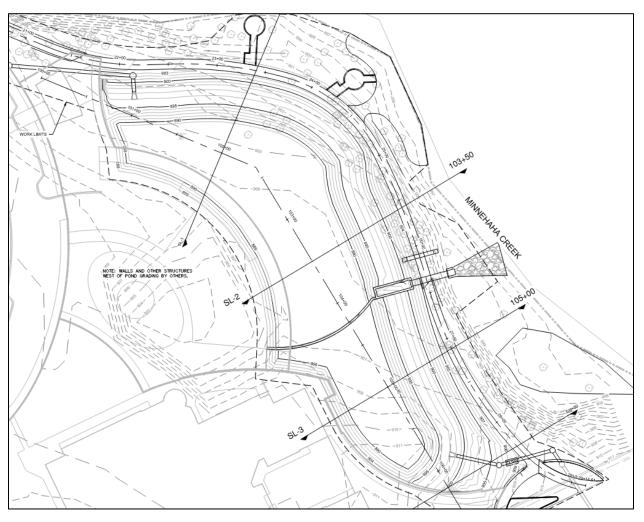
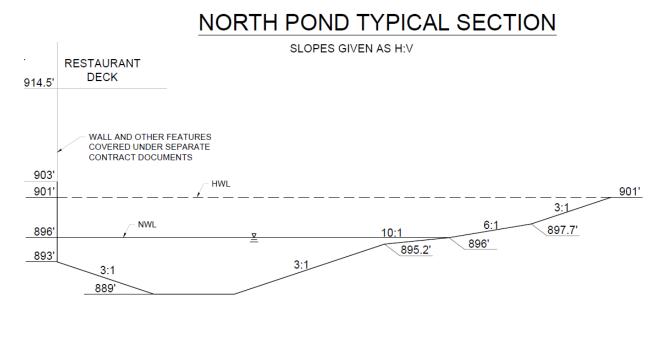


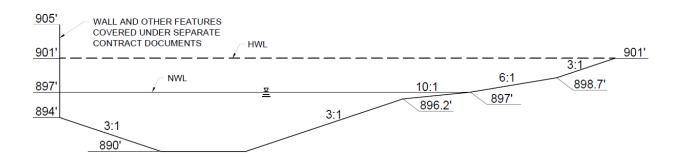
Figure 1. Plan View, Proposed Stormwater Basin

Figure 2. Typical North and South Pond Cross Sections (Sections SL-2 and SL-3 respectively, shown in Figure 1)



SOUTH POND TYPICAL SECTION

SLOPES GIVEN AS H:V



Geotechnical Site Investigation

In January 2022, a geotechnical site investigation was completed by American Engineering Testing located in Saint Paul, MN. Preliminary results from the investigation are available, however, lab and in-situ test results were not available at the time of this report, so the findings from the investigation are not included report but will be incorporated into future reports.

The objectives of this investigation were to:

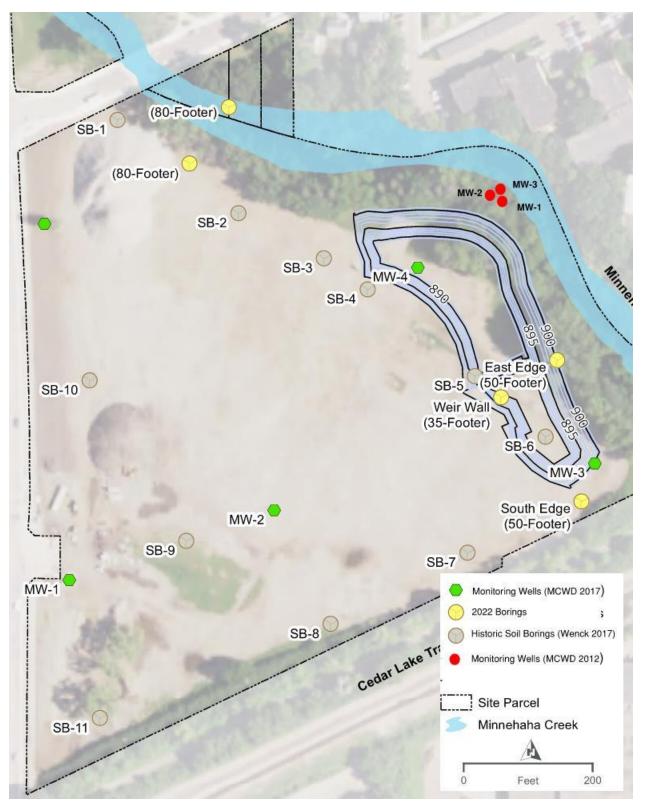
- Determine soil and rock stratigraphy across the project site as well as the characteristics of the typical soils encountered.
- Determine a better knowledge of groundwater conditions.
- Determine soil material parameters based on field and laboratory testing for use in final design.
- Assess the degree of variability of the encountered soils based on field and laboratory testing.

The scope of the geotechnical investigation included:

- One standard penetration test (SPT) boring drilled to a depth of 35 feet below ground surface (BGS)
 - Installation of a two-inch diameter PVC cased well with 5-foot screen, located at the depth interval from 30 to 35 feet BGS
 - Development of the well
 - Slug test completed within the well
- Two SPT borings at the proposed edge of the ponds drilled to 50 feet BGS.
- Two SPT borings drilled to bedrock (assumed to be 80 feet) near the proposed bridge abutments.
- Perform laboratory testing on representative soil samples collected from the investigation.

The SPT sampling will provide an insight of the in-situ ground conditions, specifically the relative strength of the soil. The piezometer installed will be used to measure groundwater at the pond location and test the in-situ permeability of the subsurface materials at that location. The rock core will be used to determine the relative quality of the rock. Finally, lab testing will be used to characterize encountered soils and help determine the soil parameters for final design. Figure 3 shows the location of historic borings and wells and the 2022 borings mentioned above.

Figure 3. Borehole Location Map



Subsurface Stratigraphy and Soil Parameters

Subsurface stratigraphy at the site was determined based on the available regional geological data and soil descriptions from historic geologic reports for the site:

- Surficial Geology of Minnesota [1]
- Wenck 2017 Borehole Logs [2]
- Wenck 2017 Monitoring Well Logs [2]
- Piezometer information from *Baseflow Restoration in Minnehaha Creek Watershed with Stormwater Infiltration* report (University of Minnesota 2013) [3]

Based on the available data, the following soils are found at the site, listed from the ground surface downward:

- Fill (SM/SC) Previous boring and well logs describe a fill material typically 2 to 5 ft thick overlying native sand deposits. The fill is classified as a gravelly, silty to clayey sand (SM/SC).
- Glacial Outwash (SP)-The native sand deposit located below the fill are described a as gravelly to silty sand based on previous boring and well logs. The fill is classified as a gravelly sand (SP). Regional geological maps show that the predominant native surficial material at the site is a glacial outwash deposit. This material is described as gravelly sand Outwash.

Preliminary results from the 2022 investigation confirm the general stratigraphy trends described above.

Soil Strength Design Parameters

Analyses were performed to assess the factor of safety for slope stability at critical cross-sections through the ponds. Pond slope stability modeling requires strength parameter inputs. The strength parameters selected for the materials encountered within the pond slopes are presented in Table 1. These parameters include the material unit weight and the drained shear strength for the soil. Soil strength parameters were selected based on values presented in literature [4,5,6]. Strength material properties will be refined based on the field and laboratory test results from the 2022 Geotechnical Investigation.

Seepage Parameters

The primary input parameter in seepage analyses is hydraulic conductivity (or "permeability") of the materials at the site. The permeability, as well as the other hydraulic input parameters, were selected based on values published from literature [7,8,9,10]. Hydraulic material properties will be refined based on field and laboratory test results from the 2022 Geotechnical Investigation.

Table 1. Soil Parameters

Soil Type	Moist Unit Weight γ (Ibs/ft ³)	Unit Parameters 😴		Anisotropy k _v /k _h ⁽¹⁾	Coefficient of Volume Compressibility (M _v) /psf ⁽²⁾	Saturated olumetric Water Content, Os (ft³/ft³) ⁽³⁾	Residual Volumetric Water Content, Or ⁽⁴⁾	GeoStudio SWCC Function	
				An	Ŭ	Ŷ	>	ő	
Fill (gravelly, silty to clayey sand)	125	0	30	1.64E-05	0.5	5.00E-06	0.32	0.032	Silty Clay
Sand (gravelly sand with varying amounts of silt)	123	0	30	1.64E-04	0.5	2.00E-06	0.33	0.033	Silty Sand
Sheetpile	N/A	N/A	N/A	3.28E-08	1	N/A	N/A	N/A	N/A

Notes:

- (1) USBR (United States Bureau of Reclamation) DS13-8 Seepage 2014
- (2) Calculated from Young's modulus values from AASHTO 2014.
- (3) Calculated from void ratio estimate from Fredlund and Rahardjo 1993.
- (4) Leij et al, 1996.

Seepage Analysis and Slope Stability

Seepage analysis and slope stability were evaluated using SEEP/W and SLOPE/W in GeoStudio 2021 R2 software [11]. SEEP/W uses the finite-element analysis technique to model water movement and porewater pressure distribution within porous materials, such as soil and rock. This program can analyze both simple and highly complex seepage problems, including saturated and unsaturated flow, steady-state and transient conditions, and various boundary conditions.

SLOPE/W module uses limit equilibrium theory to compute the factor of safety of earth and rock slopes. Like SEEP/W, SLOPE/W has an established track record for analyzing critical infrastructure within the geotechnical profession. In the limit equilibrium approach, the geologic material is assumed to be at the state of limiting equilibrium and a factor of safety is computed. SLOPE/W can use a variety of methods to compute the factor of safety of a slope while analyzing complex geometry, stratigraphy, and loading conditions.

The loading cases modeled in the seepage analyses were also analyzed for slope stability. GeoStudio allows for integration of SEEP/W and SLOPE/W, such that the porewater pressures and phreatic surface computed in SEEP/W can be automatically imported and used in the SLOPE/W analysis. This allows for a more realistic stability analysis than can be obtained by drawing in a phreatic surface. For any node on the ground surface line where the pore water pressure is positive (i.e., surface ponding condition), SLOPE/W automatically computes the equivalent weight of the water above the ground surface. A minimum slip surface depth of 3 feet was set. Slip surfaces less than 3 feet were assumed to be considered a maintenance issue.

Cross Section Geometry and Subsurface Stratigraphy

Two critical embankment cross sections were selected to evaluate seepage and stability for the proposed stormwater pond embankment based on preliminary embankment geometry and the encountered subsurface conditions at the site. Existing survey data, the Minnesota Department of Natural Resources MNTOPO website [12], existing piezometer data, and the Schematic Design

Memorandum [13] were used to determine the ground surface topography beyond the proposed pond dimensions and to estimate the bathymetry of the Minnehaha Creek. Locations of the two cross sections (labeled North-South and East-West) are shown in Figure 4 and were deemed critical based on ground surface elevations and proximity to Minnehaha Creek. Figure 5 shows the East-West cross section and slope stability results for the High Pond, Low Creek case modeled in SLOPE/W. Figure 6 shows the North-South cross section and seepage output for the Empty Pond, High Creek case modeled.

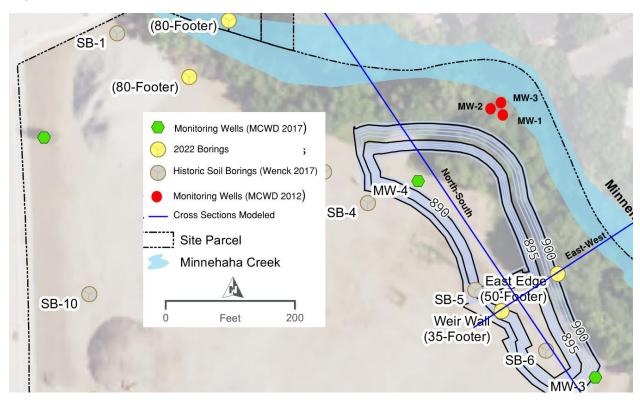


Figure 4. Location of modeled cross sections

Figure 5. East-West cross section showing slope stability results for the High Pond, Low Creek case modeled

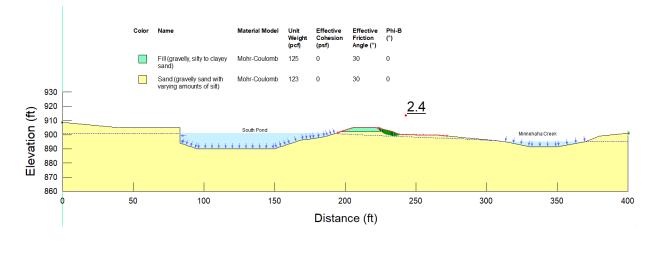
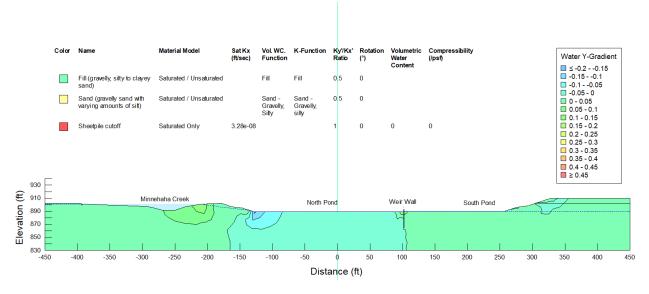




Figure 6. North-South cross section showing seepage output for the Empty Pond, High Creek case modeled



Loading Conditions

The hydraulic boundary conditions for the seepage models are provided in Table 2.

Cross Section	Loading Case	Analysis Type	Slope analyzed	Pond Water Elevation [feet]	Far field Creek Conditions
East-West	Case 1: Empty Pond, High Creek	Steady- State	Interior Slope	890	Minnehaha Creek Elev. 901 feet
	Case 1a: 894-foot Elev. Pond, High Creek	Steady- State	Interior Slope	894	Minnehaha Creek Elev. 901 feet
	Case 2: High Pond, Low Creek	Steady- State	Exterior Slope	901	Minnehaha Creek Elev. 895 feet
North- South	Case 1: Empty Pond, High Creek	Steady- State	Interior Slope – North Pond	890	Minnehaha Creek Elev. 901 feet
	Case 1a: 894-foot Elev. Pond, High Creek	Steady- State	Interior Slope - North Pond	894	Minnehaha Creek Elev. 901 feet
	Case 2: High Pond, Low Creek	Steady- State	Exterior Slope – North Pond	901	Minnehaha Creek Elev. 895 feet
	Case 1: Empty Pond, High Creek	Steady- State	Interior Slope – South Pond	890	Minnehaha Creek Elev. 901 feet

 Table 2. Hydraulic Boundary Conditions for Loading Cases

Currently, there is limited surface water elevation data of the Minnehaha Creek at the Blake Road site. In addition, well data at the site is limited. Groundwater monitoring from the Wenck 2017 report [2] (included in Attachment A) provides a limited history for the groundwater conditions. The lowest reading from Monitoring Wells 3 and 4 (the Wenck 2017 wells that are closest to the proposed stormwater basin, see Figure 1) is 896.73 feet. Unfortunately, readings from the three monitoring wells described in the University of Minnesota 2013 report [3] are based on a local benchmark that was assigned an elevation of 100 feet and the readings are not useable at this time. Considering the limited data available, conservative water elevations were selected and are described below:

- The maximum creek elevation is based on the Wenck 2017 Monitoring Well 3 water level reading at time of install (rounded to the nearest foot to obtain an elevation of 901 feet, which coincides with the high-water level of the pond; see Attachment A).
- The low creek elevation was selected as 895 feet based on information from the Wenck 2016 technical memo [14] (included in Attachment A), which stated an assumed groundwater level under the pond of 895 feet. This was selected as it was lower than the 896.73 feet elevation (the lowest reading from Monitoring Wells 3 and 4) from the Wenck 2017 report [2]. Because of the permeable granular soils at the sight, it is assumed the groundwater level readings at the wells match up well with the Creek water level.
- The high-water level elevation of the pond is 901 feet elevation. This is the overflow elevation of the pond (see Figure 2).

No additional external loading was applied to the models, such as surcharge loads associated with vehicle traffic or stockpiles. Using the seepage conditions modeled based on the hydraulic loading conditions in Table 2, the slope stability modeling cases were analyzed for the interior and exterior pond slopes. For this analysis, only steady-state seepage conditions were analyzed, and only drained strengths were applied for the soil strength parameters.

Seepage and Stability Results

Seepage Analysis Results

The pond cross sections for the proposed stormwater pond were evaluated with respect to excessive exit gradients. Guidance for *High Exit Gradients in a Cohesionless Soil* from USBR Design Standards No.13 Chapter 8: Seepage (2014) was used to evaluate seepage concerns [7].

Excessive exit gradients in cohesionless soil can lead to a "quick" ground condition at the location of seepage, which could lead to the presence of sand boils [7] and could possibly develop into progressive backward erosion and pond breach. To evaluate for the potential of excessive gradient (aka heave) in the seepage model, the vertical exit gradient (I_e) in the native Sand where the piezometric line exited the slope (the area of maximum vertical gradient) was evaluated with respect to the critical gradient, I_c , of the Sand. The I_c is defined as the ratio of the soils' buoyant unit weight to the unit weight of water. The FOS with respect to the vertical exit gradient is the ratio of the critical gradient to the exit gradient. For new dams, USBR recommends a FOS (factor of safety) of 4.0 to evaluate heave. The seepage results for all cross sections demonstrate a FOS greater than 4.0.

In addition, seepage analysis was evaluated per USACE EM 1110-2-1913, "Design and Construction of Levees" manual guidelines [16], which states that the exit hydraulic gradient does not exceed 0.5 at the toe of the pond embankment. Seepage results for all cross sections

demonstrate the exit gradient is less than the maximum allowable value of 0.5 at the toe of the pond embankment for both interior and exterior slopes, indicating seepage design requirements are satisfied.

Table 3 shows the seepage analysis results. See Attachment B for figures of the SEEP/W seepage analysis results.

Cross Section	Piezometric Conditions	Slope analyzed	Exit Gradient – USACE ¹ Recommended < 0.5	Factor of Safety- Heave Recommended USBR ² Minimum- 4.0
	Case 1: Empty Pond, High Creek	Interior Slope, South Pond	0.30	4.2
East-West	Case 1b: 894-foot Elev. Pond, High Creek	Interior Slope, South Pond	0.15	8.4
	Case 2: High Pond, Low Creek	Exterior Slope, South Pond	0.10	12.6
North- South	Case 1: Empty Pond, High Creek,	Interior Slope, North Pond	0.30	4.2
	Case 1b: 894-foot Elev. Pond, High Creek	Interior Slope, North Pond	0.15	8.4
	Case 2: High Pond, Low Creek	Exterior Slope, North Pond	0.15	8.4
	Case 1: Empty Pond, High Creek	Interior Slope, South Pond	0.00	>>4.0



¹ USACE = United States Army Corps of Engineers

² USBR = United States Bureau of Reclamation

Slope Stability Analysis Results

Slope stability criteria and guidance as defined in EM 1110-2-1913 and EM 1110-2-1902 [15,16], was used to evaluate the stormwater pond embankment stability. This was deemed the most appropriate guidance for this project.

Long Term - Steady State Seepage

For the steady state condition, the water surfaces as described in Table 2 were first used to estimate the pore water pressures in the embankment based on a seepage analysis. The pore water pressures from the seepage analysis were used in the stability analysis. Drained soil strengths are used for this analysis.

Results

The cross sections were evaluated using established FOS typically used by USACE as defined in EM 1110-2-1913 and EM 1110-2-1902 [15,16]. For the long-term stability condition, a factor of safety of 1.4 was selected. The minimum factors of safety calculated for each section under the various loading conditions are shown in Table 4. All factors of safety determined for the embankment were above minimum requirements except for the East-West (south pond) and North-South (north pond) cross sections under the empty pond, high creek condition. By increasing the pond water level to an elevation of 894 feet, a factor of safety of 1.4 is achieved. Attachment C includes figures of the SLOPE/W slope stability analysis results.

Case		Slope Analyzed	USACE Recommended Minimum Factor of Safety (EM 1110-2-1913)	East- West Cross Section (South Pond)	North- South Cross Section (North Pond)	North- South Cross Section (South Pond)
	Case 1: Empty Pond, High Creek	Interior Slope	1.4	1.3	1.1	1.9
Steady State Seepage- Drained (Long-term) Loading	Case 1b: 894' Elev. Pond, High Creek	Interior Slope		1.4	1.5	N/A
	Case 2: High Pond, Low Creek	Exterior Slope		2.4	1.4	N/A

Table 4. Slope Stability Results

Slope Stability and Seepage Findings

Preliminary engineering evaluations demonstrate that design requirements are satisfied for the proposed Blake Road Stormwater Pond except for Case 1 of the East-West (south pond) and North-South (north pond) cross sections (under the empty pond, high creek condition). While these two cases are below the recommended FOS values, they do still have a FOS greater than 1.0. All analysis were completed under steady state seepage conditions, which is conservative. If the pond is raised to elevation 894' FOS requirements are met.

In addition, the case of an empty pond and a high river is not likely. However, the pond may be emptied for maintenance purposes if it's drawn down for weir wall or outlet structure maintenance. These slope stability results can be used to inform maintenance recommendations (e.g., avoid draining the pond when the creek is high).

Final analysis can be completed upon soil testing to refine parameters, groundwater information, and information on the Minnehaha Creek water elevations.

Pedestrian Bridge, Outlet Structure, and Weir Wall Evaluation

Pedestrian Bridge

The 2022 subsurface investigation included two SPT borings drilled to bedrock (encountered at approximately 70 to 73 feet below ground surface) near the proposed bridge abutments (the two 2022 borings labeled '80-footer' on Figure 3). Preliminary results indicate pile foundation with refusal at approximately elevation 832 feet (to bedrock). The analysis will be finalized once soil laboratory results and field tests are completed.

Outlet Structure

The 2022 subsurface investigation included one SPT boring drilled to 50 feet below ground surface near the proposed weir wall (the 2022 borings labeled 'East Edge (50-footer)' on Figure 3). Preliminary results indicate a pile foundation will not be required but helical anchors may be considered to mitigate uplift from groundwater. The analysis will be finalized once soil laboratory results and field tests are completed.

Weir Wall

The 2022 subsurface investigation included one SPT boring drilled to 35 feet below ground surface near the proposed weir wall (the 2022 borings labeled 'Weir Wall (35-footer)' on Figure 3). The weir wall will consist of concrete capped sheetpile extended to a depth of 20 feet below the bottom of the pond. The weir wall design will be finalized once soil laboratory results and field tests are completed.

FJS

Abbreviations

AASHTO LRFD. American Association of State Highway and Transportation Officials Load-and-Resistance Factor Design.

EM. Engineering Manual.

FOS. Factor of Safety.

Ft. Feet.

- Ic. Critical Gradient.
- Ie. Exit Gradient.

MCWD. Minnehaha Creek Watershed District.

NAVFAC. Naval Facilities Engineering Command.

SWCC. Soil-Water Characteristic Curve.

- USACE. United States Army Corps of Engineers.
- USBR. United State Bureau of Reclamation.

FJS

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Attachments

Attachment A – Borehole Logs Attachment B – SEEP/W Seepage Analysis Results Attachment C – SLOPE/W Slope Stability Analysis Results

Attachment A

- Existing Monitoring Well Logs
- Peizometer Data from the University of Minnesota 2013 Report
- Wenck 2017 Groundwater Monitoring Report
 - Wenck 2016 Technical Memo



ORGANIZATION



Baseflow Restoration in Minnehaha Creek Watershed with Stormwater Infiltration



MWMO Watershed Bulletin: 2014-3 Prepared for the MWMO by: University of Minnesota

Appendix IV. Piezometer Installation Details

Shallow monitoring wells were installed at 4 sites along the creek as described in Section 3.3. At each site, three to four 2-in diameter, PVC wells were installed in the riparian zone approximately perpendicular to flow in the creek. A plan view of piezometer locations is provided in Figure 12. The following sections provide greater detail as to piezometer installations and observed stratigraphy for each of the sites.

Jidana Wetland

All wells at the Jidana wetland site were handaugered to a depth ranging from 3 to 5.5 ft below the surface. Vegetation at the site transitioned from cattails (edge of the channel to piezometer 2 as labled in Figure A.5.), to Phragmites (piezometer 1), to trees (piezometer A). All piezometers were screened in the sandy aquifer underlying up to 4 feet of organic material at the site. Piezometers were screened across the bottom-most 10-inches of the PVC pipe. The aquifer was comprised predominantly of coarse sand interspersed with gravel and small rocks (up to 3-inches in diameter). With the exception of piezometer 1, which was dry from August 2012 to March 2013, the water table remained above screened sections.

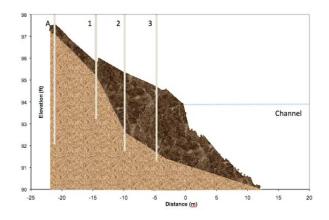


Figure A.5. Cross-section of wells installed at the Jidana wetland. The cross section is comprised of a layer of organic material (dark brown shading) up to 4-ft thick near the stream underlain by a layer of coarse sand and gravel/cobble (light brown shading) to which the 10-in screened interval at the bottom of all wells is open.

Lahti Wetland

Two sets of piezometers were installed at the Lahti wetland (Figure 12). Piezometers at the upstream end of the site were installed during the spring of 2013. Piezometers 1 and 3 were installed by hand while a drill rig was used to install piezometers 2s and 2d. Cattails were the dominant vegetation type from the channel to piezometer 1. A layer of organic material with a relatively uniform thickness of 4 to 5 ft was encountered at this site. Although at different depths (Figure A.6.), all piezometers were open to the same sand and gravel aquifer underlying the layer of organic material. An additional bore hole was augered near the location of piezometers 2s and 2d to discern the presence of any low permeability layers within the aquifer. Such a layer, consisting of silty-clay till, was encountered at a depth of 45 ft. The water table remained perched above the ground surface at all piezometers from June to early August, 2013.

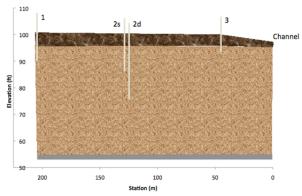


Figure A.6. Cross-section of wells installed on the upstream end of the Lahti wetland site. A relatively uniform, 4-ft thick organic layer (brown shading), overlays the sandy aquifer (light brown shading). The 10-in screened interval of all piezometers is open to the sandy aquifer. A confining sandy clay layer (dark gray shading) was encountered at a depth of about 45 ft in a boring conducted near piezometers 2s and 2d. Note that the extension of this layer across the rest of the site is assumed.

The second set of piezometers was installed approximately 1000 ft downstream (Figure A.7.) Grasses, namely *Phragmites*, were the dominant vegetation type across this site. A relatively thick (about 6 ft) organic layer was encountered immediately below the ground surface. A 10-inch screened section at the bottom of all piezometers was open to the sand and gravel aquifer underlying this organic layer. A thin clay layer was encountered between the organic and sandy aquifer at piezometers 1 and 2.

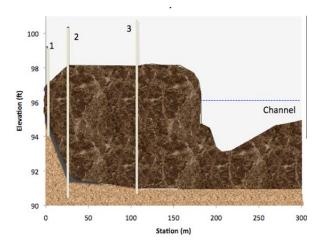


Figure A.7. Cross-section of wells installed on the downstream end of the Lahti wetland site. A thick layer (up to 6 ft) of organic soil (brown shading) overlays a layer of gleyed, silty sand (light brown shading) to which the 10-in screened interval of all piezometers is open. A thin clay layer (solid gray shading) capping the sand layer was observed at Piezometers 1 and 2. The piezometric head in piezometer 3 was greater than the ground surface throughout monitoring in 2013.

Blake Cold Storage Site

Soil characteristics within the riparian area immediately adjacent to the site were examined with a hand auger (Figure A.8.). Piezometer installation was also completed with a hand auger in July 2012. A silt layer ranging in thickness from 1 to 3 feet overlays a relatively compacted till layer (Figure A.9.) Compared to the other sites, this gravely sand layer was more difficult to penetrate with the hand auger. Additional soil explorations of the lawn area between the wooded riparian area and parking lot of the Cold Storage plant were conducted by a drill rig (Figure A.8.). Borings in the lawn area indicated the presence of a 7 to 12 ft layer of silty- to clayey- sand fill material overlying a silty-sand aquifer.



Figure A.8. Approximate locations of piezometer installations (solid red circles) within wooded riparian area of creek and soil borings completed with a drill rig (black and white circles) in the upslope lawn area.

Well 1 Well 2 101 Well 3 Well 3 Channel -6 -1 4 9 14 19 24

Figure A.9. Cross-section of wells installed at the Cold Storage site on Blake Road. Underlying a 1-2 foot layer of silt (dark brown shading) is a thick layer of compacted loamy sand till with large gravel and stones embedded throughout. The 10-in screened interval of all wells is open to this layer.

Utley Park

Soil stratigraphy was initially explored by hand auger during 2012 in the lawn area immediately adjacent the stream. In general, the site is overlain by about 0.5 ft of top soil, underlain by about 2 ft of compacted clay. A graveley sand layer was encountered below the clay layer; however, the diameter of gravel in this layer was too large to permit penetration with the hand auger. Due to interest in this site as a location in which groundwater may be perched, subsequent borings and piezometer installations were conducted during the spring of 2013. Figure A.10. illustrates the location and depth of piezometers relative to the stream channel. A relatively low conductivity till layer was encountered at a depth of 50 ft.

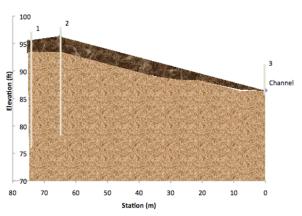


Figure A.10. Cross-section of wells installed at the Utley Park site in Edina. Underlying a 1-2 foot layer of silty-clay fill material (dark brown shading) is a thick layer of compacted loamy sand till with large gravel and stones embedded throughout. The 10-in screened interval of all wells is open to this layer.

Phase II Environmental Site Assessment Addendum: Groundwater Monitoring Report



Hopkins Cold Storage 325 Blake Road North Hopkins, MN

Prepared for: Minnehaha Creek Watershed District and Hennepin County

15320 Minnetonka Blvd. Minnetonka, MN 55345



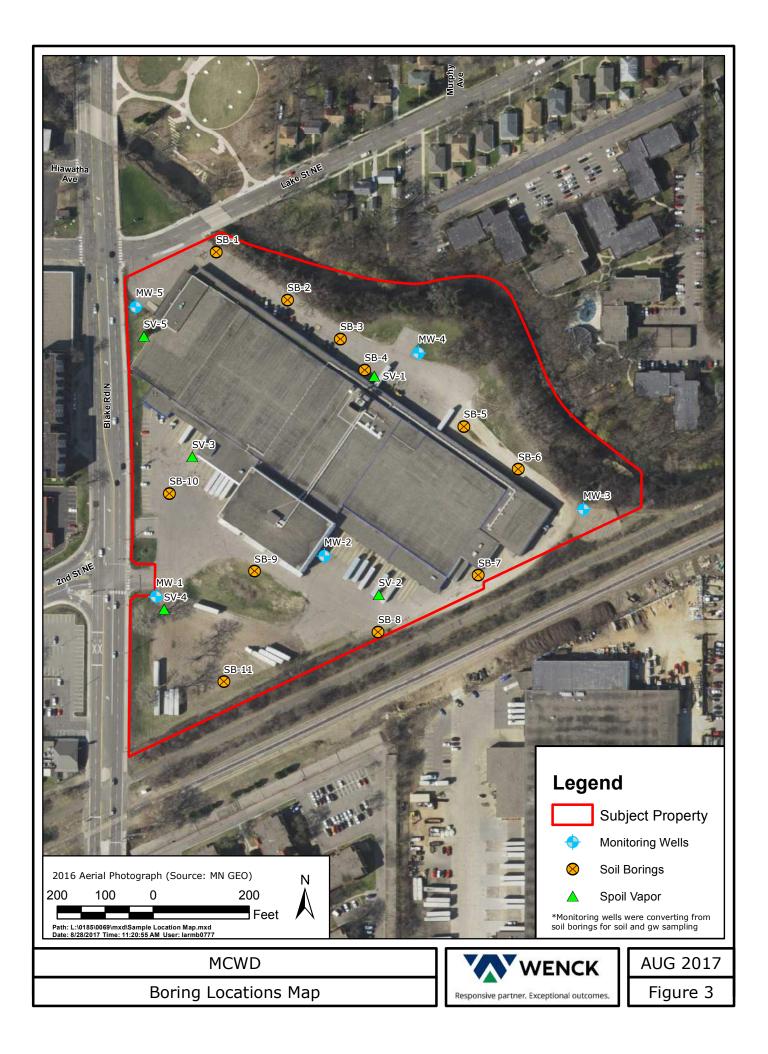
Prepared by:

WENCK Associates, Inc. 1802 Wooddale Drive Woodbury, MN 55125-2937 Phone: 651-294-4580 Fax: 651-228-1969

Table 1 Summary of Historical Groundwater Elevation Data Hopkins Cold Storage 325 North Blake Road, Hopkins, Minnesota Wenck Project No. B0185-0069 October 2017

Well ID No.	MW-1	MW-2	MW-3	MW-4	MW-5
Northing*	150415.50	150517.00	150584.90	150923.70	151019.30
Easting*	499515.50	499862.80	500400.80	500049.10	499471.00
TOC Elevation (ft above MSL)	909.13	907.19	911.27	907.59	913.49
Ground Elevation (ft above MSL) Top of Screen Elevation (ft above	907.0	907.0	909.1	905.5	910.8
MSL)	899.2	897.8	899.8	897.5	901.8
Bottom of Screen Elevation (ft above MSL)	889.2	887.8	889.8	887.5	891.8
Date of Measurement	MW-1	MW-2	MW-3	MW-4	MW-5
08/22/17	898.24	897.79	897.05	897.50	898.37
09/19/17	897.57	897.23	896.73	897.26	896.77

Notes: Horizontal coordinates values shown are the North American Datum of 1988, Hennepin County coordinate system



Soil Boring Logs

	\wedge	V	/E	NCK			LOG OF BOR	ING SB-1				
Respor	nsive pa	irtner. E	xcep	tional outcomes.					(Page	1 o	f 1)	
		Cold St 325 Blak Hopkin hase II Inv roject # B0	e Rd I s, MN /estiga	tion	Date Started Date Completed Contractor Drilling Method Sampling Method	: 8/16/17 : 8/16/17 : Range : Push P : Macro	, Environmental robe	Operator Logged By Checked By	: Too : CJ/ : ML	A		
Depth in Feet	Surf. Elev. 913	USCS	GRAPHIC	Water Levels		DESCR	Boring Depth: 20' Estimated Depth of Fill: IPTION	2.5'		Water Level	Soil Sample Interval	PID Result (PPM)
0-	- 913	Bit		Bituminous surfac	e					1		
-		Fill		Gravel base SAND, well grade moist (Fill)	d, some silt, slight cl	ay, grave	l and organics, dark bro	own/black, slightly	/		0.5-2.5'	0.1
5-	- 908			GRAVELLY SANI moist (Outwash)	D, medium to coarse	grained,	some cobbles, light bro	own, dry to slightly				0.4
-		GW/SP									5-7.5'	0.8
- 10-	- 903									-		0.6
	- 898				0-15' rock in shoe					v		
		GW/SP		GRAVELLY SANI (Outwash)	D, medium to coarse	grained,	some cobbles, light bro	own, wet				1.3
				End of boring @ 2	20'							1.0
	I on estimat	ed from G	oogle	Earth.								

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		Cold Si 325 Blak Hopkin	ke Rd N		Date Started Date Completed Contractor	: 8/16/1 : 8/16/1 : Range		Operator Logged By Checked By	: Todd : CJA : MLH		
		Phase II Inv	vestiga	tion	Drilling Method	: Push F		Sheeked by			
		Project # B	0185-0	077	Sampling Method	: Macro	Core				
Depth in Feet	Surf. Elev.	USCS	GRAPHIC	Water Levels			Boring Depth: 20' Estimated Depth of	Fill: 9'	Water Level	l Sample Interval	PID Result (PPM)
De	912	ns	GR			DESCR	IPTION		Ma	Soil	ЫЧ
0-	912	Bit		Bituminous surfac						1	
		<u> </u>		<u></u>	.е				1		
-	-	Fill		Gravel base SILT, slight clay, s	sand, gravel and org	anics, bla	ck, slightly moist (F	ill)	/	0.5-2.5'	1.0
-		Fill		GRAVELLY SAN in part (Fill)	D, well graded, brow	n, slightly	moist, some lenses	s of black organic silt			0.6
5	907	Fill		SANDY GRAVEL part (Fill)	, very fine to coarse,	brown, s	ightly moist, some	brown and black silt ir	1		0.8
- - 10	902			(Outwash)	D, medium to coarse	grained,	some cobbles, light	t brown, moist			0.4
-	- 502			Becoming wet @	10'					10-12.5'	0.5
-		GW/SP									0.6
- 15	- 897			Becoming coarse	grained @ 15						0.3
-	-			End of boring @ 2	20'						0.4
20-	1		<u>1997</u>						I		
Elevatio	on estima	ated from G	ioogle	Earth.							

	\wedge	V	/E	NCK			LOG OF BO	RING SB-3				
Respor	nsive pa	artner. E	xcept	tional outcomes.					(Page	1 0	f 1)	
		Cold Si 325 Blak Hopkin Phase II Inv Project # Bl	ke Rd I s, MN vestiga	N	Date Started Date Completed Contractor Drilling Method Sampling Method	: 8/16/17 : 8/16/17 : Range : Push P : Macro	, Environmental robe	Operator Logged By Checked By	: Too : CJ/ : ML	4		
Depth in Feet	Surf. Elev. 912	USCS	GRAPHIC	Water Levels		DESCR	Boring Depth: 20' Estimated Depth of F	ill: 5'		Water Level	Soil Sample Interval	PID Result (PPM)
0	- 912	Bit Fill			ce ne organics, slight sa D, well graded, loose			ightly moist (Fill)			0.5-2.5'	1.9
-		Fill Fill Fill		CLAYEY SILT, so	, very fine to coarse,)		r moist, (Fill)				0.9
5	- 907			SAND, fine to me	dium grained, moder	rately den	se, light brown, mois	t (Outwash)				1.0
	- 902	SP										1.3
-											10-12.5'	2.9
- 15-	- 897	SP		Becoming wet @		nd cobble	s, light brown, very n	noist (Outwash)		v		2.7
-				No Recovery @ 1	5-20' rock in shoe							
Elevatio	on estimat	ted from G	oogle							1		

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Respor	nsive pa	rtner. Ex	xcept	tional outcomes.					(Page	1 0	f 1)	
	F	Cold St 325 Blak Hopkins Phase II Inv	e Rd I s, MN	N	Date Started Date Completed Contractor Drilling Method	: 8/16/17 : 8/16/17 : Range : Push P	, Environmental	Operator Logged By Checked By	: Toc : CJ <i>I</i> : MLI	4		
	P	roject # BC)185-0	077	Sampling Method	: Macro	Core			-		
Depth in Feet	Surf. Elev. 912	USCS	GRAPHIC	Water Levels		DESCR	Boring Depth: 20' Estimated Depth of	f Fill: 10'		Water Level	Soil Sample Interval	PID Result (PPM)
	912											
Ŭ		Bit		Bituminous surfac								
-		Fill			D, fine to coarse gra							1.6
-		Fill										2.5
5-	907	Fill		GRAVELLY SAND), fine to coarse gra	ined, brow	n, slightly moist (F	Fill)				
-		Fill		SANDY CLAY, so	me silt, slight organ	ics, dark b	rown, moist (Fill)				5-7.5'	2.6
-	- 902	Fill		GRAVELLY SANI petroleum odor, b	D, fine to coarse gra rown, moist (Fill)	ined, som	e silt in part, slight	to moderate		•		140.5
- 10		GW/SP), coarse grained, s ng petroleum odor fr			et (Outwash)			10-12.5'	216.8
	- 897											2.7
-		SP		SAND, fine to mee	dium grained, light b	prown, wet	(Outwash)				15-17.5'	0.9
-		ог 		End of boring @ 2	0'							0.7
20-										•		
Elevatio	on estimat	ted from G	oogle	Earth.								

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Respo	nsive pa	artner. E	xcept	tional outcomes.					(Page 1 d	of 1)	
		Cold Si 325 Blak Hopkin Phase II Inv Project # Bl	ke Rd N ns, MN vestiga	N	Date Started Date Completed Contractor Drilling Method Sampling Method	: 8/16/17 : 8/16/17 : Range : Push F : Macro	7 Environmental Probe	Operator Logged By Checked By	: Todd : CJA : MLH		
Depth in Feet	Surf. Elev. 911	nscs	GRAPHIC	Water Levels		DESCR	Boring Depth: 20' Estimated Depth of	f Fill: 6.5'	Water Level	Soil Sample Interval	PID Result (PPM)
0-	- 911 - -	Fill		CLAYEY SAND, s	and and silt, brown, some silt and organic	cs, black,		ome black organic silf			0.6
	906	Fill		in part (Fill)	, nne to coarse gra	ined, brov	n, signay molet, s			2.5-5'	0.8
- 2 - 2017 1:0185/0069 325 Blake Investigation Proposal and Grant/Phase II Investigation/Phase II Field Work(Cold Storage Quicklog)SB-5.bot - 10 - 10 - 10 - 10 - 10 - 10 - 10		Fill			D, medium grained,			Deposit)			0.8
	- - - - 901			SANDY GRAVEL Becoming wet @	-	me cobble	es, light brown, slig	htly moist (Outwash)		7.5-10'	1.2
gation/Phase II Fie											1.4
ant/Phase II Investi 12-	- 896	GW/SP									0.7
n Proposal and Gr											0.9
25 Blake Investigatio	-			End of boring @ 2	20'						0.9
20 -											
Elevati	on estima	L ited from G	Google	Earth.							



Respo	nsive pa	artner. Ex	xcept	tional outcomes.					(Page 1	of	1)	
		Cold St 325 Blak Hopkins	e Rd I s, MN	N	Date Started Date Completed Contractor	-	Environmental	Operator Logged By Checked By	: Todd : CJA : MLH			
		Phase II Inv	-		Drilling Method Sampling Method	: Push P : Macro						
Depth in Feet	Surf.	Project # BC	GRAPHIC	Water Levels			Boring Depth: 20' Estimated Depth of	f Fill: 10'		Water Level	Sample Interval	Result (PPM)
ept	Elev. 912	nscs	RAI			DESCR	IPTION		:	/ate	Soil S	PIDF
		>	G			DECON			:	<	Ň	Ч
0-	912	Fill		GRAVEL, some sa	and and silt, brown,	dry (Fill)						
	-	Fill		CLAYEY SAND, s	ome silt and organio	cs, dark br	own/black, moist (Fill)				1.2
-		Fill		SILT, slight sand a	and clay, soft, browr	n, moist (F	ill)					1.2
	007	Fill		GRAVELLY SAND), fine to coarse gra	ined, brow	n, slightly moist (F	ill)				1.2
- 5	- 907	Fill		GRAVELLY SANE sand and clay in p	D, fine to coarse gra art (Fill)	ined, brow	n, slightly moist, s	ome black silt with			5-7.5'	1.5
		Fill		SILT, some sand, sand in part (Fill)	clay and organics, o	dark browi	n/black, moist, som	ne brown gravelly		•		1.3
- 10	- 902	GW/SP		SANDY GRAVEL,	coarse grained, so	me cobble	s, light brown, wet	(Outwash)			10-12.5'	2.1
- 15-	- 897											1.8
-	-	GW/SP		GRAVELLY SANE), fine to coarse gra	ined, sligh	t cobbles, light bro	wn, wet (Outwash)				1.0
. .	-	GW		GRAVEL, some sate of boring @ 2	and and cobbles, lig	ht brown,	wet (Outwash)					1.1
20-	1											
Elevatio	u on estima	L ted from G	oogle	Earth.								

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Respo	nsive p	artner. E	xcept	tional outcomes.					(Page 1 o	of 1)	
		Cold S 325 Blak Hopkin Phase II In	ke Rd N is, MN	N	Date Started Date Completed Contractor Drilling Method	: 8/16/1 : 8/16/1 : Range : Push F	7 Environmental	Operator Logged By Checked By	: Todd : CJA : MLH		
		Project # B	-		Sampling Method	: Macro					
				Water Levels	F3					1	
Depth in Feet	Surf. Elev.	S	GRAPHIC	Water Levels			Boring Depth: 20' Estimated Depth of	' Fill: 0.5'	Water Level	Sample Interval	Result (PPM)
ept	912	nscs	RA			DESCR	IPTION		/ate	Soil 3	PID F
			G						5	٥ ٥	_ <u> </u>
0-	+ 912	Bit		Bituminous surfac	<u>م</u>					1	<u> </u>
		— F W		Gravel base					/		
	-	OL			some clay, soft, blac	k, moist (Swamp Deposit)		/		0.7
	-			CLAYEY SILT SC	oft, brown, moist (Ou	twash)					
- 5-	907	ML								2.5-5'	1.5
og 5 .	- 307	SP		SAND, fine to me moist (Outwash)	dium grained, coarse	ening dow	nward, moderately	dense, light brown,			1.4
- duickie	-			GRAVELLY SAN	D, fine to coarse gra	ined, sligt	t cobbles, light bro	wn, slightly to very			
orage				moist (Outwash)	, j	, 0					
	902										2.1
		GW/SP		Becoming wet @	12'				T	10-12.5'	3.0
ase il invesuga	-										2.7
				SAND, fine to ver	y fine grained, light t	prown, we	t (Outwash)				
- 15 – 12 – 15 – 15 – 15 – 15 – 15 – 15 –	+ 897 - -	SP									1.2
				End of boring @ 2	20'						1.4
20-	1								I		<u>.</u>
Elevati	I on estima	ated from G	Google	Earth.							
>											

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Responsive partner. Exceptional outcomes.	

	Respor	nsive p	artner. E	xcep	tional outcomes.					(Page	1 of	f 1)	
-			Cold S 325 Blał Hopkin Phase II In Project # B	ke Rd I ns, MN vestiga	Nation	Date Started Date Completed Contractor Drilling Method Sampling Method	: 8/16/1 : 8/16/1 : Range : Push F : Macro	7 Environmental Probe	Operator Logged By Checked By	: Too : CJ, : ML	4		
	Depth in Feet	Surf. Elev. 914	nscs	GRAPHIC	Water Levels		DESCR	Boring Depth: 20' Estimated Depth of	f Fill: 2'		Water Level	Soil Sample Interval	PID Result (PPM)
-	-0	- 914	Bit Fill Fill			ace some organics, black, moist (Fill) , some clay, soft, black, moist (Swamp Deposit)						1-2'	0.5
			OL SM			ne clay, soft, brown,							0.9
08-30-2017 T: 018510069 325 Blake Investigation Proposal and Grant/Phase II Investigation/Phase II Field Work/Cold Storage Quicklog/SB-8.bor	5-	- 909			GRAVEL, some s	and, slight cobbles,	light brow	n, dry to slightly mo	oist (Outwash)				0.5
Id Work\Cold Storag	- - 10-	904	GW										0.5
gation\Phase II Fie	-	-			GRAVELLY SAN	D, medium grained,	slight cob	bles, light brown, rr	noist (Outwash)				1.6
ant\Phase II Investi	- - 15-	- 899			Becoming wet @	13'							0.6
on Proposal and Gra	-		GW/SP										0.8
5 Blake Investigatic	- - 20-	-			End of boring @ 2	20'							0.9
5\0069 32	20-											-	
08-30-2017 T:\018	Elevatio	on estima	Ited from G	Google	Earth.								

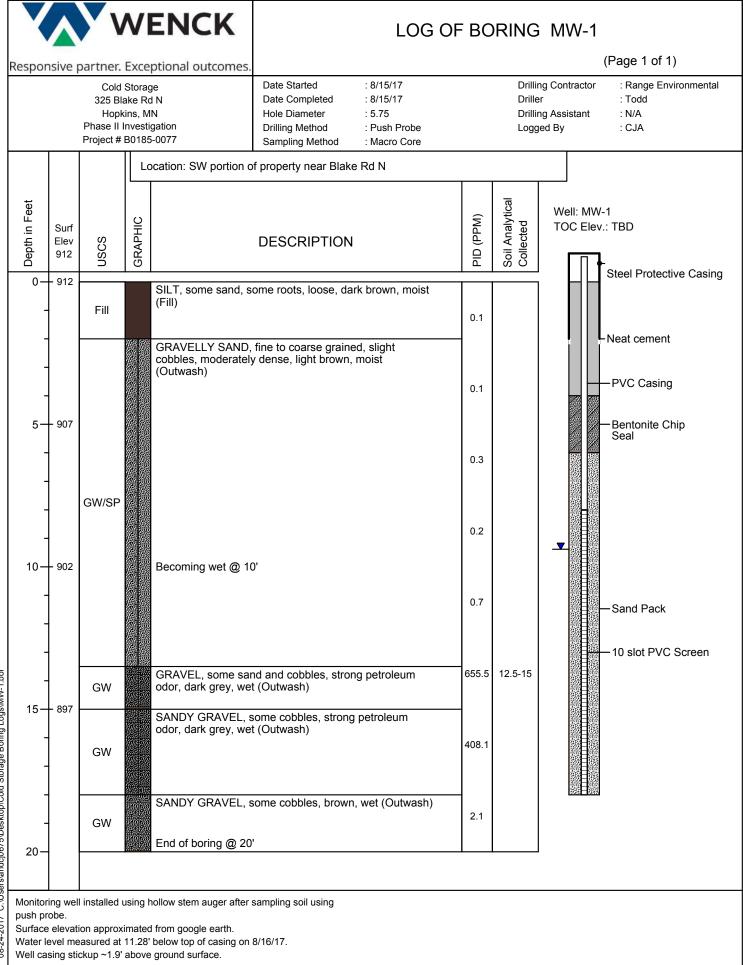
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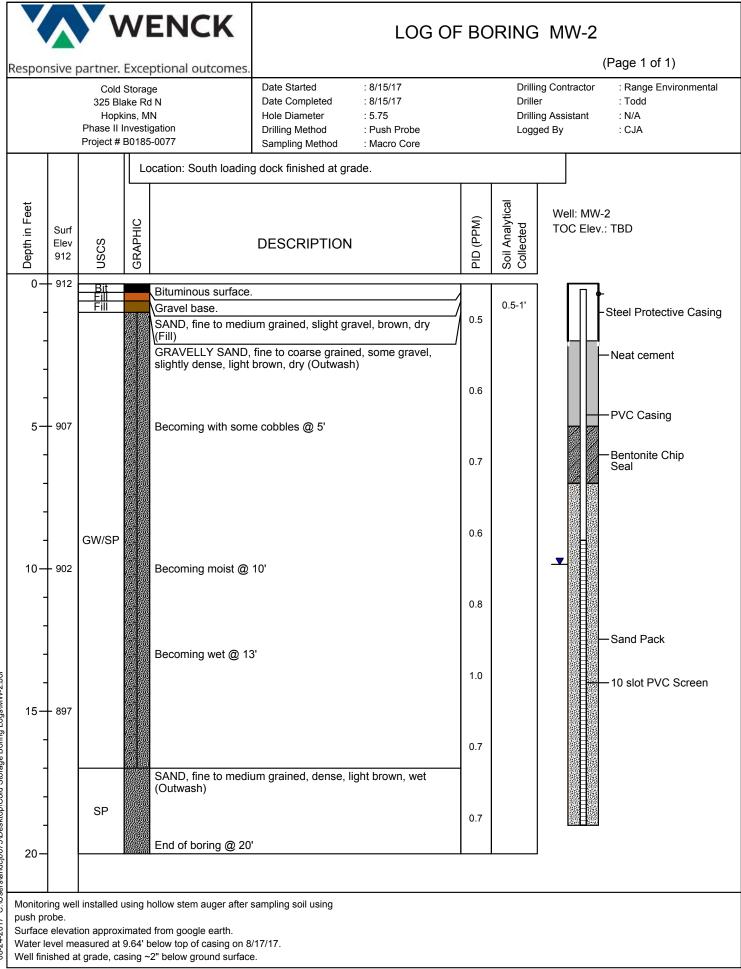
Responsive partner. Excep	otional outcomes.					(Page 1 o	of 1)	
Cold Storag 325 Blake Rd Hopkins, M Phase II Investig	l N N gation	Date Started Date Completed Contractor Drilling Method	: Push P	, Environmental robe	Operator Logged By Checked By	: Dave : CJA : MLH		
Project # B0185-	Water Levels	Sampling Method	: Macro	Boring Depth: 20' Estimated Depth of	Fill: No Fill Observed	Water Level	Soil Sample Interval	PID Result (PPM)
0-912 ML SP	C (Topsoil)	nics, trace very fine s rained, light brown, o D, medium to coarse	dry (Outwa	ash)			0-2.5'	0.0
5-907								0.0
								0.0
10-902	Becoming wet @	10'					,	0.0
GW/SP								0.1
								0.3
								0.4
15-897 15-897 20-SC Elevation estimated from Google		stiff, light brown, wet	(Outwash)				0.4
	End of boring @	20'				/		
Elevation estimated from Google	e Earth.							

	X		V	VE	NCK			LOG OF BO	RING SB-10				
Re	espor	nsive p	artner. E	xcept	tional outcomes.					(Page	1 o	f 1)	
			Cold S 325 Blal Hopkir Phase II In Project # B	ke Rd N ns, MN vestiga	Nation	Date Started Date Completed Contractor Drilling Method Sampling Method	: 8/17/1 : 8/17/1 : Range : Push F : Macro	7 Environmental Probe	Operator Logged By Checked By	: Da : CJ <i>i</i> : ML	4		
	Depth in Feet	Surf. Elev. 912	NSCS	GRAPHIC	Water Levels		DESCR	Boring Depth: 20' Estimated Depth of I	Fill: 0.5'		Water Level	Soil Sample Interval	PID Result (PPM)
	-0 - -	912	Bit		Bituminous surfac Gravel base GRAVELLY SAN (Outwash)	ce D, medium to coarse	grained,	some cobbles, light	brown, dry			0.5-2.5'	0.4
	-	907	GW/SP										0.5
		- 907	SP		SAND, fine to me (Outwash)	dium grained, slight s	gravel, m	oderately dense, ligt	nt brown, moist				1.5
	- - 10—	902			GRAVELLY SAN	D, fine to coarse grai	ned, som	e cobbles, light brov	vn, moist (Outwash)				1.1
	-				Becoming wet @	12'					▼		1.6
s\SB-10.boi	- - 15—	- 897	GW/SP										0.8
Storage Boring Log	-												1.0
)675\Desktop\Cold	- - 20—				End of boring @ 2	20'							0.6
ers\andcjC	20 -						_			_	_	_	
08-24-2017 C:\Users\andcj0675\Desktop\Cold Storage Boring Logs\SB-10.bor	Elevatio	on estima	ated from G	Google	Earth.								

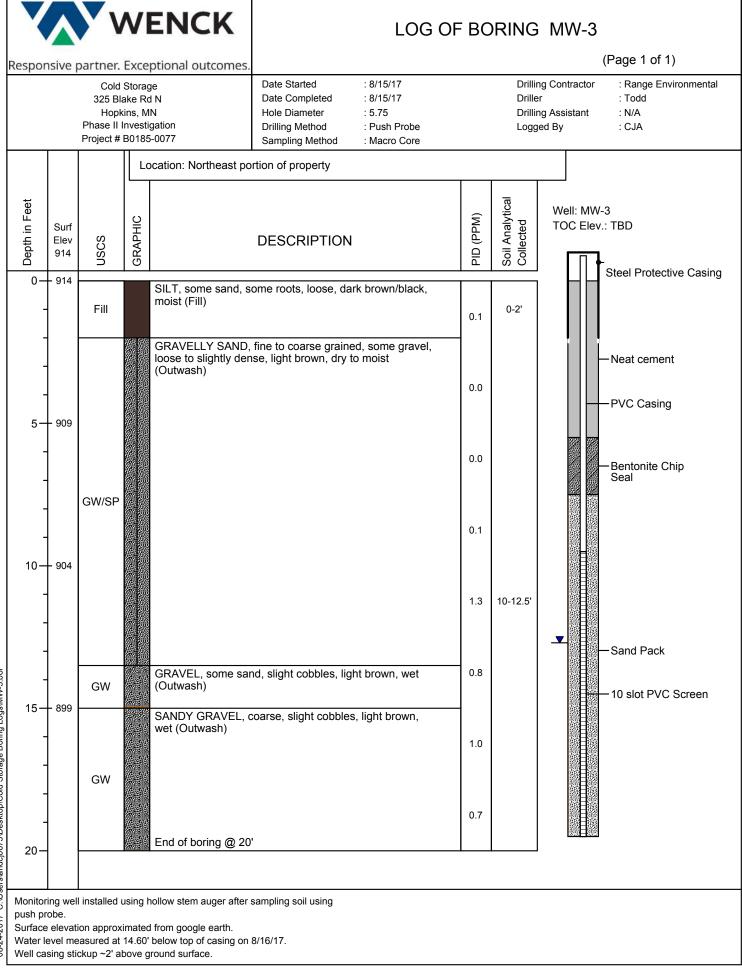


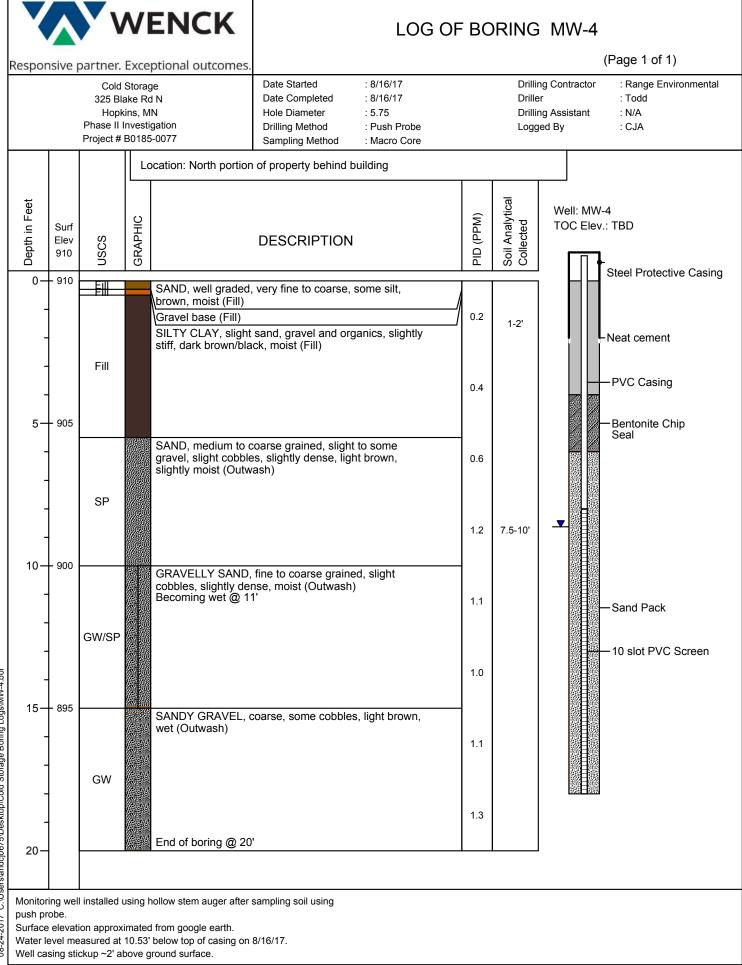
Respon	nsive pa	artner. E	xcep	tional outcomes.					(Page	1 of	1)	
	I	Cold Si 325 Blak Hopkin Phase II Inv	ke Rd I s, MN	N	Date Started Date Completed Contractor Drilling Method	: 8/17/1 : 8/17/1 : Range : Push F	7 Environmental	Operator Logged By Checked By	: Da : CJ/ : ML	4		
	F	Project # B	0185-0	077	Sampling Method	: Macro	Core					
Depth in Feet	Surf. Elev.	S	GRAPHIC	Water Levels			Boring Depth: 20' Estimated Depth of	f Fill: ~1'		Water Level	Sample Interval	Result (PPM)
Dept	912	nscs	GRA			DESCR	RIPTION			Wate	Soil 3	PID I
0-	912	Fill		SAND, well grade (Possible Fill)	ed very fine to coarse	e grained,	slight silt and clay,	brown, moist				
				GRAVELLY SAN	D, very fine to mediu twash)	ım graine	d, some cobbles, lig	ght brown, dry to			1-2'	0.2
-	907											0.5
		GW/SP										1.5
	902											0.8
												1.2
	- 897				, coarse grained, sli	ght cobble	es, light brown, wet	(Outwash)		•		0.9
-		GW										1.6
				End of boring @ 2	20'							1.1
20-]									•		
15- 	I on estima	L ated from G	loogle	Earth.								

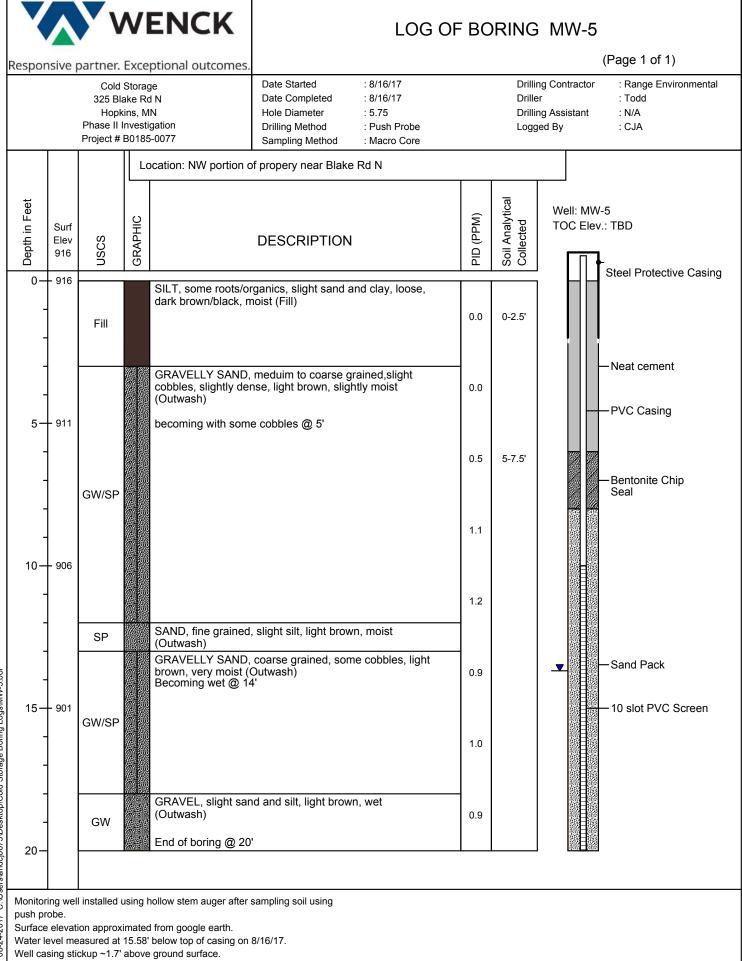




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Responsive partner. Exceptional outcomes.

To: Michael Hayman, Project Manager, Minnehaha Creek Watershed District

From: Chris Meehan, Wenck Associates, Inc. Mark Schroeher, Wenck Associates, Inc. Erik Megow, Wenck Associates, Inc.

Date: January 7, 2016

Subject: Storm Water Treatment Concepts at 325 Blake Road

Minnehaha Creek Watershed District (MCWD) is currently working with a development team to evaluate options for site development at 325 Blake Road in Hopkins, MN. Wenck was tasked to have a better understanding of how much, where and to what extents the storm water will be routed to the site.

Verify Storm Water Volumes

The two major diversion inflows planned for the 325 Blake parcel were the Lake Street Diversion Project –(MCES) and the Powell Road Diversion Project (MCWD). The Powell Road Diversion Project has since been constructed and the Lake Street Diversion is entering final design. As these projects progressed design modifications were required which resulted in a change to the stormwater volumes which would be diverted to 325 Blake. As a result there was a need to determine the current volumes and the necessary footprint for a stormwater BMP on the site.

A HydroCAD model was developed with the updated attributes of the each of the projects to determine the runoff volume that can be directed to the 325 Blake Road stormwater BMP (Table 1). The volumes calculated in the analysis were based on the 1.0 and 1.25-inch 24-hour rainfall events. These two events represent water quality depths used for stormwater BMP sizing.

Storm Event	Runo	off Volume (ac-f	t)	BMP Footprint
Storm Event	From Powell	From Lake St.	Total	(ac)*
1.0-inch	3.93	1.92	5.85	1.95
1.25-inch	6.23	2.73	8.96	2.99

Table 1 – Runoff Volumes and BMP Footprint Size

*The BMP footprint is based on an assumed depth of 3 ft.

Site Design Refinement

Based on the two rainfall events mentioned above, the footprint of the filtration basins were calculated and placed graphically in Figure 1. The footprints shown in Figure 1 are the overall impact area of each infiltration basin based on side slopes of 4 horizontal to 1 vertical and tie into the existing surface. The BMP depth was assumed as 3 feet from elevation 898.0 to 901.0. These elevations were determined by understanding the approximate groundwater depth (bottom of basin) and the two diversion structure inverts (overflow elevation). The existing site is generally flat with the exception of the

Michael Hayman MCWD January 7, 2016

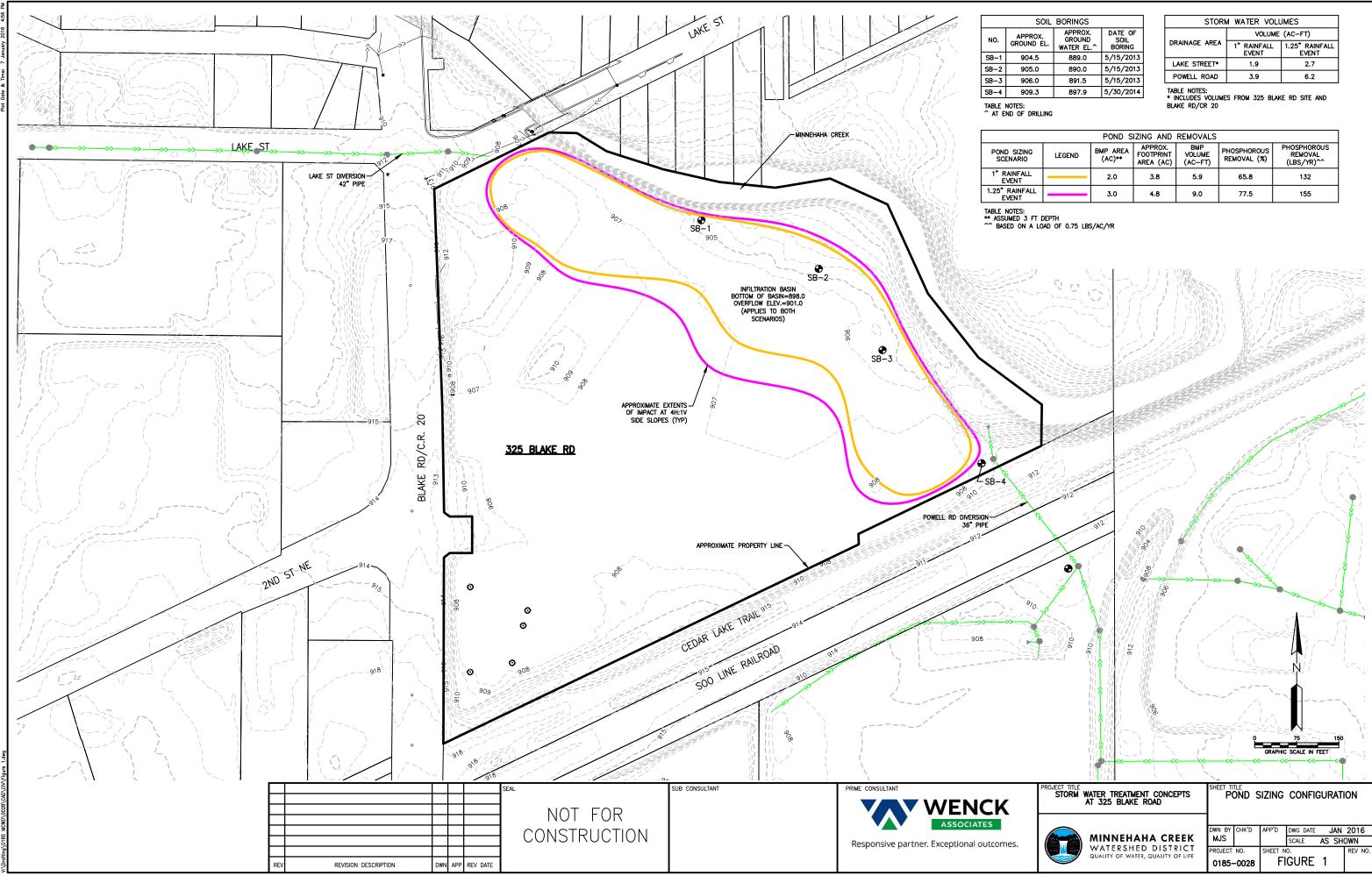


northeastern edge of the site going down to the creek, indicating the exact shape and location of the proposed filtration basin will have minimal effect on the earthwork for the site.

Soil borings from both May of 2013 and May 2014 were reviewed to understand the existing groundwater in the area and to determine the filtration basin bottom elevation. A basin bottom elevation of 898.0 was determined based on three feet of separation from the assumed ground water level. The basin overflow elevation is based on the Lake Street and Powell Road Diversions. Lake Street has an overflow elevation of 902.31 at the diversion structure before water would backup into the system. Powell Road has an overflow elevation of 901.06 at the diversion structure before backing up into the system and thus dictates the overflow elevation for the proposed basin.

Construction Cost Estimate

Both an overall component cost estimate and detailed cost estimate for the storm water treatment concepts were developed. The component cost used a combination of the 2013 Feasibility Study estimates and the 2015 325 Blake Demolition report. Assumptions for the estimates are included in each document. The storm water treatment concept is estimated in the range of \$1,865,550 to \$2,238,660. These costs are higher than the original 2013 feasibility study estimate largely due to the assumed common excavation quantity. The original estimate assumed a common excavation quantity of 34,000 cubic yards based on calculated storm water volumes at the time. The current common excavation quantity is estimated at 62,500 cubic yards and is based on the removing soil material between the bottom of the proposed basin and the existing surface. The common excavation unit cost currently assumes all material will be hauled off site; however, this unit cost could be reduced if some soil material remains on site.



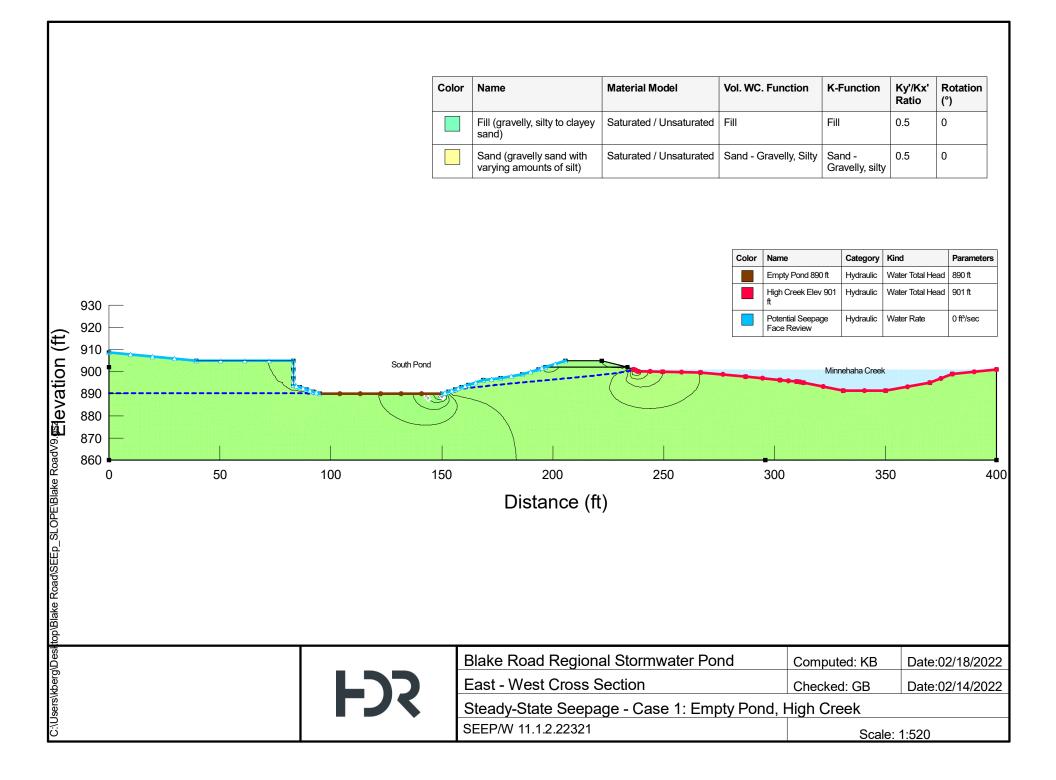
SOIL	BORINGS	
APPROX. ROUND EL.	APPROX. GROUND WATER EL.^	DATE OF SOIL BORING
904.5	889.0	5/15/2013
905.0	890.0	5/15/2013
906.0	891.5	5/15/2013
909.3	897.9	5/30/2014

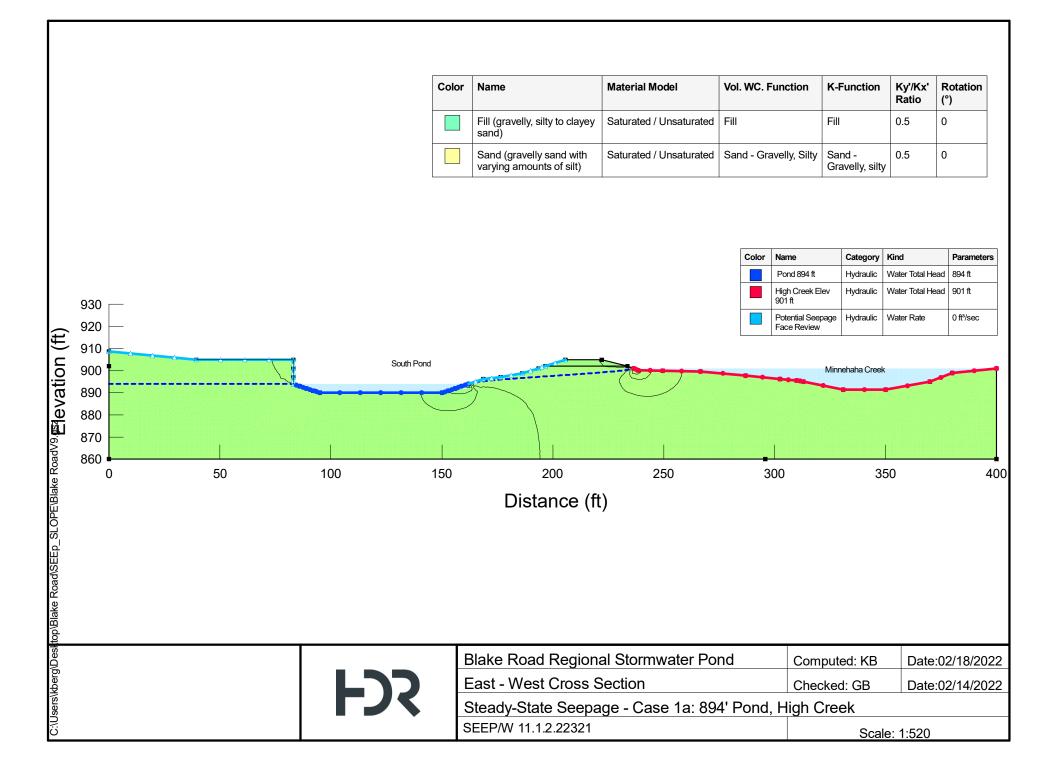
STORM WATER VOLUMES										
VOLUME	(AC-FT)									
1" RAINFALL EVENT	1.25" RAINFALL EVENT									
1.9	2.7									
3.9	6.2									
	VOLUME 1" RAINFALL EVENT 1.9									

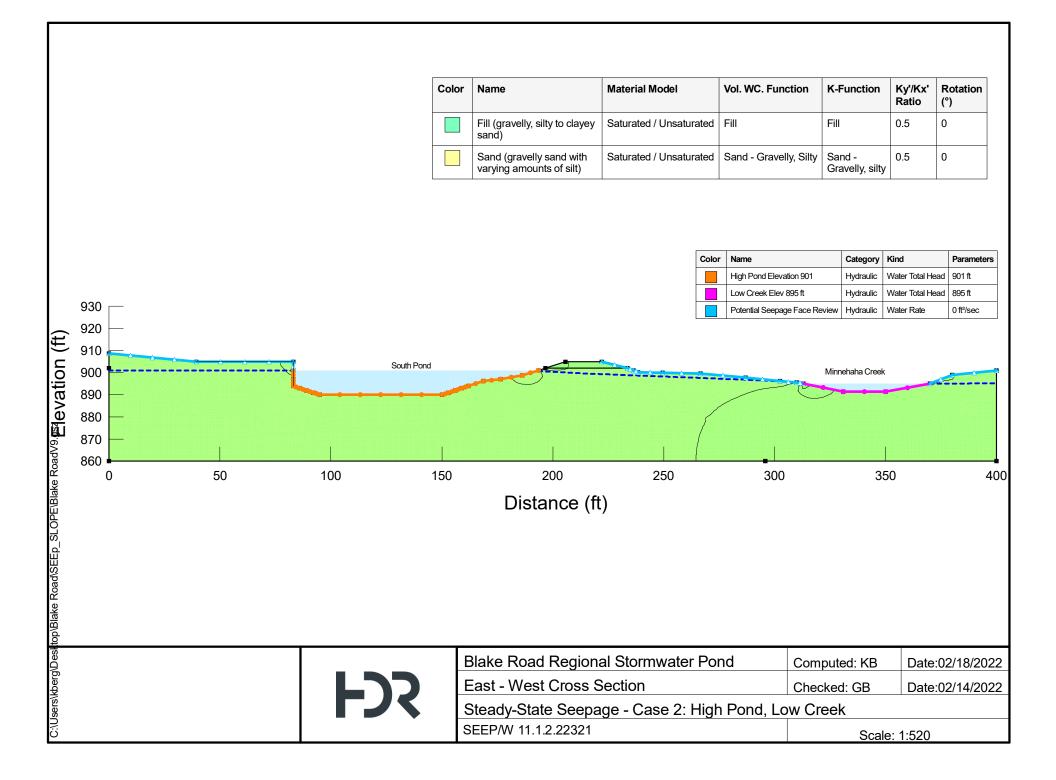
	POND SIZING AND REMOVALS													
IZING RIO	LEGEND	BMP AREA (AC)**	APPROX. FOOTPRINT AREA (AC)	BMP VOLUME (AC-FT)	PHOSPHOROUS REMOVAL (%)	PHOSPHOROUS REMOVAL (LBS/YR)^^								
IFALL NT		2.0	3.8	5.9	65.8	132								
INFALL IT		3.0	4.8	9.0	77.5	155								

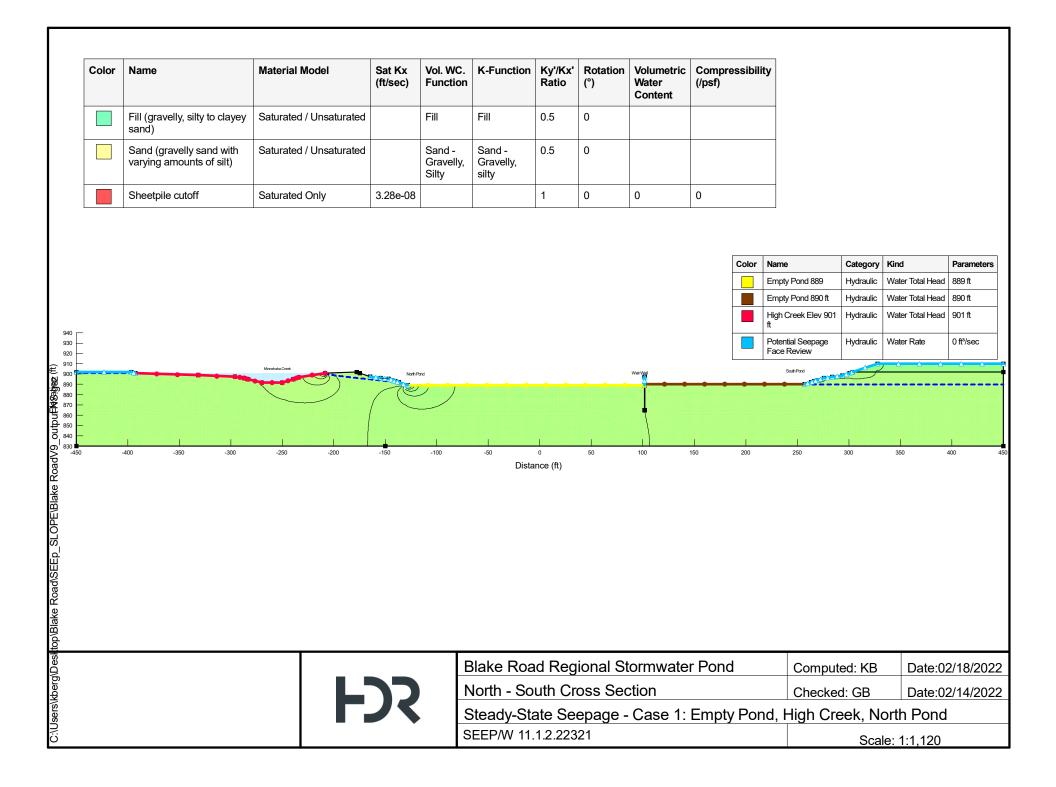
Attachment B

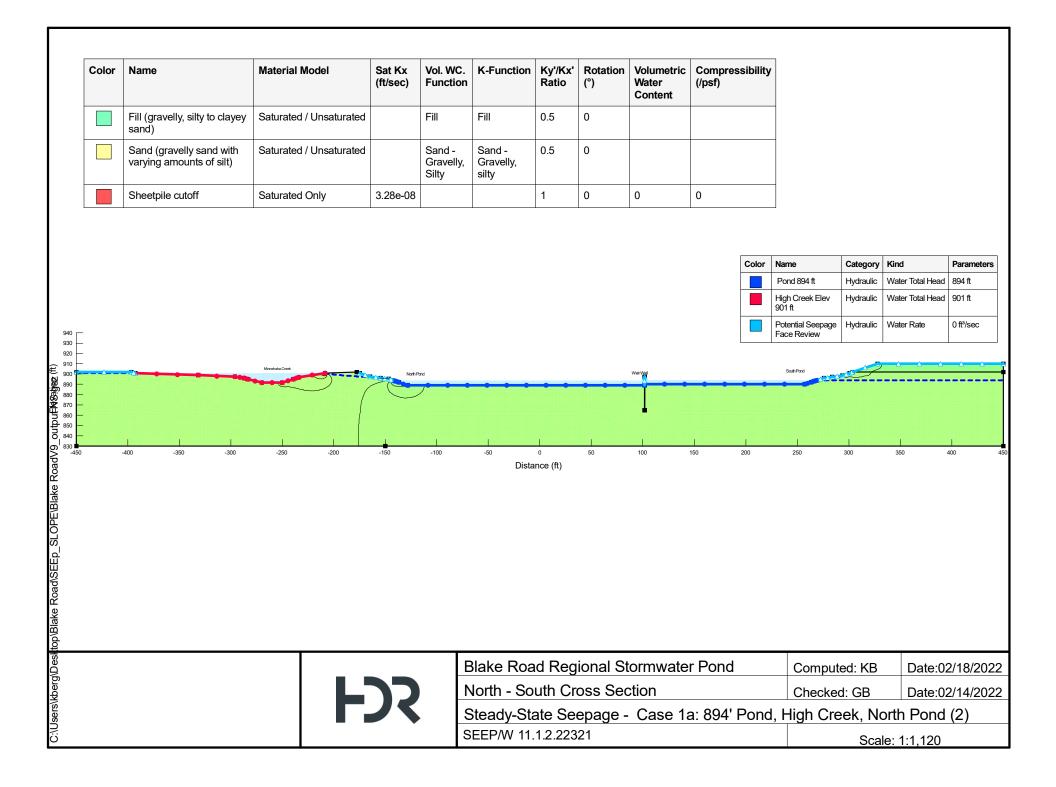
SEEP/W Seepage Analysis Results

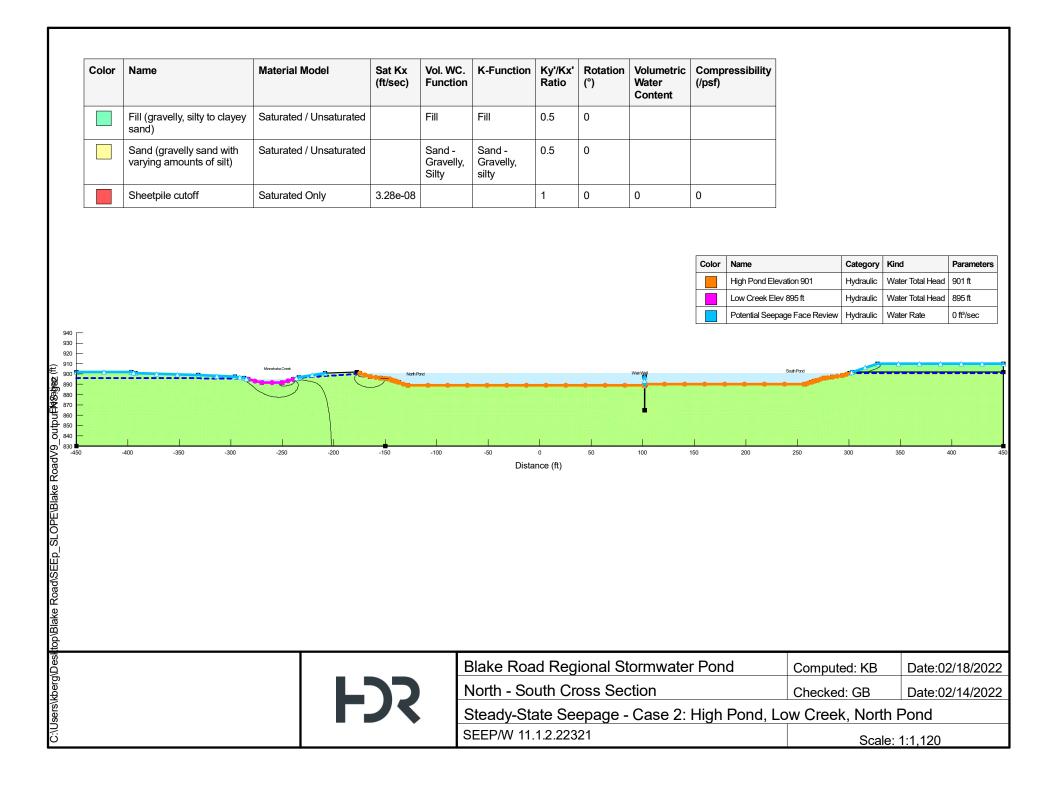


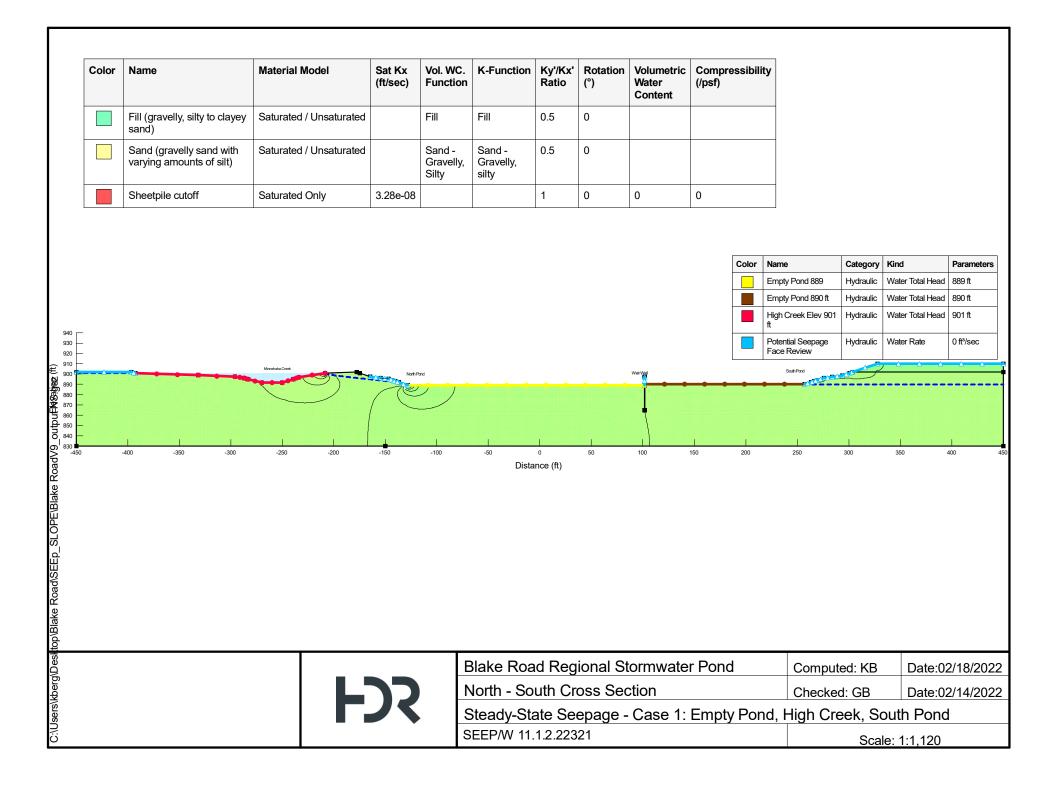










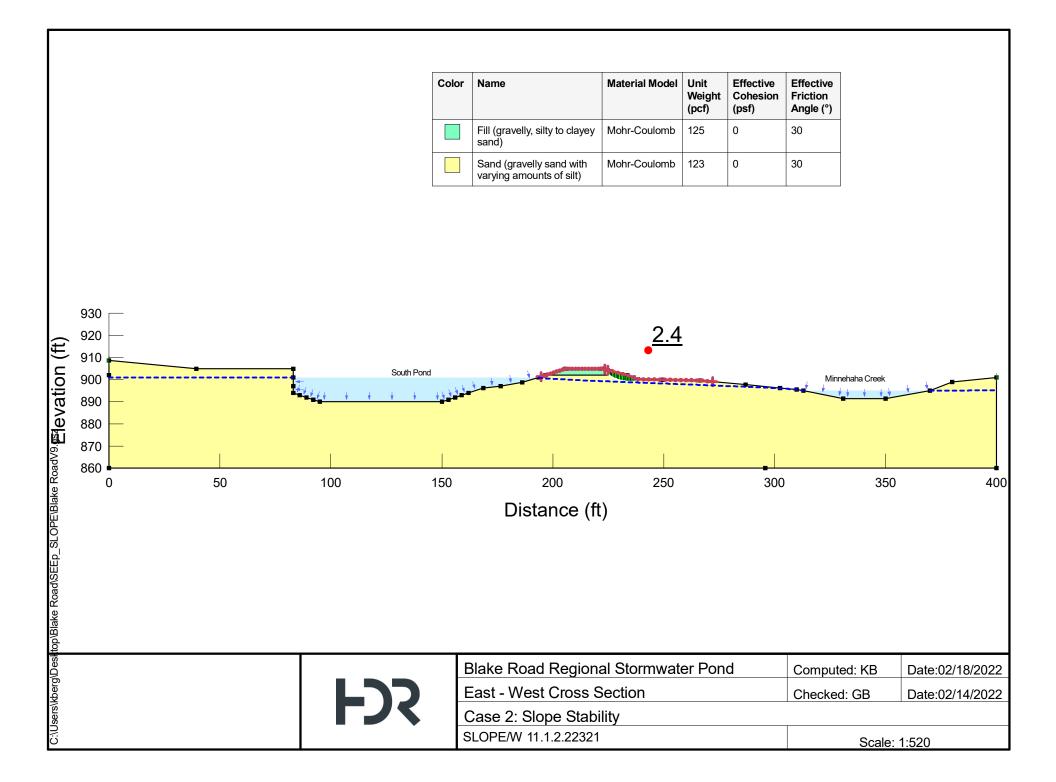


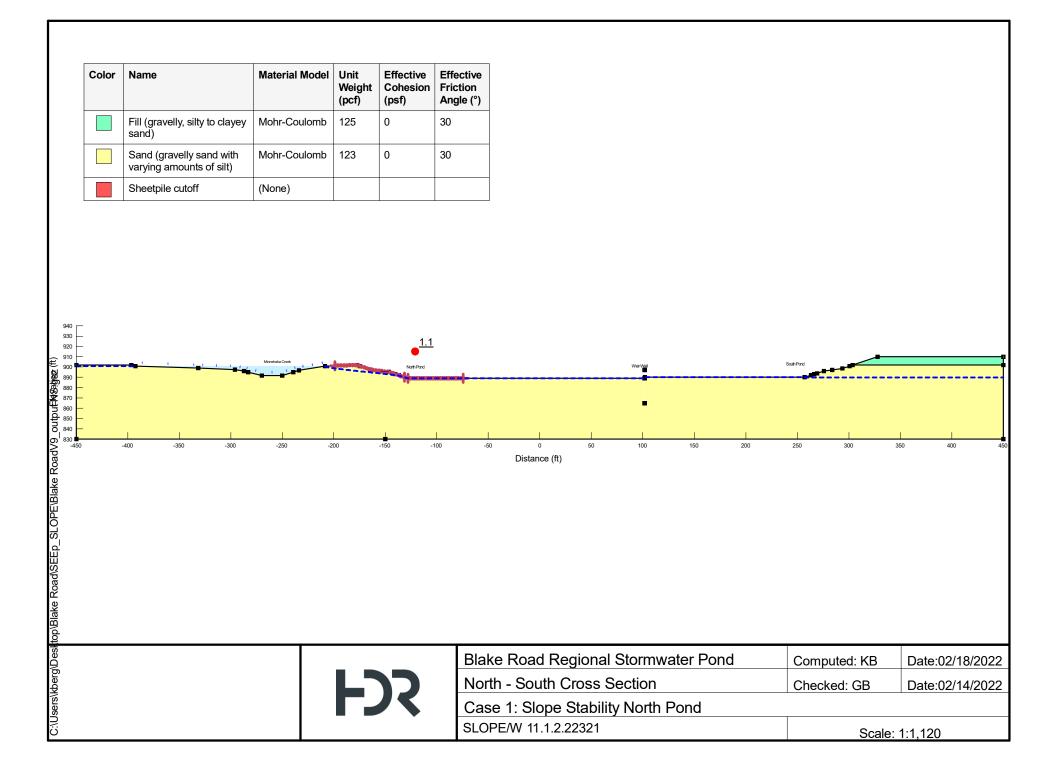
Attachment C

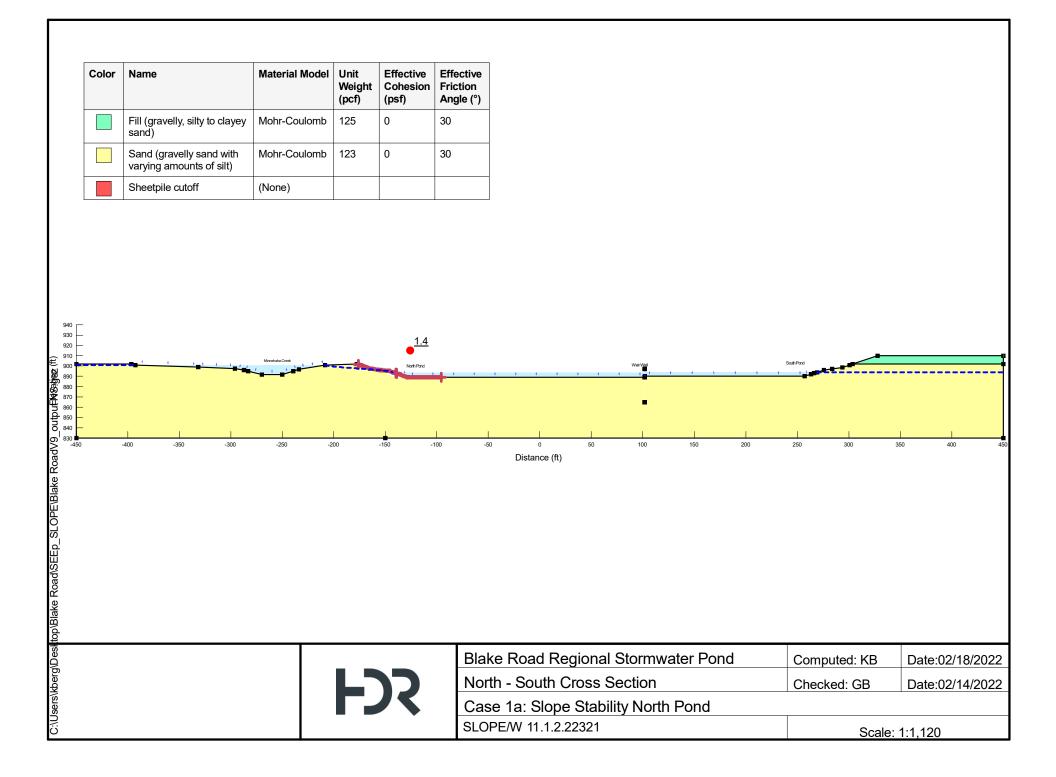
SLOPE/W Slope Stability Analysis Results

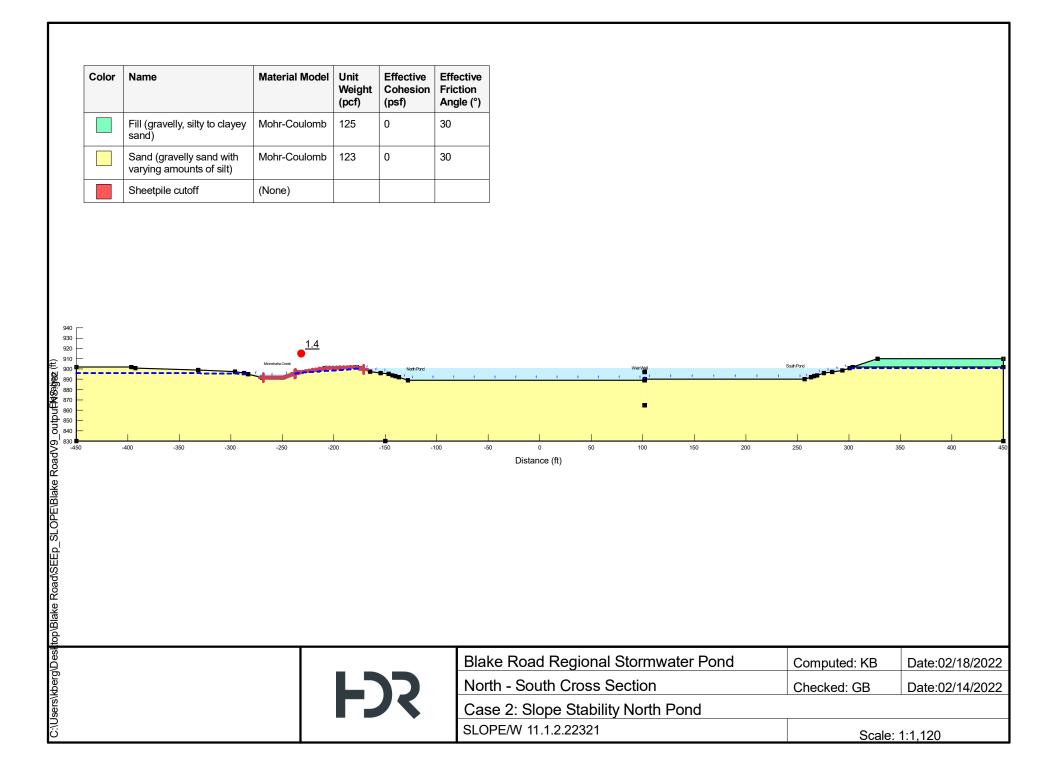
evation (ft)	930 920 910 900 890 880		South F	Color	Fill (gravelly, silty to clayey sand) Sand (gravelly sand with varying amounts of silt)	Material Model Mohr-Coulomb Mohr-Coulomb	Unit Weight (pcf) 125 123	Effective Cohesion (psf) 0 0	Effective Friction Angle (°) 30 30	ehaha Creek	· · · · · · · ·	* *
koadV9.	870 -											
Blake RoadV9.	870	50	100	150	200 Distance (ft	250		 300		350		400
top\Blake Road\SEEp_SLOPE\Blake RoadV9.Eaevation (ft)	870 -	50	100	150	²⁰⁰ Distance (ft			 300		350		400
g\Des <mark>it</mark> top\Blake Road\SEEp_SLOPE\Blake RoadV9. E	870 -	50		E)	er Pon		Compute		Date:02/18	
\\therg\Des <mark>it</mark> op\Blake Road\SEEp_SLOPE\Blake RoadV9. E	870 -	50		E	Distance (ft) al Stormwate	er Pon			ed: KB	Date:02/14	3/2022
C:\Users\kberg\Des <mark>it</mark> top\Blake Road\SEEp_SLOPE\Blake RoadV9. E	870 -	50	100 FDR	E E	Distance (ft Blake Road Regiona) al Stormwate Section lity	er Pon		Compute	ed: KB		3/2022

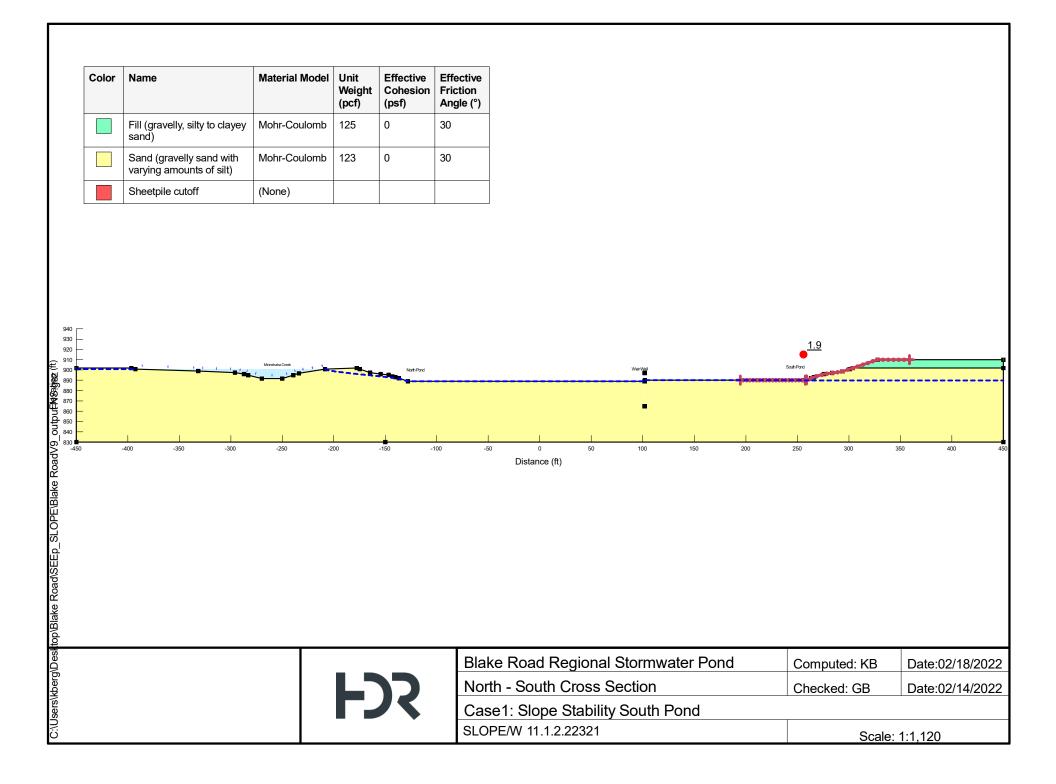
sktop\Blake Road\SEEp_SLOPE\Blake RoadV9.	930 920 910 900 890 880 870 860 0	50	South Pond	150	Fill (gravelly, silty to clayey sand) Sand (gravelly sand with varying amounts of silt) 4 200 Distance (ft		Unit Weight (pcf) 125 123	Effective Cohesion (psf) 0 0	<u><u>v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u></u>	aha Creek		400
C:\Users\kberg\Desktop\Blake Road					Blake Road Regiona	al Stormwate	er Pon	d	Computed	l: KB	Date:02/18/2	2022
s\kberç			FS		East - West Cross S				Checked:	GB	Date:02/14/2	2022
User					Case1a: Slope Stab	ility						
ú.				5	SLOPE/W 11.1.2.22321					Scale: 1	1:520	













Appendix E

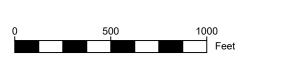
Cost Estimate

			1	1		-		
Minnehaha Creek Wa	atershed District							
Blake Road Developn					Public Realm			
Opinion of Probable	Costs				Stormwater	_		
18-Feb-22								
					REDEVELOPMEN			
		OPINION OF	PROBAB	LE CONSTRUC	TION COSTS (OPC BASELINE OP		ETAILED/60% DE	SIGN PHASE
						ECT CO	DST	
AREA	ITEM	SUB-ITEM	UNITS	QUANTITY	UNIT PRICE		COST	COMMENTS
OVERALL	General Conditions	Mobilization	%	5%	of construction	\$	171,244.46	
		Erosion/Sediment Control	%			\$	102,746.68	
	Site Preparation	Clearing and Grubbing Dewatering	AC LS	1.2	\$10,663.95 \$80,000.00			Vegetated areas only Pond excavated in the wet, dewatering for outlet structure
		Scarify site for seeding/planting	MSF	348	\$7.40	\$	2,575	
	Demolition/Removals	Remove SD MH Remove SD Pipe	EA LF	2	\$870.00 \$18.50		1,740 2,128	
		Abandon and Grout SD Pipe	LF	2	\$18.50		18,000	Includes removal of headwall and restoration of bank
		Remove Trees	EA	20	\$600.00		12,000	12"+ caliper, smaller trees removed via clearing/grubbing
MAIN PARCEL	Earthwork	Pond Excavation Haul and dispose	CY CY	37,000 44,400	\$12.55 \$ 6.29		464,350 279,276	Assumes 20% bulking, 10 mile hauling no disposal fee
		Finish Grading	SY	18,000			4,680	
	Stormwater	Pipe Connections Baffle Inlets	EA EA	2	\$ 1,800.00 \$ 30,000.00		3,600 60,000	Connect to Powell and Lake Diversions Costs from Technical report estimates
		36" RCP	LF	105			14,727	Powell Diversion - Includes Excavation
		42" RCP 1.5'Hx4'W RCB	LF LF	532 30			76,379 9,000	Lake Diversion - includes Excavation Includes excavation and backfill
		4'Hx6'W RCB	LF	40			24,000	Includes excavation and backfill
		Manhole	EA	6			43,572	
		Pipe End Section RCB Culvert End Section	EA EA	2			4,400 12,000	
		HPTRM	SY	53	\$ 45.00	\$	2,400	60'x8'
	Outlet Structure	Riprap Structural Excavation	CY CY	103 120			7,717 1,380	Filter material incidental
		Reinforced Concrete	CY		\$ 1,000.00		1,380	
		Grating Miccellancour Structures	SF	80			11,200	
		Miscellaneous Structures Stoplogs	LS LS	1			6,000 12,000	Hinging, handles, locks ,etc with lifter
		Guardrail	LF	94	\$ 120.00	\$	11,280	
		H-Piles Interpretive Signage	LF EA	570 1			25,650 2,000	W10x49
	Weir Wall	Sheetpile	SF	3,840	\$ 48.00	\$	184,320	Conservative estimate, PZ-22 assumed, 160'x24' (8' exposed)
		Concrete Cap Connections to Outlet and Cascade Weir	CY EA	120			96,000	Cap along 120 LF of wall
	Pedestrian Bridge	Wood Pedestrian Bridge	SF	2 1,200			8,000 204,000	Spans creek to connect to nature play
		Concrete Base Slab	CY	30				15 CY each side
	Site Finishing/Surfacing	H-Piles Pond Seeding	LF AC	300 0.5			13,500 1,063	W10x49 Hydroseeding with mulch and fertilizer
-		Non-Pond Seeding	AC		\$ 1,287.39		5,150	Hydroseeding with mulch and fertilizer
		Tree Planting Paved Trails	EA LF	40 1,200	\$ 500.00 \$ 70.00		20,000 84,000	Assume 10' wide
		Signage/Wayfinding/Interp	LS		\$ 100,000.00		100,000	
	Trailboad	Site Lighting	LS SF	1 1,502	\$ 80,000.00 \$ 25.00		80,000	
	Taineau	Permeable Pavers Flush Curb	LF	250			37,550 10,000	
		Planter Seatwall	LF	137			34,250	
		Limestone Seatwall (Straight Segments) Bench	LF EA	110 3			38,500 7,500	
		Trailhead Kiosk	EA	2		\$	36,000	
		Bike Rack Trash Receptable	EA EA	3			1,950 1,000	
		Drinking Fountain (with utilities)	EA	1			10,000	
		Interpretive Signage Planting Soils (18" depth)	LS CY	1 41			8,000 1,640	
		Trees	EA				3,600	
		Irrigation	LS	1			5,000	
	The Landing	Shrubs Bunker Sand	SF CY	741 288			4,446 11,520	
		Glacial Boulders	EA	13			13,000	
		Crushed Limestone (4" depth) Stone Edger	SF LF	185 54	\$ 4.00 \$ 20.00		740 1,080	
		Hammock Poles	EA	4			2,000	
		Glacial Boulders	EA EA	13 1			8,450 10,000	
		Canoe Rack Log Seating	EA	1			10,000 1,600	
	Upstream Picnic Area	Crushed Limestone (4" depth)	SF	550			2,200	
<u> </u>		Stone Edger Limestone Seatwall (Curved Segments)	LF	110 36			2,200 15,120	
		Glacial Boulders	EA	13	\$ 650.00	\$	8,450	
		Picnic table Bike Rack	EA	1			4,000 1,200	
		Interpretive Signage	EA	1	\$ 2,000.00	\$	2,000	
	Downstream Picnic Area	Crushed Limestone (4" depth) Stone Edger	SF LF	550 80	\$ 4.00 \$ 20.00		2,200 1,600	
		Limestone Seatwall (Curved Segments)	LF	18			7,560	
		Glacial Boulders Bike Back	EA EA	13			8,450 1,200	
		Bike Rack Interpretive Signage	EA	1			1,200 2,000	
NATURE PLAY	Nature Play Area	play equipments/seating/creek access	LS	1	\$ 300,000.00	\$	300,000	
G2G PLAZA	Blake and Lake	Greenway/Gateway Plaza	LS	1	\$ 700,000.00	\$	700,000	
		Stormwater Construction Subtotal				\$	1,594,234	47%
		Public Realm Construction Subtotal				\$ \$	1,830,656	477
		Total Construction Subtotal	<u> </u>			\$	3,424,889	check \$ 3,424,889
						Ş	3,424,889	3,424,889
		Mob/SWPPP				\$	273,991	
		Subtotal				\$	3,698,880	
		Contractor Incidentals		10%		\$	369,888.04	
		Subtotal				\$	4,068,768	
		Design Contingency		20%		\$	813,753.69	Will reduce as design progresses
		Subtotal				\$	4,882,522	
		Construction Contingency		10%		\$	488,252.21	Stays to account for work near water, unique structures, etc.
		Total				\$	5,370,774	
		Stormwater				\$	2,500,014	
		Public Realm				\$	2,870,761	



WATERSHED DISTRICT







Contract Drawings For

325 BLAKE RD

RESTORATION & REDEVELOPMENT PROJECT

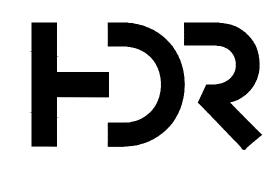
HDR Project No. 10268112

HOPKINS, MINNESOTA JUNE, 2022

<u>GENERAL</u> GC102 GC103 GC104 GC105

SITE WORK CG301

L001 L002 L010 L030 L110 L111 L160 L161 L410 L411 L412 L413 L500 - L580 L590 - L595





INDEX OF DRAWINGS

GENERAL NOTES SYMBOLOGY SURVEY AND CONTROL ALIGNMENT TABLES

EC101 - EC105 EROSION CONTROL PLAN EC104 - EC105 EROSION CONTROL DETAILS CD101 - CD103 DEMOLITION AND PRESERVATION PLAN CG101 - CG105 SITE GRADING PLAN CG201 - CG202 SITE TYPICAL SECTIONS POND CROSS SECTIONS CT101 - CT104 TRAIL PLAN AND PROFILES CP101 - CP104 STORM SEWER PLAN AND PROFILES ST101 - ST120 STRUCTURAL PLAN AND DETAILS LANDSCAPE GEN NOTES SITE ORIENTATION PLAN SITE MATERIALS SCHEDULE PLANTING, SOILS, AND FURNISHING SCHEDULES HARDSCSAPE PLAN A - SOUTH HARDSCAPE PLAN B - NORTH PLANTING PLAN A - SOUTH PLANTING PLAN B - NORTH HARDSCAPE ENLARGEMENT PLAN - TRAILHEAD HARDSCAPE ENLARGEMENT PLAN - LANDING

HARDSCAPE ENLARGEMENT PLAN - NAT PLAY HARDSCAPE ENLARGEMENT PLAN - GATEWAY PLAZA

HARDSCAPE DETAILS

PLANTING AND TREE PRESERVATION DETAILS

		1		2		3		
ſ								
		<u>GENERAL</u>	CONSTRUCTION	NOTES				
	1.	LOCATE AND PROTECT ALL SHOWN IN THE PLANS. THE CONTACTING GOPHER ONE HOURS PRIOR TO COMMEN	CONTRACTOR CALL FOR A U	IS RESPONSIBLE FOR FILITY LOCATE AT LE	R			
	2.	THE CONTRACTOR IS RESP MINNESOTA NPDES/SDS CC (SWPPP) AND MEETING ALL	INSTRUCTION S	TORMWATER PERMIT	Г			
	3.	STAKE LIMITS OF CONSTRU REVIEW PRIOR TO STARTIN			TIVE TO			
	4.	USE CAUTION WHEN WORK MINNEHAHA CREEK. ANY D OF THE CONTRACTOR.						
	5.	ALL PRE-PROJECT DRAINA OTHERWISE SHOWN ON TH			UNLESS			
	6.	RESTORE AREAS DISTURBI).			
	7.	DO NOT INTERRUPT OR BLO	OCK PUBLIC RO	AD TRAFFIC.				
	8.	ALLOW ACCESS TO OTHER PROPERTY BY OTHER CON EMERGENCY PERSONNEL T SWLRT TRAIL.	TRACTORS. PR	OVIDE ACCESS FOR				
L								NAGED
	UPLITYOF	W P I R					PROJECT MA	
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MINNEHAHA CREEK WATERSHED DISTRICT

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ISSUE	DATE	DESCRIPTION	
0	2/18/2022	60% DRAFT FOR CLIENT REVIEW	

PROJECT MANAGER	ANDREW F. JUDD
PROJECT NUMBER	10268112

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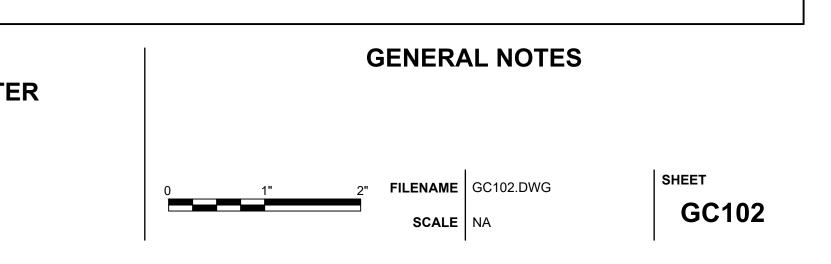
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325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343



1

CIVIL I	MAPPING SYMBOLOGY	UTILITY/CIVIL LINE SYMBO	LOG
Ý Ý Ý	– EMBANKMENT SLOPE (CUT) –	— — — — — — — UTILITY BENEATH	STRUC
	– EMBANKMENT SLOPE (FILL)		
H:V	- EMBANKMENT SLOPE RIGHT ARROW RIGHT	LIMITS OF CONST	RUCTION
H:V	EMBANKMENT SLOPE LEFT ARROW LEFT	ROW	
×	SPOT ELEVATION/POINT #	— — — — — — — EXISTING CONTO	ur (ming
۲	SURVEY BENCHMARK	25 EXISTING CONTO	UR W/EL
CP-X	SURVEY CONTROL POINT	SURVEYED EDGE	
	HORIZONTAL CONTROL POINT	NEW CONTOUR (N	
\odot	VERTICAL CONTROL POINT		
₿ _×	TEST PIT		
⊘ _×	SOIL BORING		
4 ~~~	FLOW ARROW	——————————————————————————————————————	
∑	WATER LEVEL IN SECTION/PROFILE	SANITARY SEWER	2
- 	DOWNGUY		MAIN
Ūx	EXTERIOR UTILITY JUNCTION BOX	\longrightarrow storm sewer	
(xxx)	INTERSTATE HIGHWAY SYMBOL		
$\widetilde{\frown}$	US HIGHWAY SYMBOL	OVERHEAD ELEC OVERHEAD ELEC STREET LIGHTS	IRICAL
		UNDERGROUND E	LECTRIC
	STATE HIGHWAY SYMBOL	CABLE CABLE CABLE UNDERGROUND 1	EI EPHO
			ELEPHO
E	HAY BALE SILT CHECK		RY SEWE
0	TEMPORARY SEDIMENT TRAP		FIC WATE
O _x	PIEZOMETER		
⊗®	RAIL SIGNAL		ROL LOG
× ¥ 0	FIRE HYDRANT		
	MONITORING WELL		
3	SANITARY MANHOLE		
	PROVIDE SANITARY MANHOLE		
СВ	STORM SQUARE CATCH BASIN		
CB	STORM ROUND CATCH BASIN		
D	STORM DRAINAGE MANHOLE		
\bowtie	DOMESTIC WATER VALVE		
PD	PEDESTAL		
\boxtimes	POWER BOX		
Ø	POLE		
,- ,-	TARGET ELEVATION		

				PROJECT MANAGER	ANDREW F. JUDD
	ISSUE DATE	- F DF	SCRIPTION	PROJECT NUMBER	10268112
MINNEHAHA CREEK WATERSHED DISTRICT					

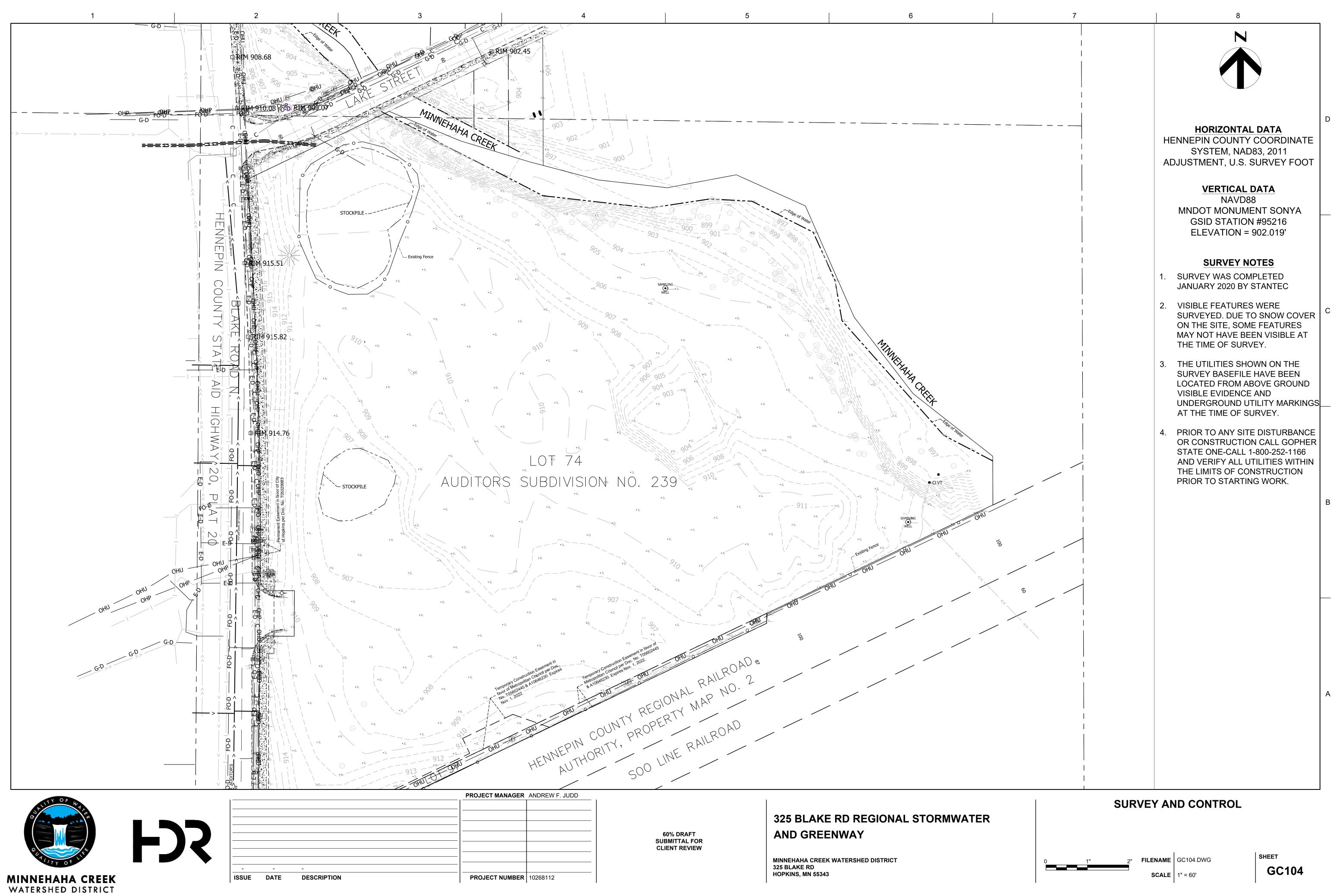
OGY	GENERAL SYMBOLOGY	SHEET NAMING CONVENTION
TRUCTURE	ARROW INDICATES DIRECTION OF PLAN NORTH	DISCIPLINE DESIGNATOR & DISCIPLINE ORDER G GENERAL V SURVEYING / MAPPING X DEMOLITION
JCTION	PLAN 1/4" = 1'-0" PLAN TITLE	C CIVIL L LANDSCAPING U MULTI-DISCIPLINE S STRUCTURAL A ARCHITECTURAL D PROCESS M MECHANICAL (HVAC) P PLUMBING
R (MINOR)	SECTION LETTER	F FIRE PROTECTION E ELECTRICAL
R W/ELEVATION (MAJOR)	FLAG INDICATES DIRECTION OF SECTION CUT	Y INSTRUMENTATION
F WATER		DRAWING TYPE DESIGNATOR
NOR)	SHEET WHERE SECTION IS LOCATED	0 GENERAL (SCHEDULES, SYMBOLS, LEGENDS) 1 PLANS 2 PROFILES / ELEVATIONS
JOR)	SECTION CUT MARKER	3 SECTIONS 4 LARGE SCALE VIEWS
L LOG, TYPE WOOD CHIP	SECTION LETTER	5 DETAILS 6 DIAGRAMS
11	DETAIL #	7 3D REPRESENTATIONS
	SECTION SHEET WHERE	EXAMPLE
	SECTION VIEW IS FIRST CUT *	PLAN AND PROFILE, SHEET 1 C DISCIPLINE DESIGNATOR
IAIN	# XXX	2 DRAWING TYPE DESIGNATOR 0 1
ICAL	SHEET WHERE DETAIL IS LOCATED * DETAIL MARKER FOR REFERENCING DETAILS INCLUDED IN DRAWING SET.	SHEET NUMBER C 2 0 1 SAMPLE SHEET NUMBER
ECTRICAL	< xxxxxxxxx>	
LEPHONE	DETAIL MARKER FOR REFERENCING DETAILS BOUND IN SPECIFICATIONS OR SEPARATE VOLUME.	
SEWER	DETAIL NUMBER	
CWATER	DETAIL #	GENERAL NOTES: 1. THIS IS A STANDARD CIVIL SYMBOLOGY SHEET. ALL SYMBOLS ARE NOT
	SCALE XXX SHEET WHERE DETAIL	NECESSARILY USED ON THIS PROJECT.
L LOG, TYPE ROCK	WAS CALLED OUT *	2. SCREENING OR SHADING OF WORK IS USED TO INDICATE EXISTING COM OR TO DE-EMPHASIZE PROPOSED IMPROVEMENTS TO HIGHLIGHT SELECT
	DETAIL TITLE ELEVATION NUMBER	WORK. REFER TO CONTEXT OF EACH SHEET FOR USAGE.
	ARROW INDICATES	
	POINT OF VIEW XXX SHEET WHERE ELEVATION	
	IS LOCATED * SINGLE ELEVATION OR PHOTO MARKER	
	ARROW INDICATES POINT OF VIEW ELEVATION	
	XXX INDICATES SHEET WHERE ELEVATION IS LOCATED	
	Č MULTIPLE ELEVATION OR PHOTO MARKER	
	ELEVATION IDENTIFICATION	
	NUMBER #	
	SCALE SHEET WHERE POINT OF VIEW MARKER CAN BE FOUND *	
	ELEVATION TITLE	
	 * EXCEPTIONS WHERE THE SHEET NUMBER IS REPLACED BY A DASH (-). 1) FOR COMMON DETAILS, SECTIONS, ELEVATIONS OR DETAILS THAT ARE CUT OR CALLED OUT ON MULTIPLE SHEETS. 2) SECTIONS, ELEVATIONS OR DETAILS THAT ARE LOCATED ON THE SAME SHEET THEY ARE CUT OR CALLED OUT ON. 	

60% DRAFT SUBMITTAL FOR CLIENT REVIEW

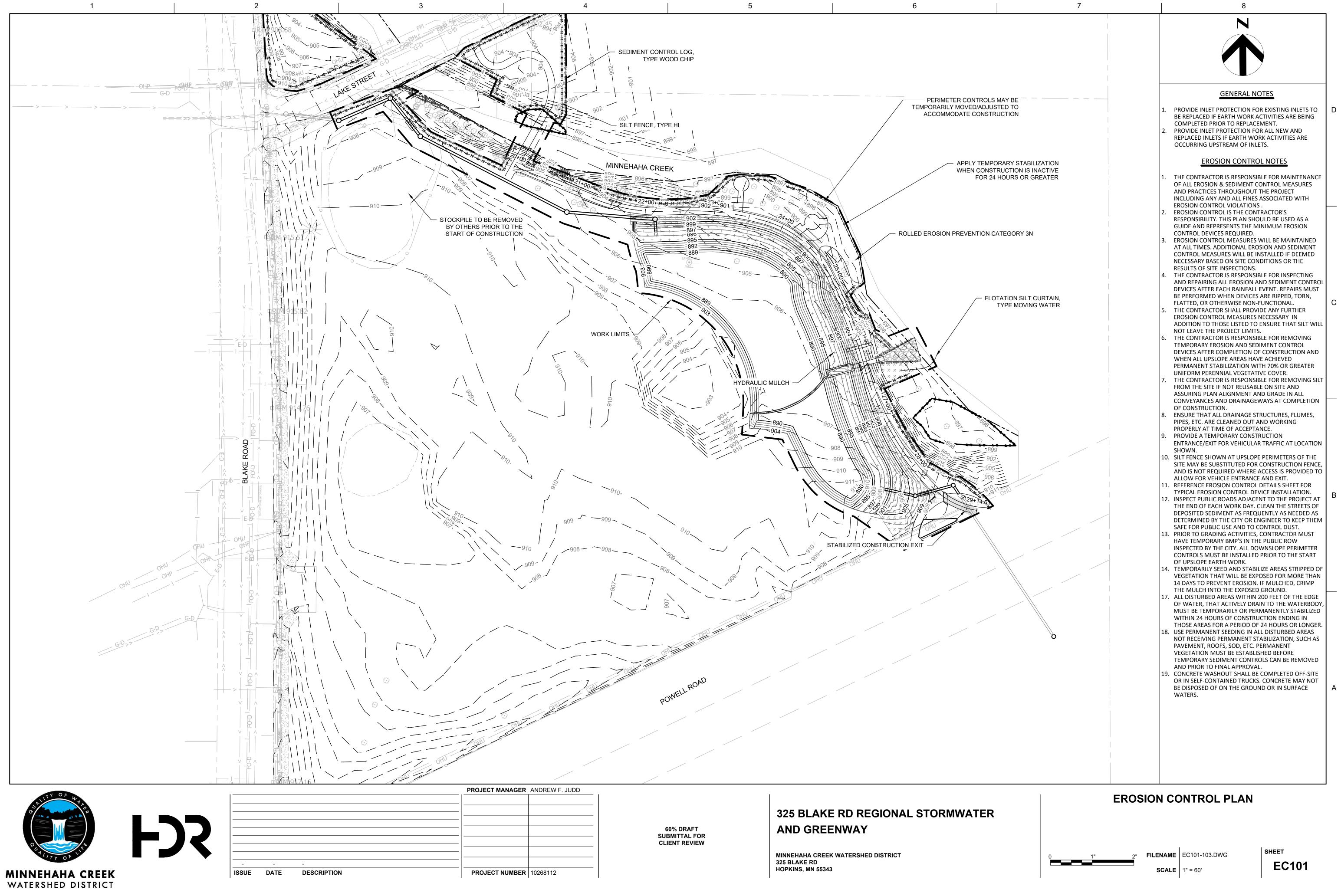
325 BLAKE RD REGIONAL STORMWATE AND GREENWAY

MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343

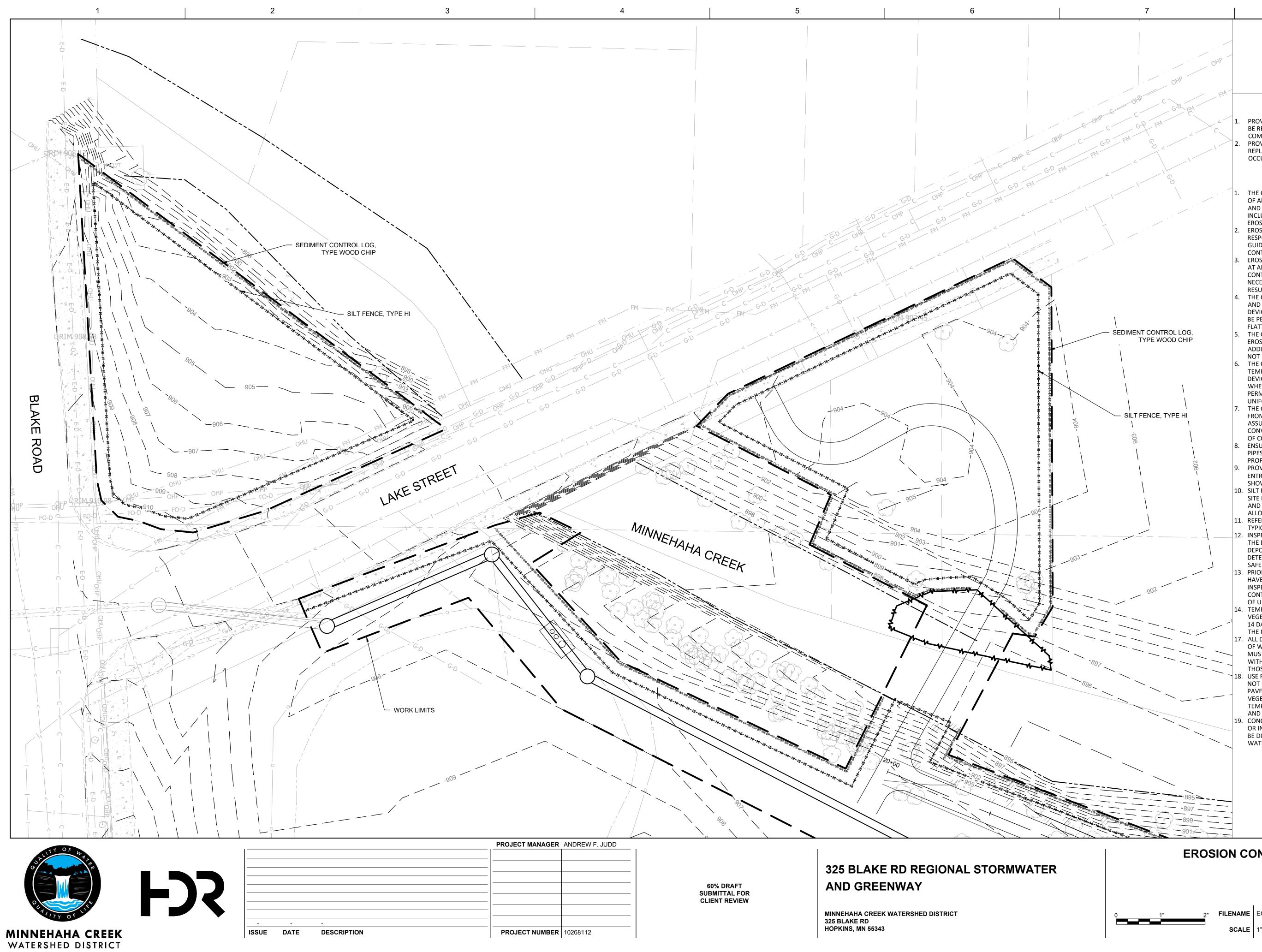
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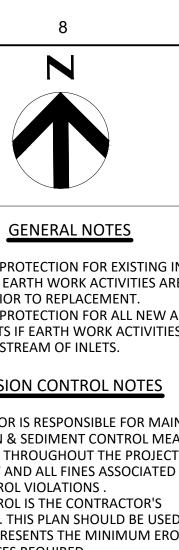


ANDREW F. JUDD
10268112



PROJECT MANAGER	ANDREW F. JUDD
PROJECT NUMBER	10268112





PROVIDE INLET PROTECTION FOR EXISTING INLETS TO D BE REPLACED IF EARTH WORK ACTIVITIES ARE BEING COMPLETED PRIOR TO REPLACEMENT. PROVIDE INLET PROTECTION FOR ALL NEW AND REPLACED INLETS IF EARTH WORK ACTIVITIES ARE OCCURRING UPSTREAM OF INLETS.

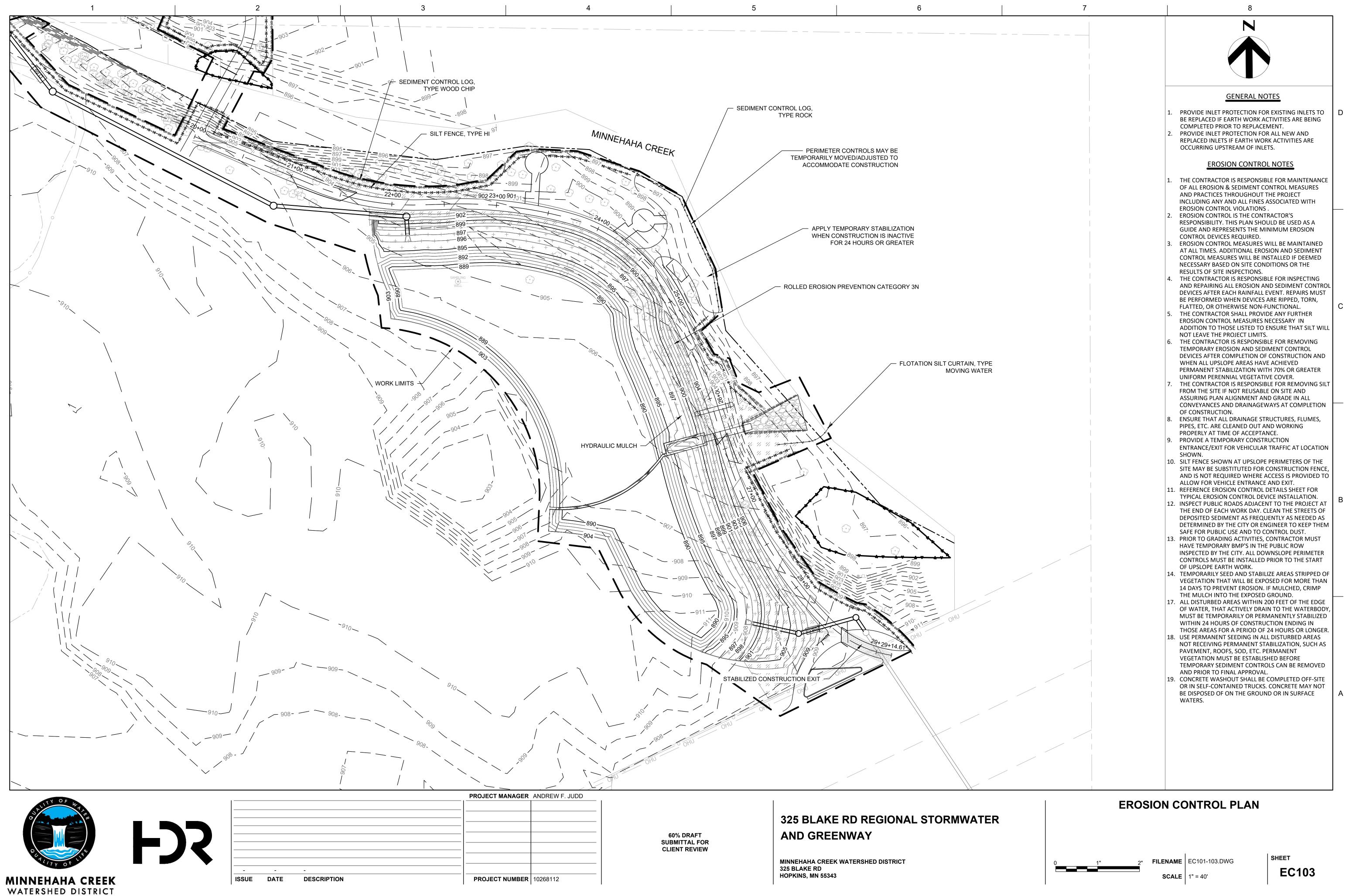
EROSION CONTROL NOTES

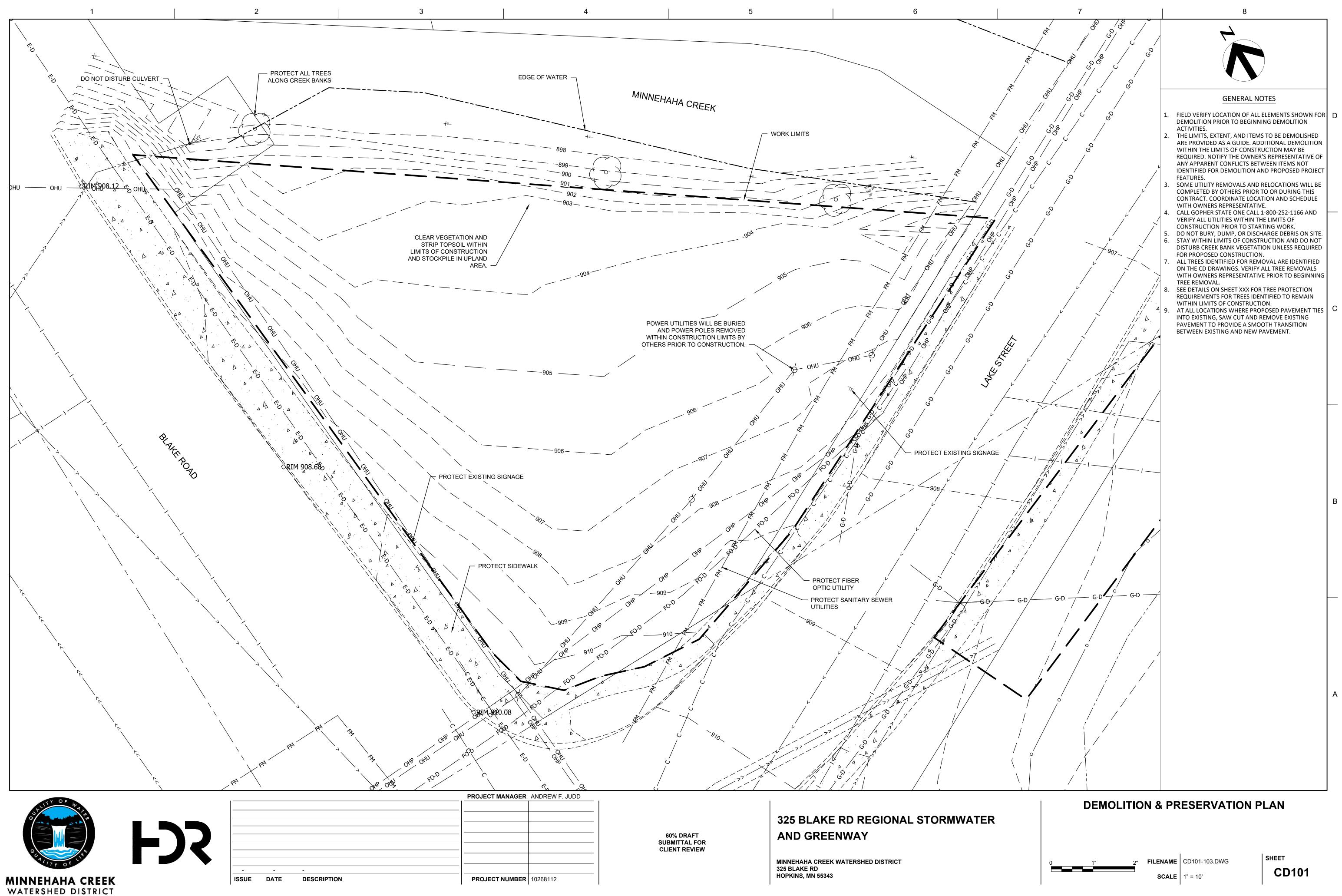
THE CONTRACTOR IS RESPONSIBLE FOR MAINTENANCE OF ALL EROSION & SEDIMENT CONTROL MEASURES AND PRACTICES THROUGHOUT THE PROJECT INCLUDING ANY AND ALL FINES ASSOCIATED WITH EROSION CONTROL VIOLATIONS . **EROSION CONTROL IS THE CONTRACTOR'S** RESPONSIBILITY. THIS PLAN SHOULD BE USED AS A GUIDE AND REPRESENTS THE MINIMUM EROSION CONTROL DEVICES REQUIRED. EROSION CONTROL MEASURES WILL BE MAINTAINED AT ALL TIMES. ADDITIONAL EROSION AND SEDIMENT CONTROL MEASURES WILL BE INSTALLED IF DEEMED NECESSARY BASED ON SITE CONDITIONS OR THE RESULTS OF SITE INSPECTIONS. THE CONTRACTOR IS RESPONSIBLE FOR INSPECTING AND REPAIRING ALL EROSION AND SEDIMENT CONTROL DEVICES AFTER EACH RAINFALL EVENT. REPAIRS MUST BE PERFORMED WHEN DEVICES ARE RIPPED, TORN, С FLATTED, OR OTHERWISE NON-FUNCTIONAL. THE CONTRACTOR SHALL PROVIDE ANY FURTHER EROSION CONTROL MEASURES NECESSARY IN ADDITION TO THOSE LISTED TO ENSURE THAT SILT WILL NOT LEAVE THE PROJECT LIMITS. THE CONTRACTOR IS RESPONSIBLE FOR REMOVING TEMPORARY EROSION AND SEDIMENT CONTROL DEVICES AFTER COMPLETION OF CONSTRUCTION AND WHEN ALL UPSLOPE AREAS HAVE ACHIEVED PERMANENT STABILIZATION WITH 70% OR GREATER UNIFORM PERENNIAL VEGETATIVE COVER. THE CONTRACTOR IS RESPONSIBLE FOR REMOVING SILT FROM THE SITE IF NOT REUSABLE ON SITE AND ASSURING PLAN ALIGNMENT AND GRADE IN ALL CONVEYANCES AND DRAINAGEWAYS AT COMPLETION OF CONSTRUCTION. ENSURE THAT ALL DRAINAGE STRUCTURES, FLUMES, PIPES, ETC. ARE CLEANED OUT AND WORKING PROPERLY AT TIME OF ACCEPTANCE. PROVIDE A TEMPORARY CONSTRUCTION ENTRANCE/EXIT FOR VEHICULAR TRAFFIC AT LOCATION SHOWN. 10. SILT FENCE SHOWN AT UPSLOPE PERIMETERS OF THE SITE MAY BE SUBSTITUTED FOR CONSTRUCTION FENCE, AND IS NOT REQUIRED WHERE ACCESS IS PROVIDED TO ALLOW FOR VEHICLE ENTRANCE AND EXIT. 11. REFERENCE EROSION CONTROL DETAILS SHEET FOR TYPICAL EROSION CONTROL DEVICE INSTALLATION. 12. INSPECT PUBLIC ROADS ADJACENT TO THE PROJECT AT THE END OF EACH WORK DAY. CLEAN THE STREETS OF DEPOSITED SEDIMENT AS FREQUENTLY AS NEEDED AS DETERMINED BY THE CITY OR ENGINEER TO KEEP THEM SAFE FOR PUBLIC USE AND TO CONTROL DUST. 13. PRIOR TO GRADING ACTIVITIES, CONTRACTOR MUST HAVE TEMPORARY BMP'S IN THE PUBLIC ROW INSPECTED BY THE CITY. ALL DOWNSLOPE PERIMETER CONTROLS MUST BE INSTALLED PRIOR TO THE START OF UPSLOPE EARTH WORK. 14. TEMPORARILY SEED AND STABILIZE AREAS STRIPPED O VEGETATION THAT WILL BE EXPOSED FOR MORE THAN 14 DAYS TO PREVENT EROSION. IF MULCHED, CRIMP THE MULCH INTO THE EXPOSED GROUND. ALL DISTURBED AREAS WITHIN 200 FEET OF THE EDGE OF WATER, THAT ACTIVELY DRAIN TO THE WATERBOD MUST BE TEMPORARILY OR PERMANENTLY STABILIZED WITHIN 24 HOURS OF CONSTRUCTION ENDING IN THOSE AREAS FOR A PERIOD OF 24 HOURS OR LONGER USE PERMANENT SEEDING IN ALL DISTURBED AREAS NOT RECEIVING PERMANENT STABILIZATION, SUCH AS PAVEMENT, ROOFS, SOD, ETC. PERMANENT VEGETATION MUST BE ESTABLISHED BEFORE TEMPORARY SEDIMENT CONTROLS CAN BE REMOVED AND PRIOR TO FINAL APPROVAL. 19. CONCRETE WASHOUT SHALL BE COMPLETED OFF-SITE OR IN SELF-CONTAINED TRUCKS. CONCRETE MAY NOT BE DISPOSED OF ON THE GROUND OR IN SURFACE WATERS.

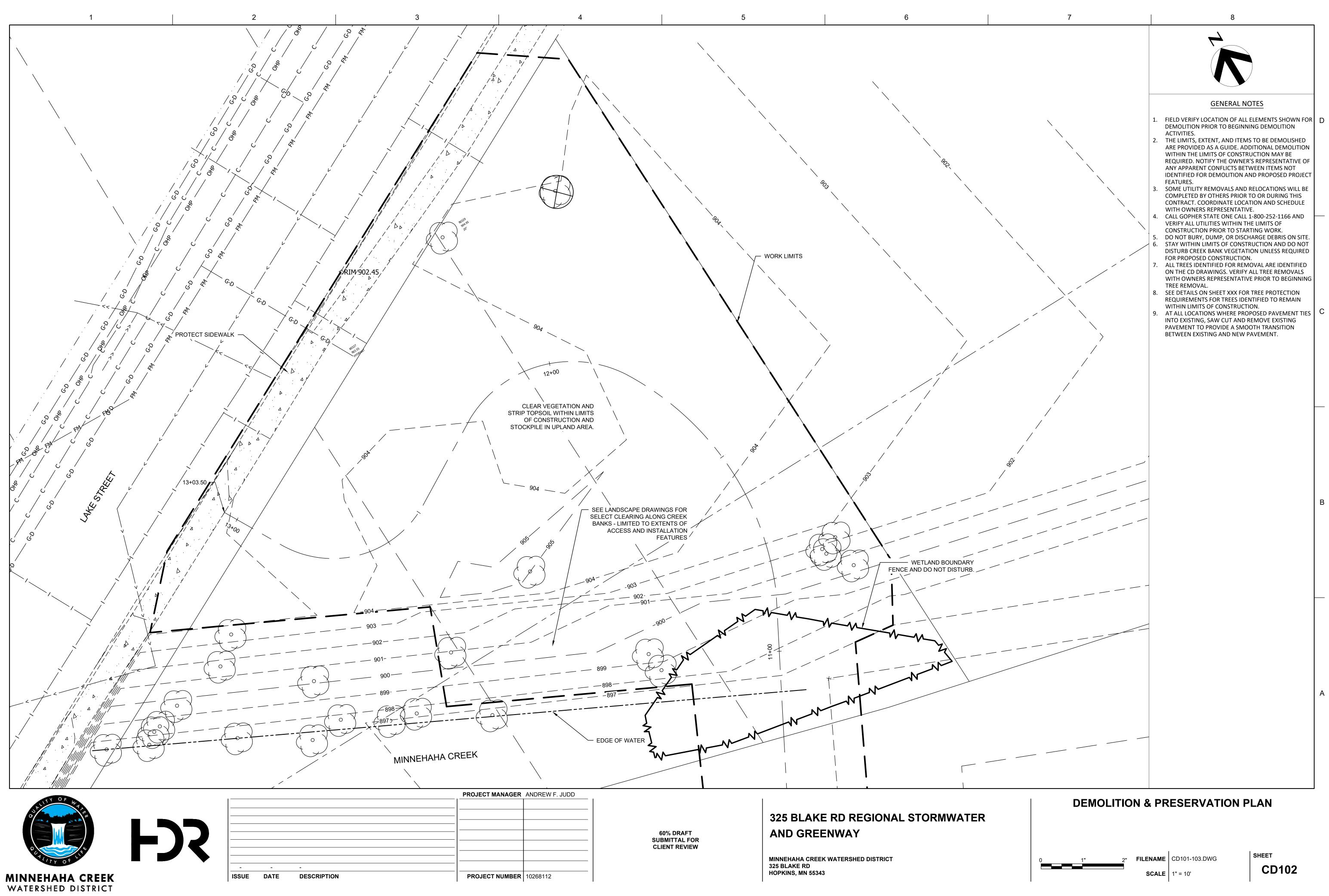
EROSION CONTROL PLAN

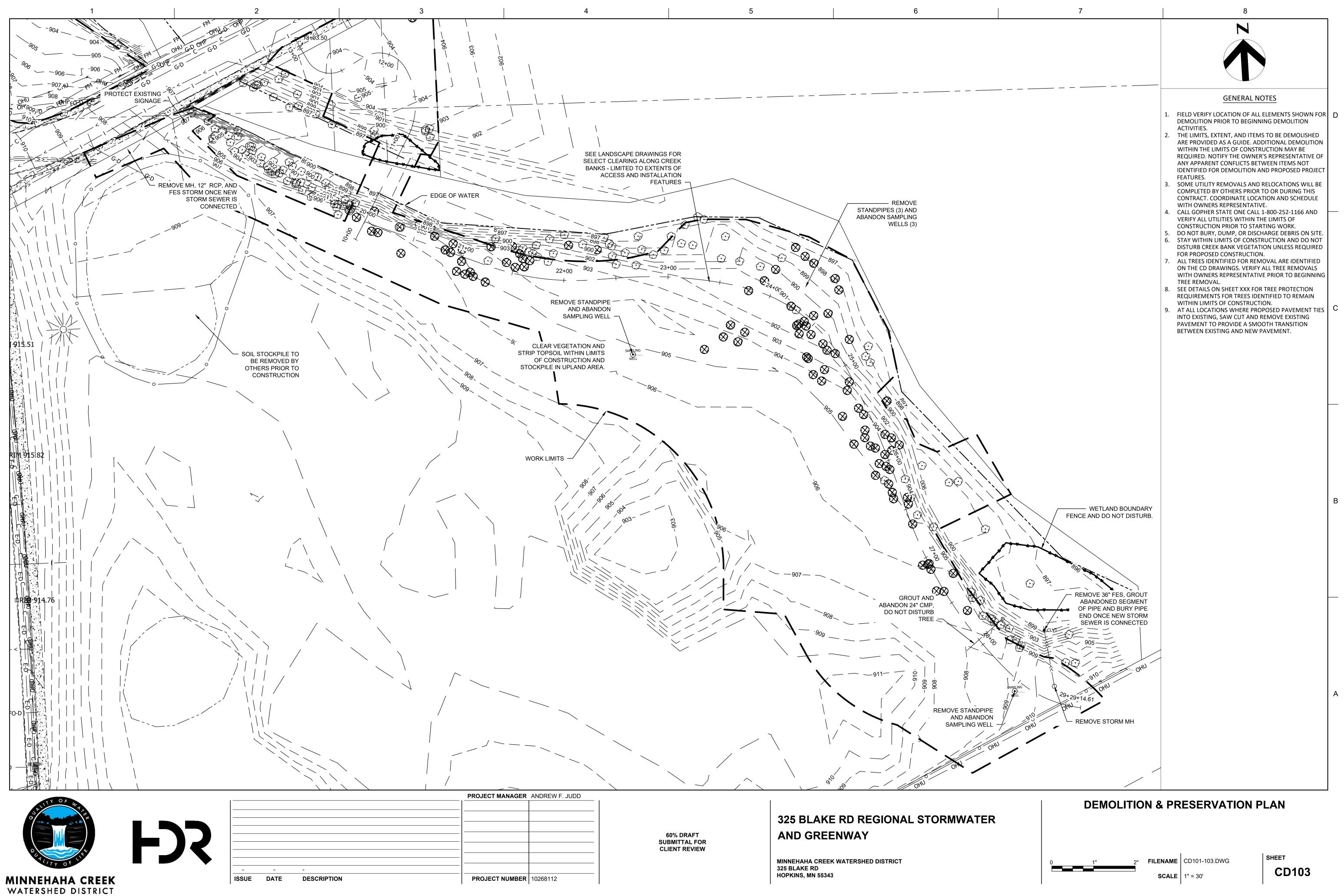
FILENAME EC101-103.DWG **SCALE** 1" = 20'

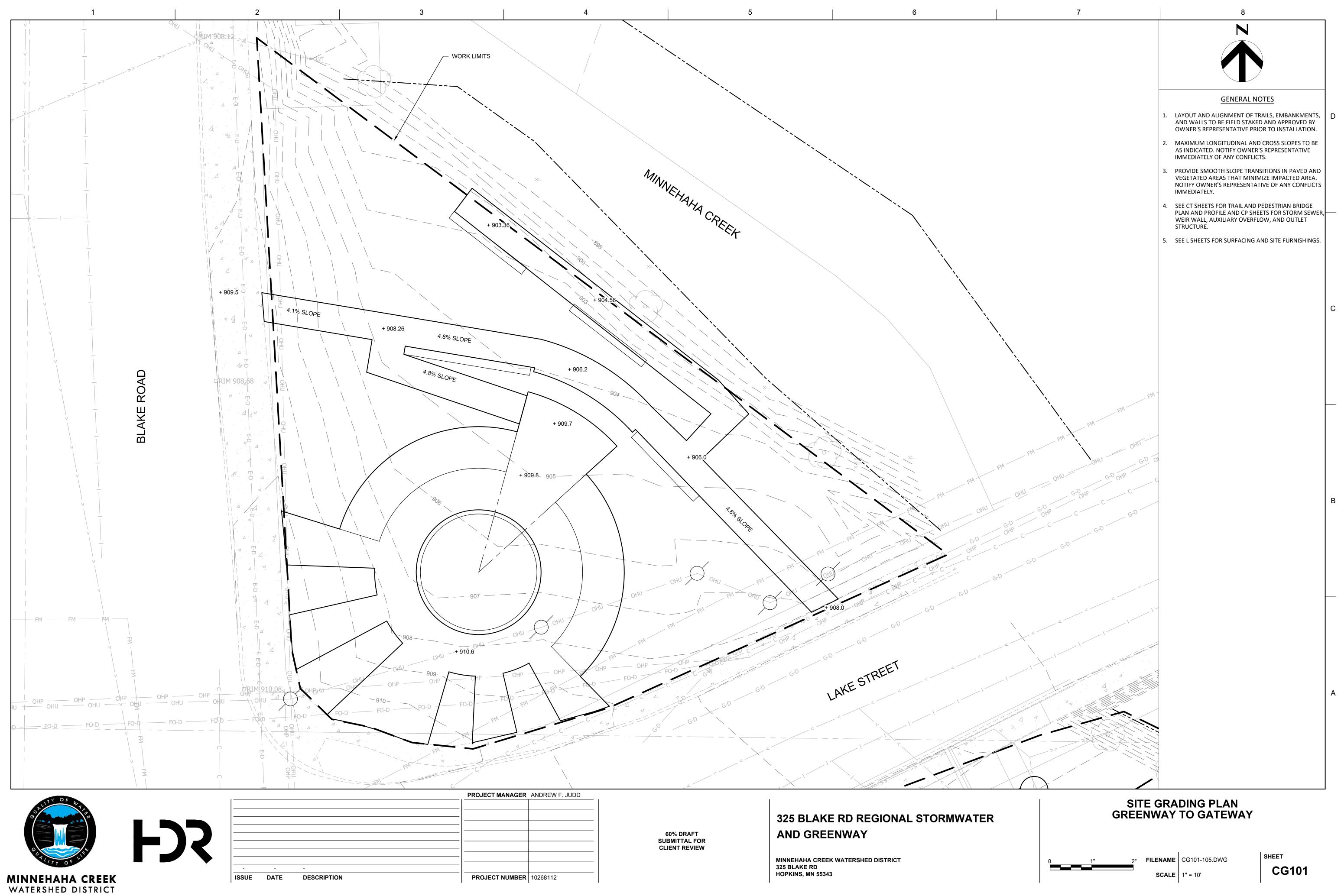
SHEET EC102



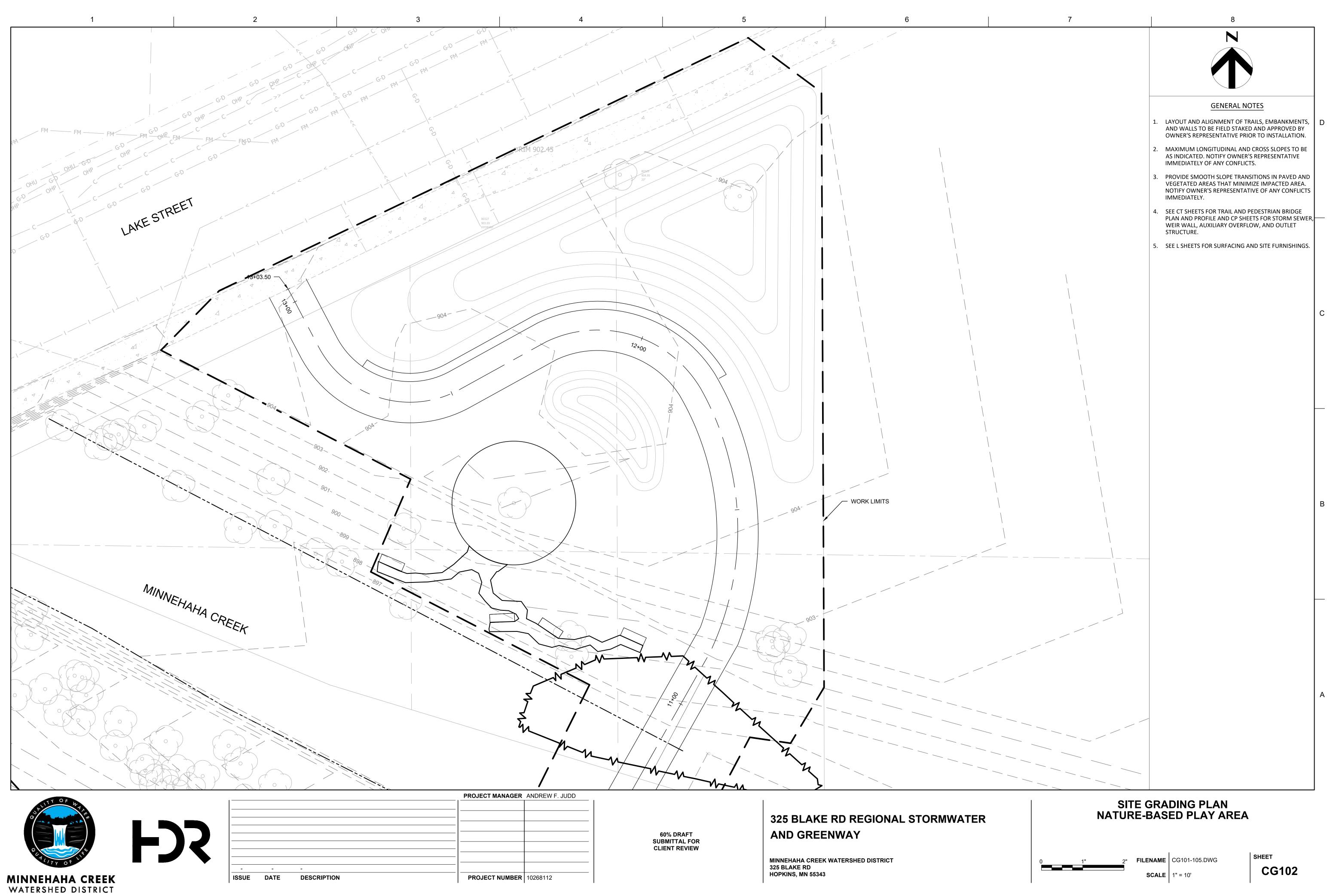


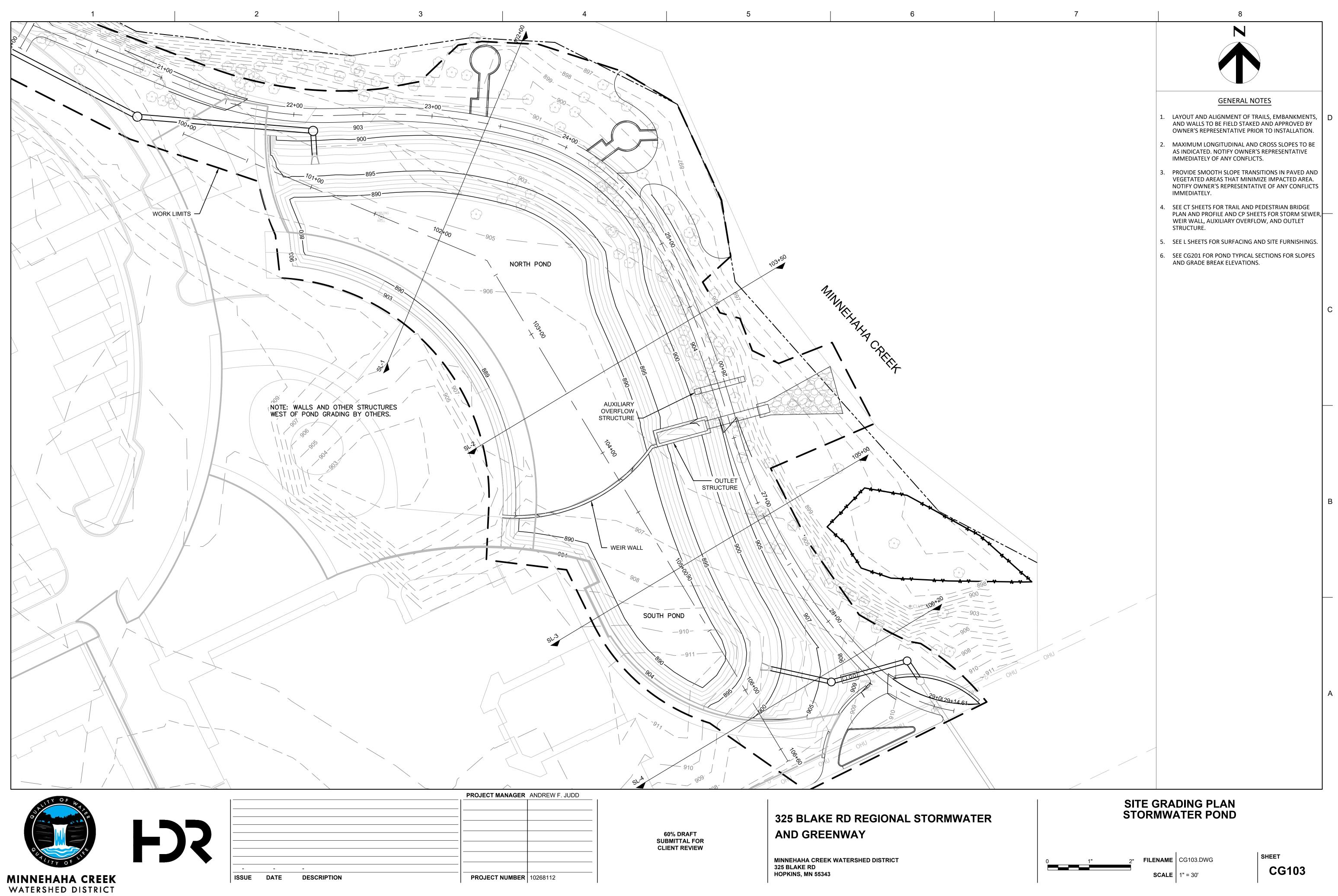




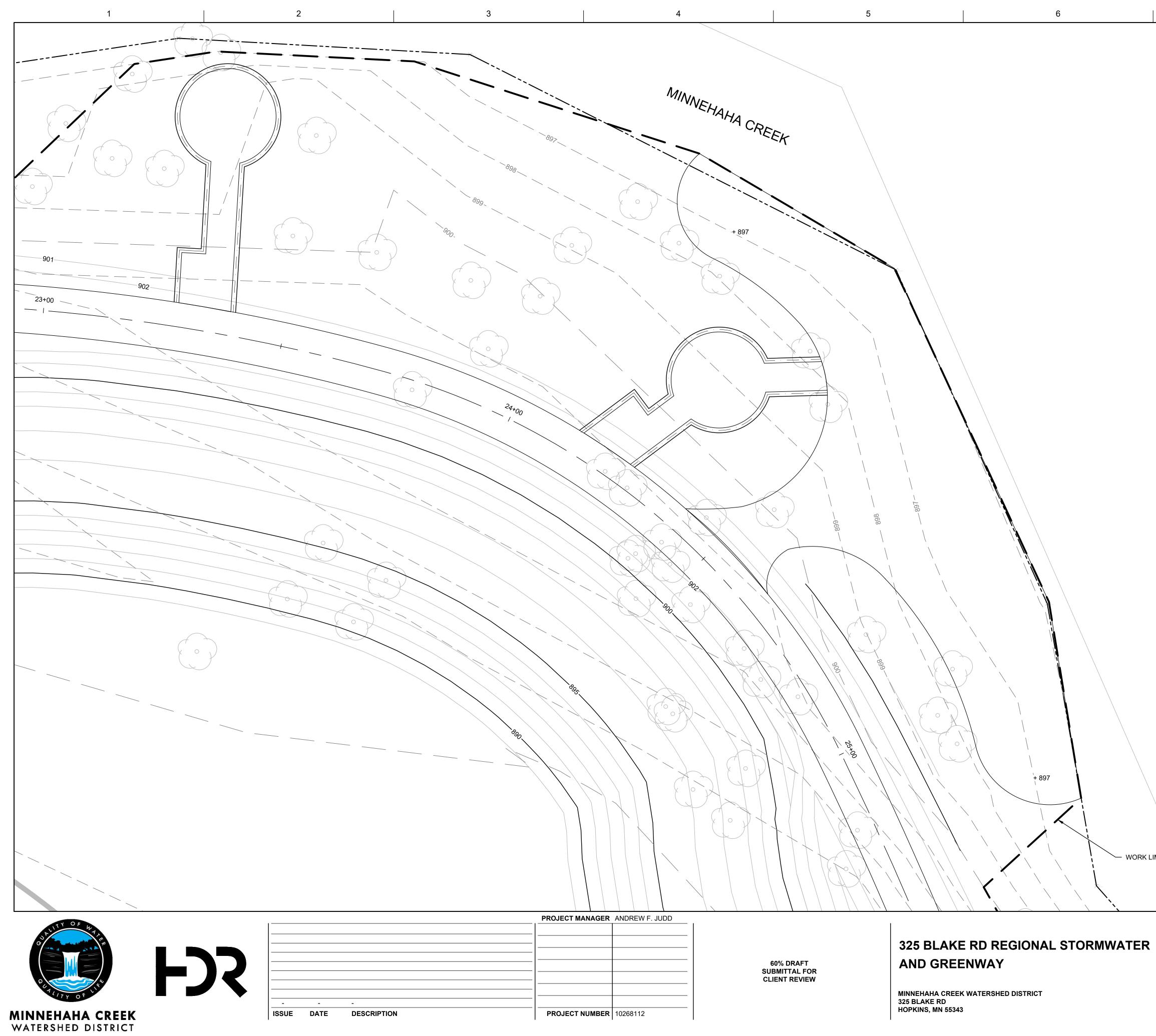


PROJECT MANAGER	ANDREW F. JUDD
PRO JECT NUMBER	10268112





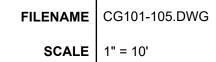
PROJECT MANAGER	ANDREW F. JUDD
PROJECT NUMBER	10268112



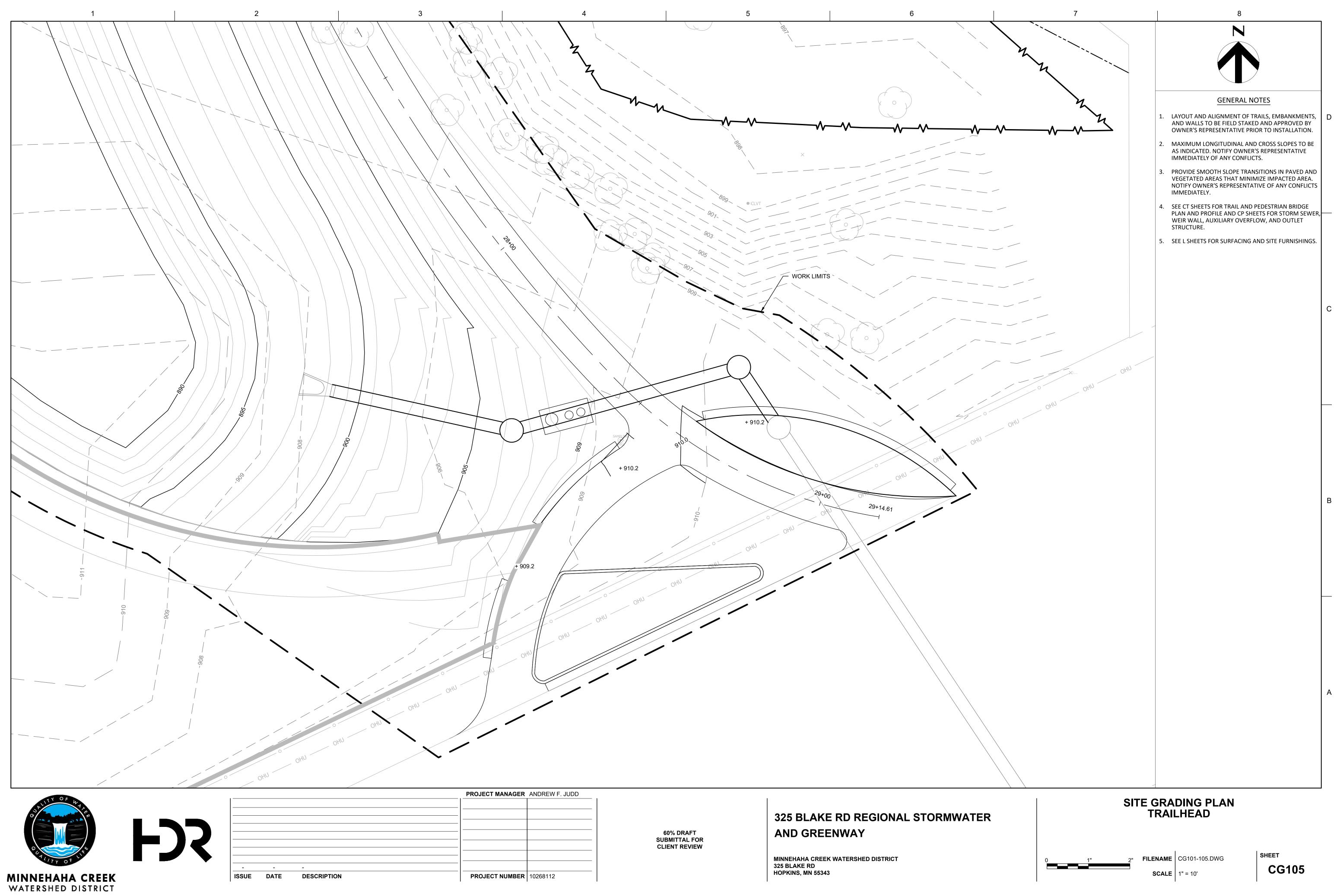
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	GENERAL NOTES
1.	LAYOUT AND ALIGNMENT OF TRAILS, EMBANKMENTS, AND WALLS TO BE FIELD STAKED AND APPROVED BY OWNER'S REPRESENTATIVE PRIOR TO INSTALLATION.
2.	MAXIMUM LONGITUDINAL AND CROSS SLOPES TO BE AS INDICATED. NOTIFY OWNER'S REPRESENTATIVE IMMEDIATELY OF ANY CONFLICTS.
3.	PROVIDE SMOOTH SLOPE TRANSITIONS IN PAVED AND VEGETATED AREAS THAT MINIMIZE IMPACTED AREA. NOTIFY OWNER'S REPRESENTATIVE OF ANY CONFLICTS IMMEDIATELY.
4.	SEE CT SHEETS FOR TRAIL AND PEDESTRIAN BRIDGE PLAN AND PROFILE AND CP SHEETS FOR STORM SEWER, WEIR WALL, AUXILIARY OVERFLOW, AND OUTLET STRUCTURE.
5.	SEE L SHEETS FOR SURFACING AND SITE FURNISHINGS.

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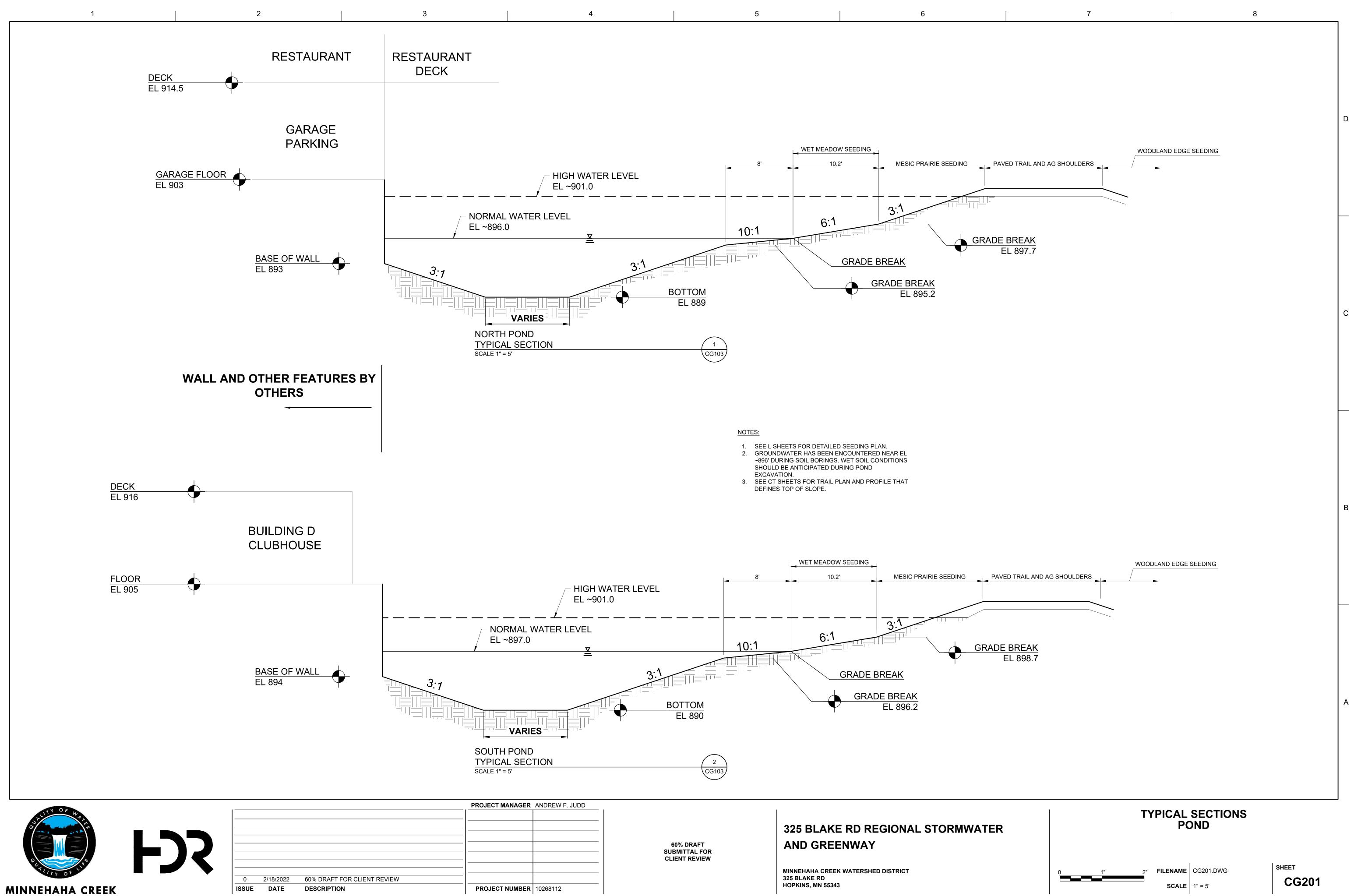




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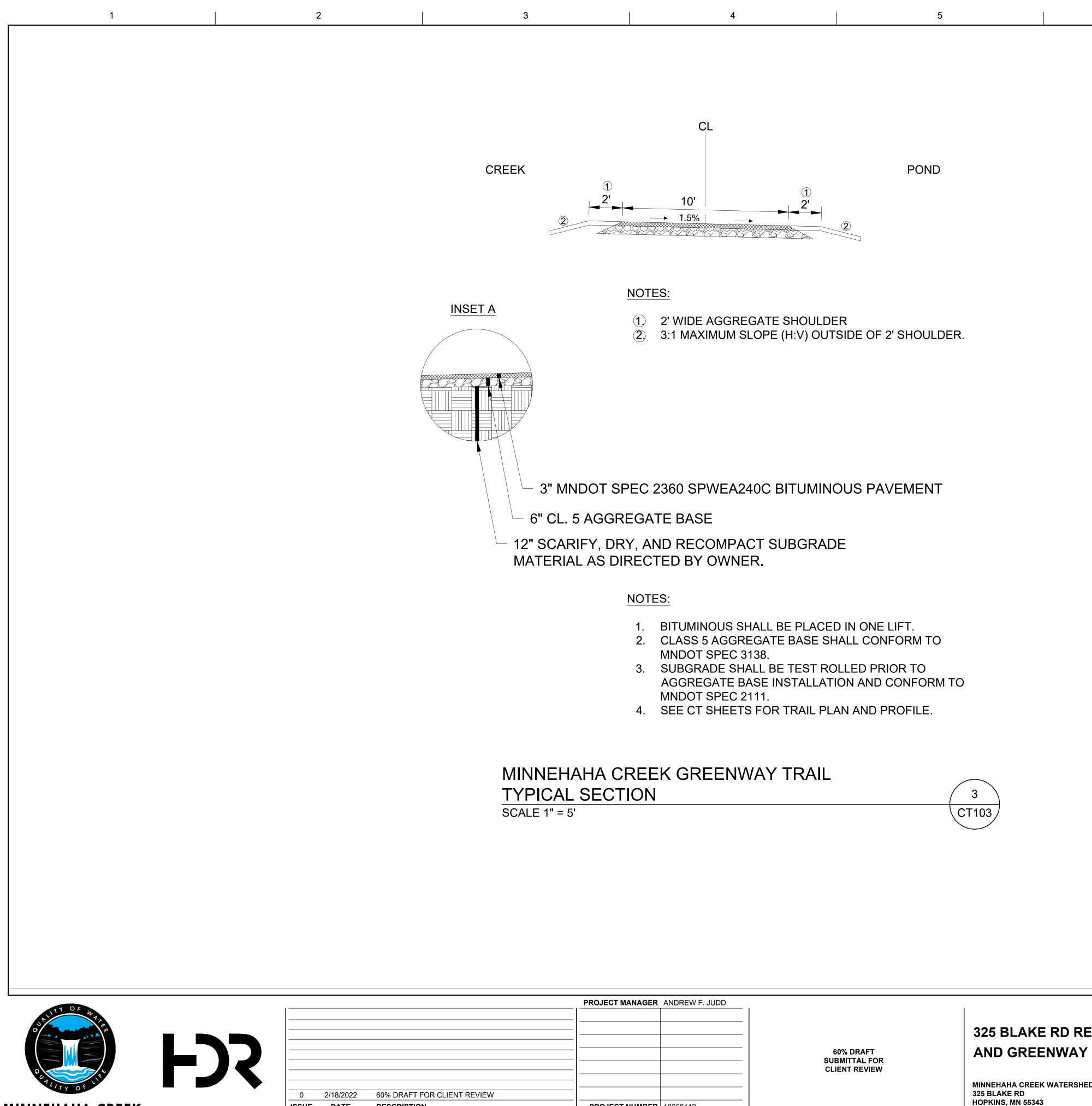


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NORMAL WATER LEVEL EL ~897.0 <u>₹</u>		
	3:1 BOTTOM EL 890	GRADE BREAK GRADE BREAK EL 896.2
SOUTH POND TYPICAL SECTION SCALE 1" = 5'	2 CG103	
PROJECT MANAGER ANDREW F. JUDD		
		325 BLAKE RD REGIONAL STORMWAT
	60% DRAFT SUBMITTAL FOR CLIENT REVIEW	AND GREENWAY
PROJECT NUMBER 10268112	3	IINNEHAHA CREEK WATERSHED DISTRICT 25 BLAKE RD OPKINS, MN 55343

WATERSHED DISTRICT

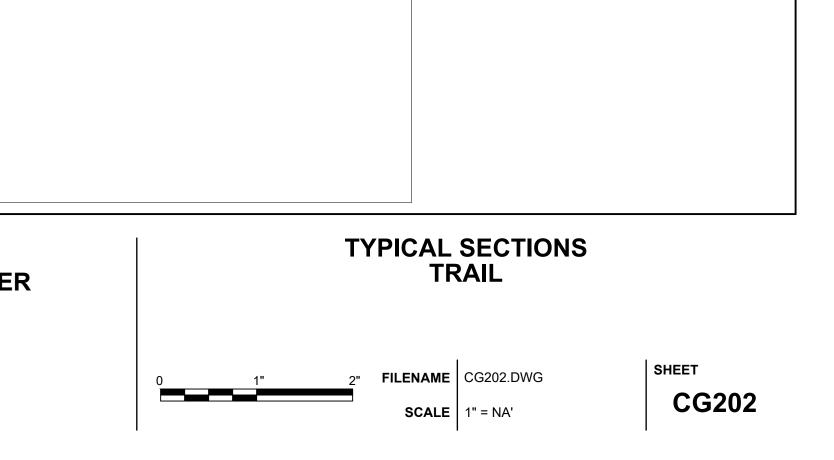


ISSUE DATE DESCRIPTION

PROJECT MANAGER	ANDREW F. JUDD
PROJECT NUMBER	10268112

325 BLAKE RD REGIONAL STORMWATER

MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343



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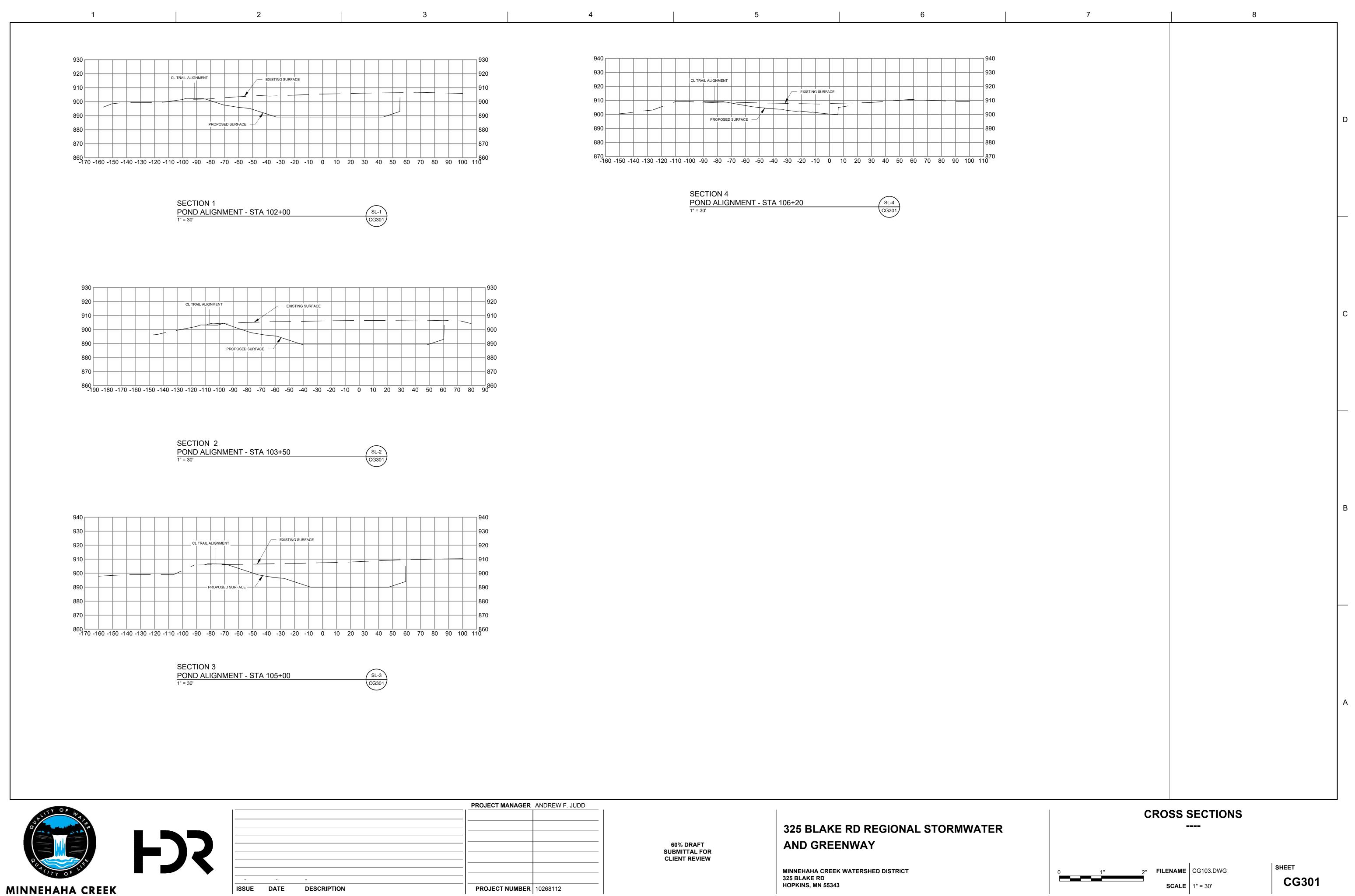
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WATERSHED DISTRICT

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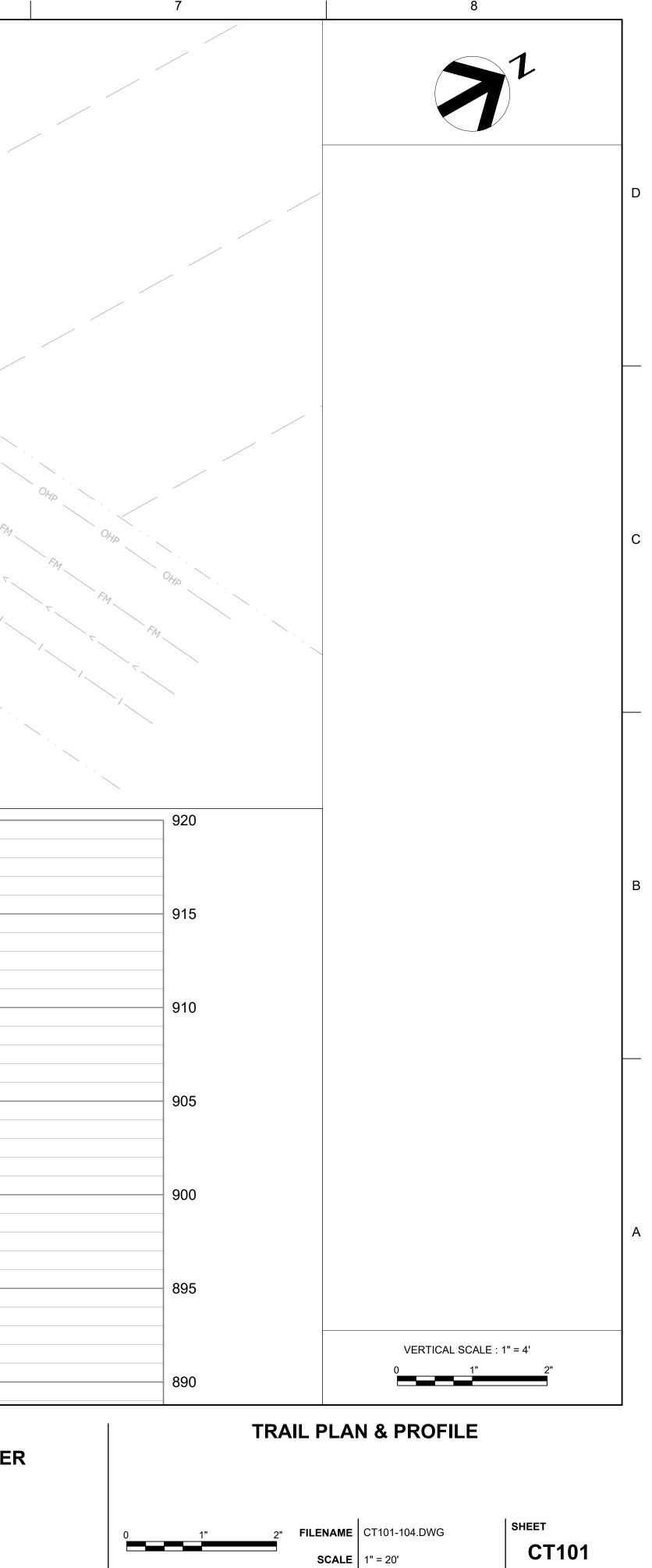
PROPOSED PRO	DFILE TO BE DEVELOPED AT 90%				
EXISTING GROUND	 				
/					
PROJECT MANAGER ANDRE	EW F. JUDD				

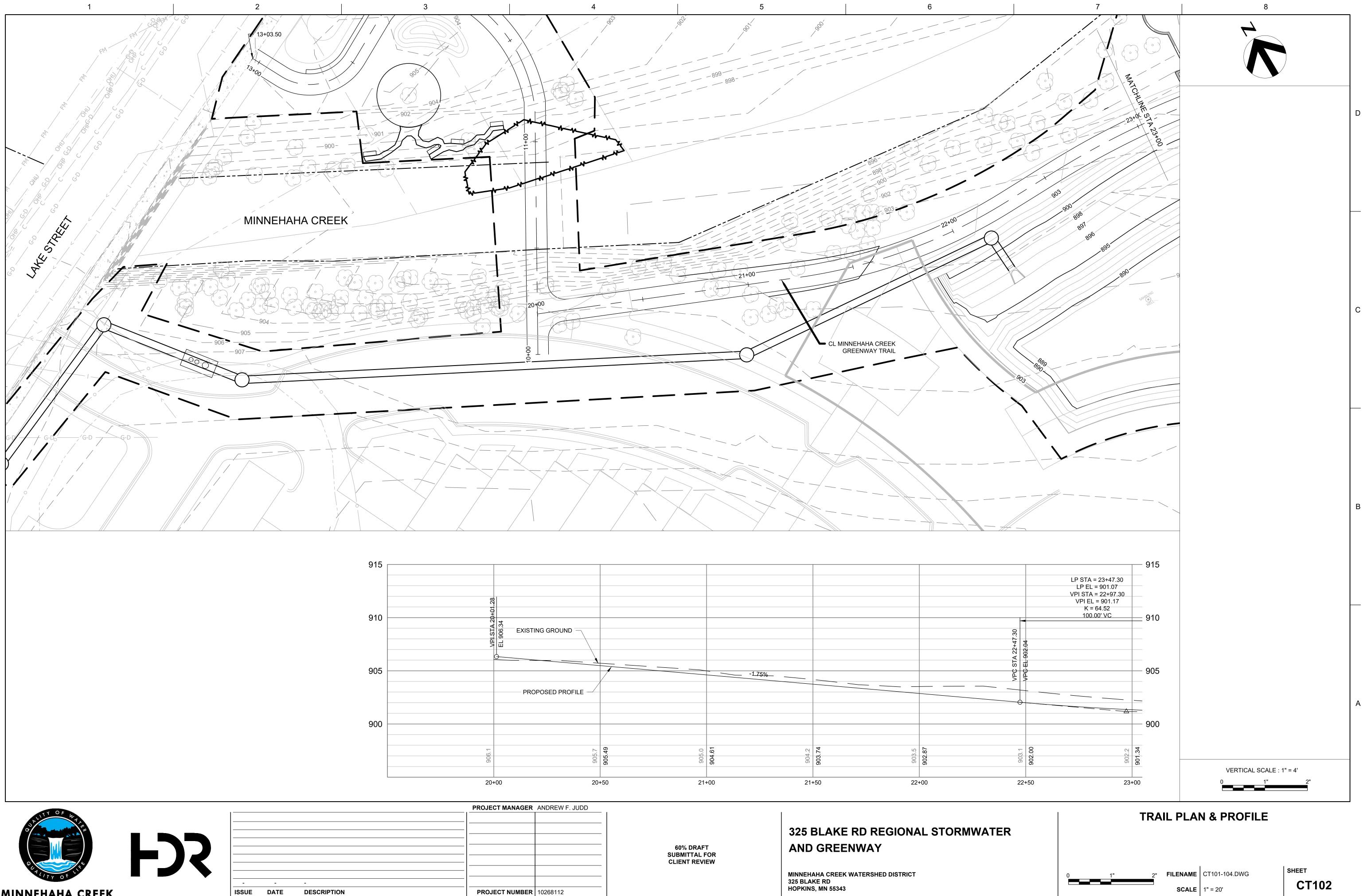
PROJECT MANAGER	ANDREW F. JUDD
PROJECT NUMBER	10268112

60% DRAFT SUBMITTAL FOR CLIENT REVIEW

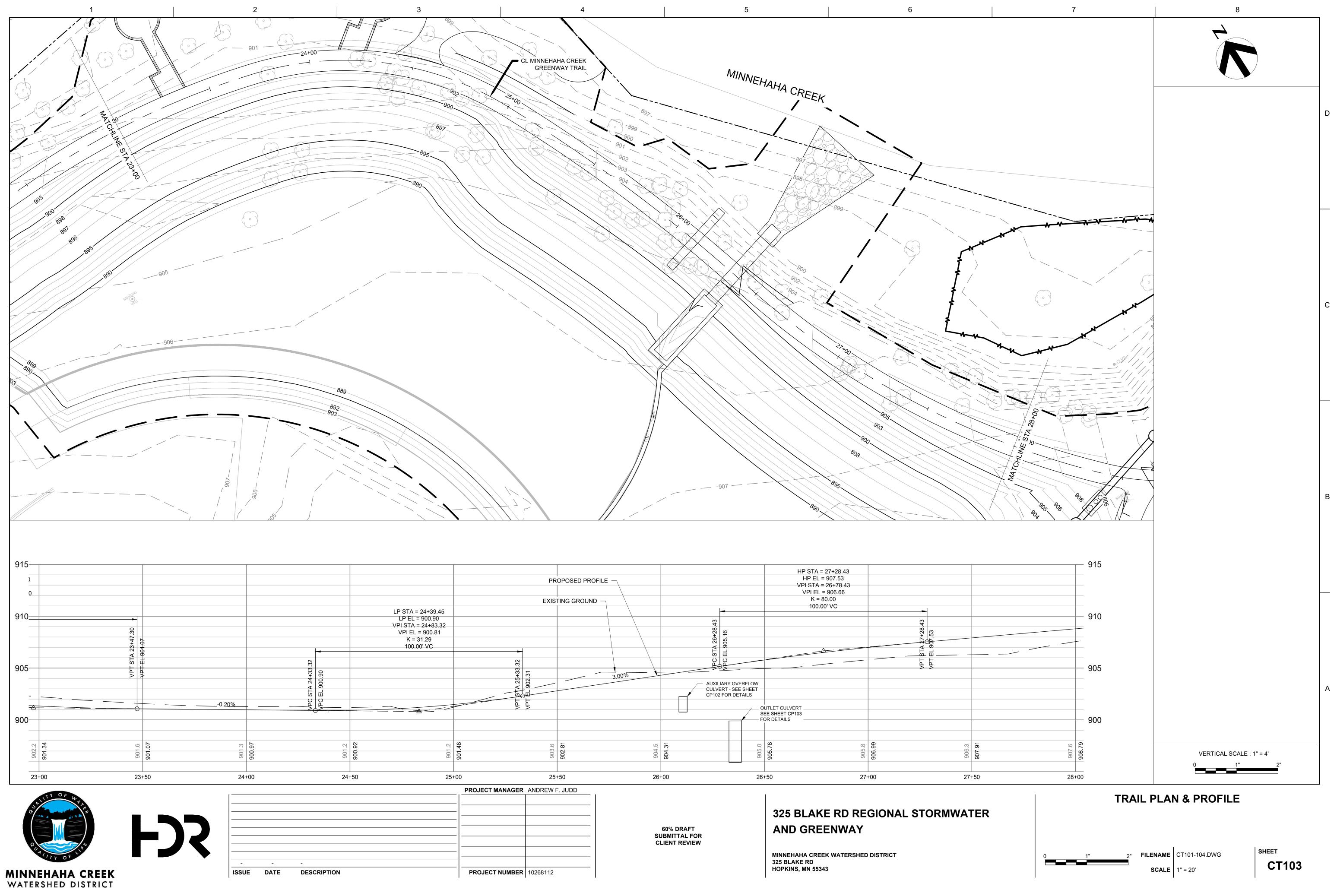
325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

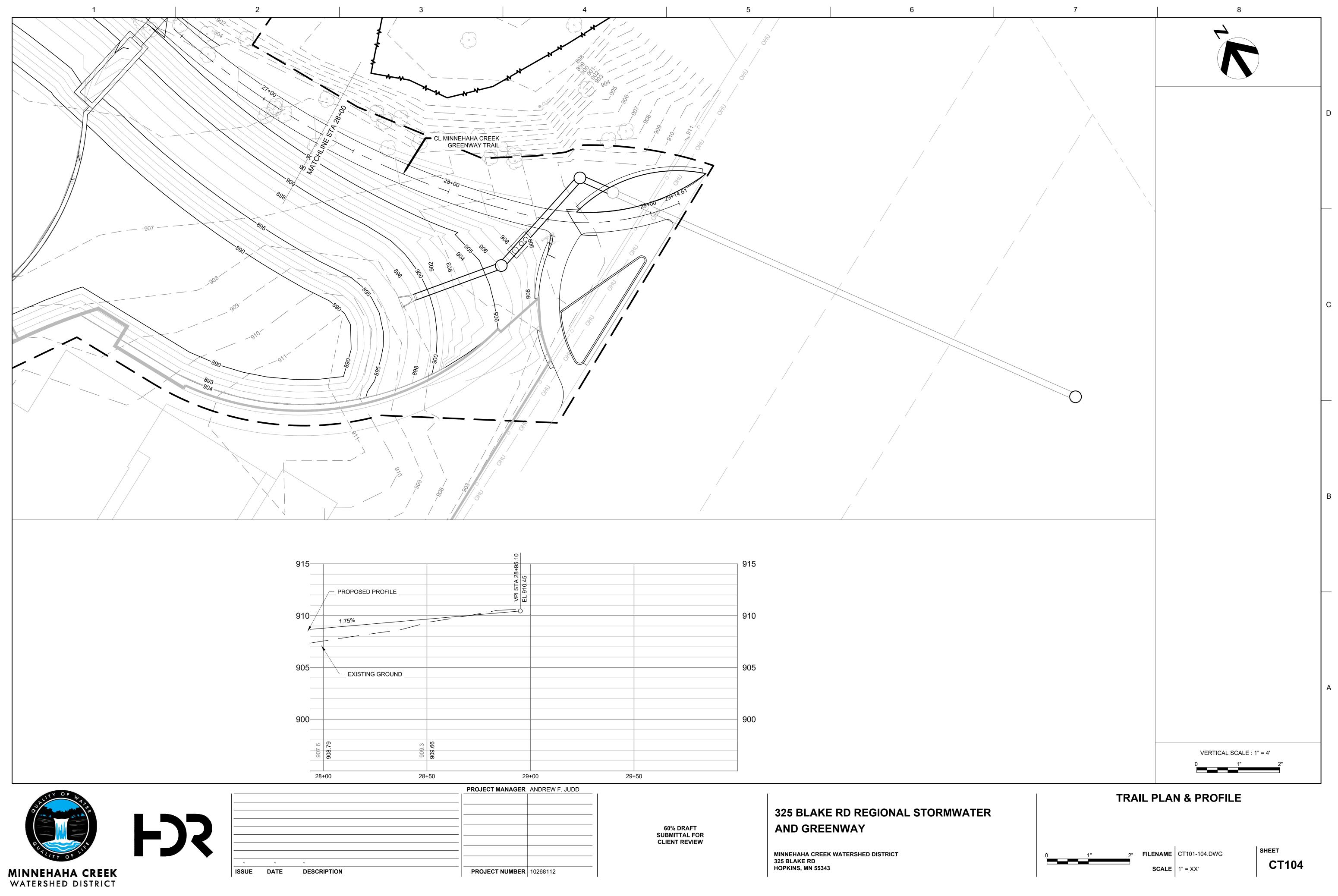
MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343

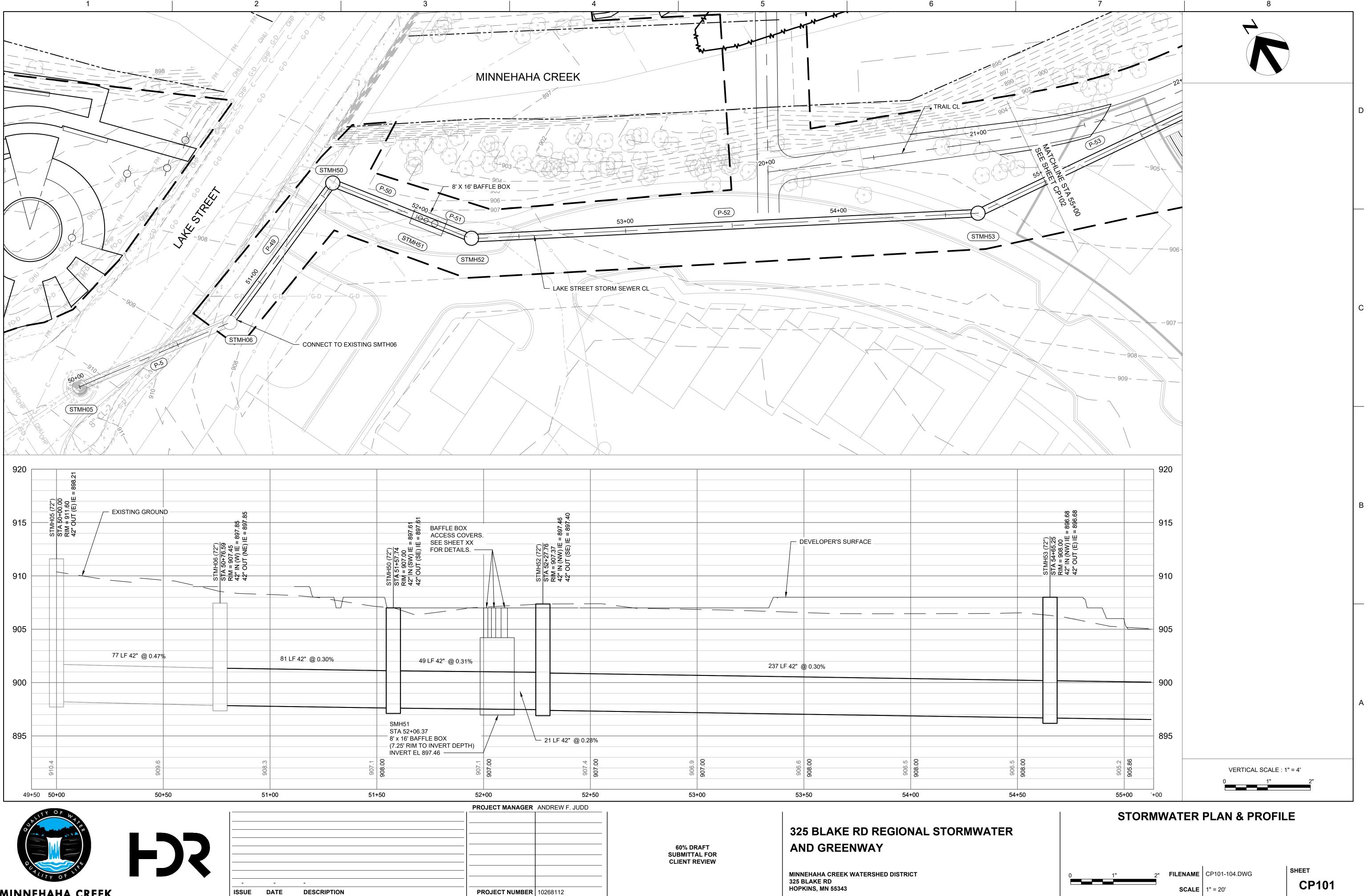




CDE CONTRACTOR CONTRAC		
PROPOSE	D PROFILE	
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PROJECT MANAGER ANDF	EW F. JUDD	60% DF SUBMITT CLIENT F
PROJECT NUMBER 10268	112	



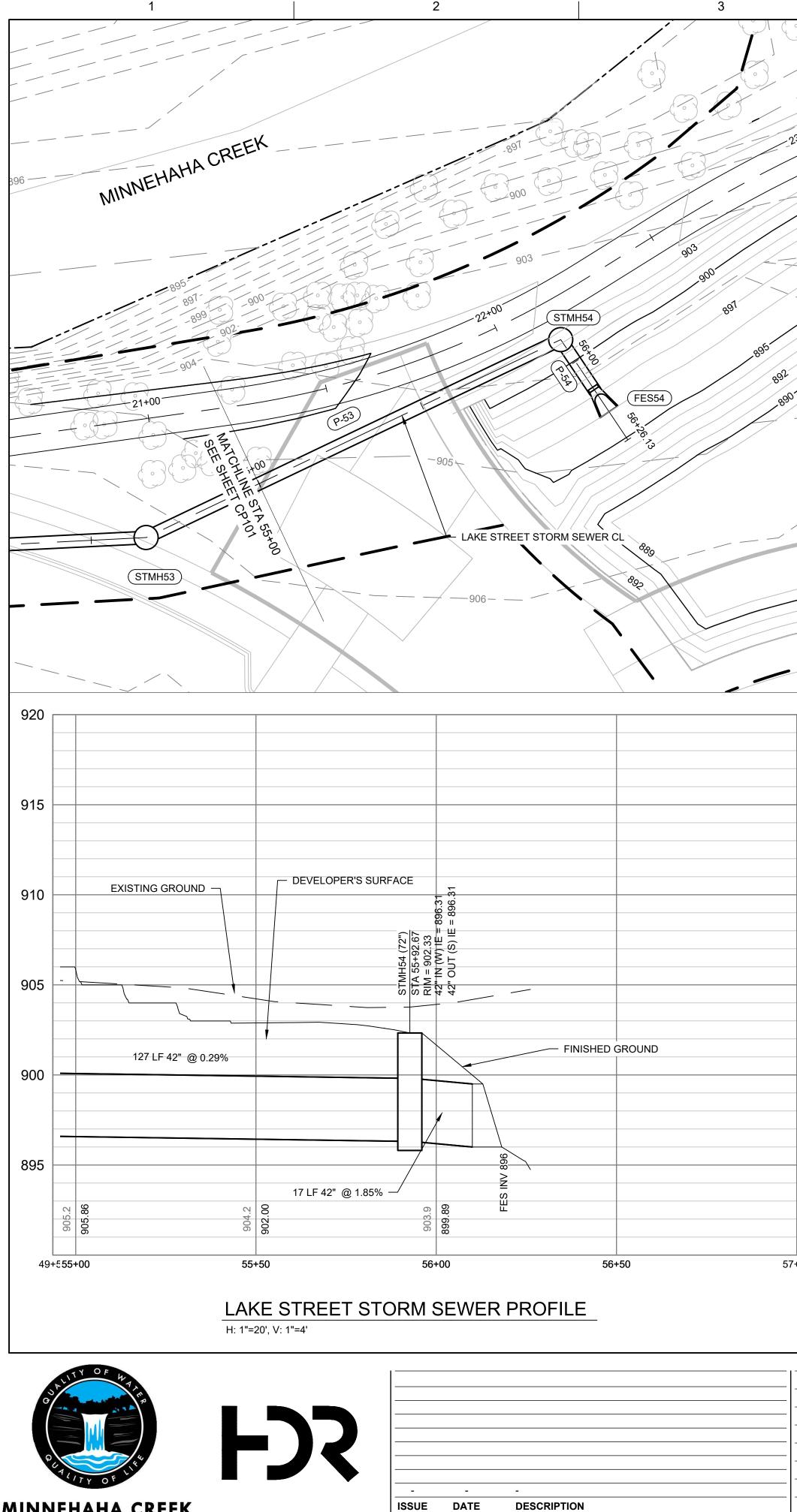




DESCRIPTION

PROJECT NUMBER	10268112

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						221	5 BLAKE RD REG		NAL STORM	
				60% DR	AFT		ID GREENWAY			



DESCRIPTION

PROJECT MANAGER	ANDREW F. JUDD
PROJECT NUMBER	10268112

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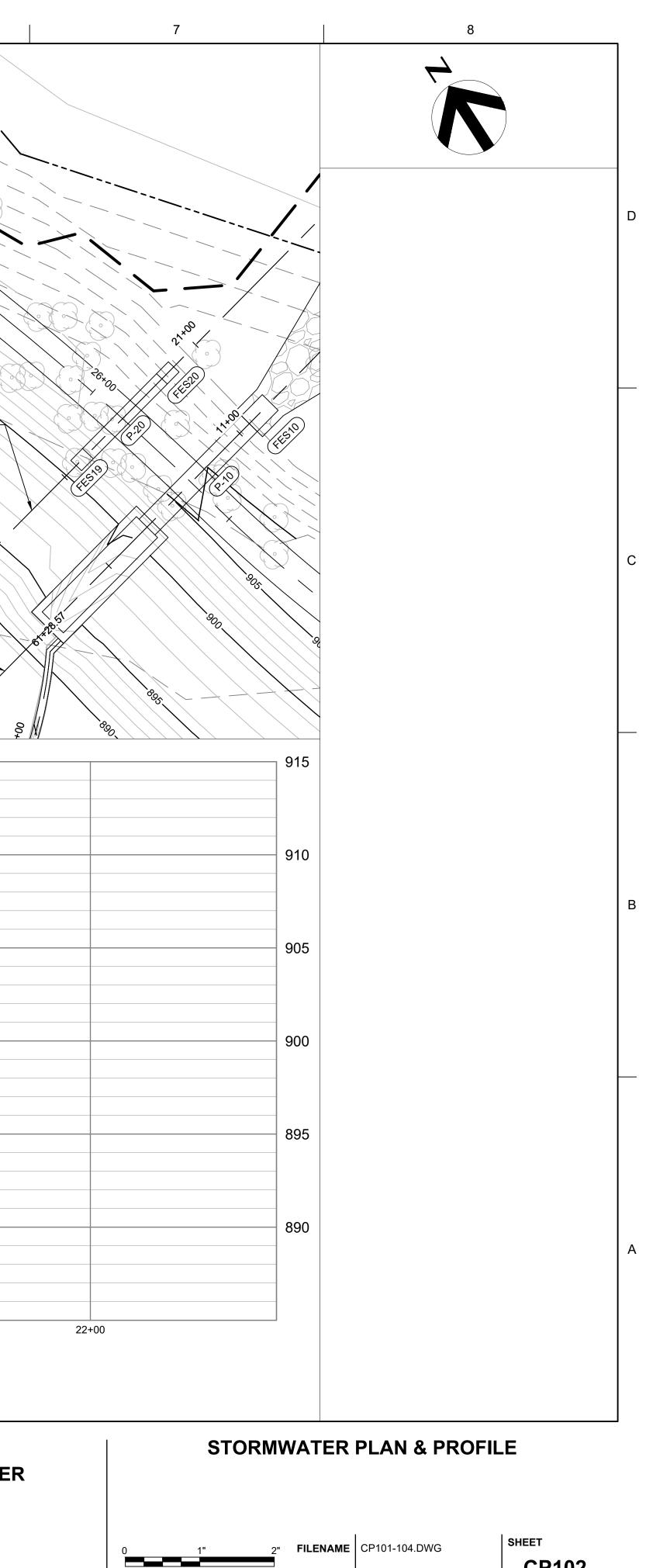
325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343

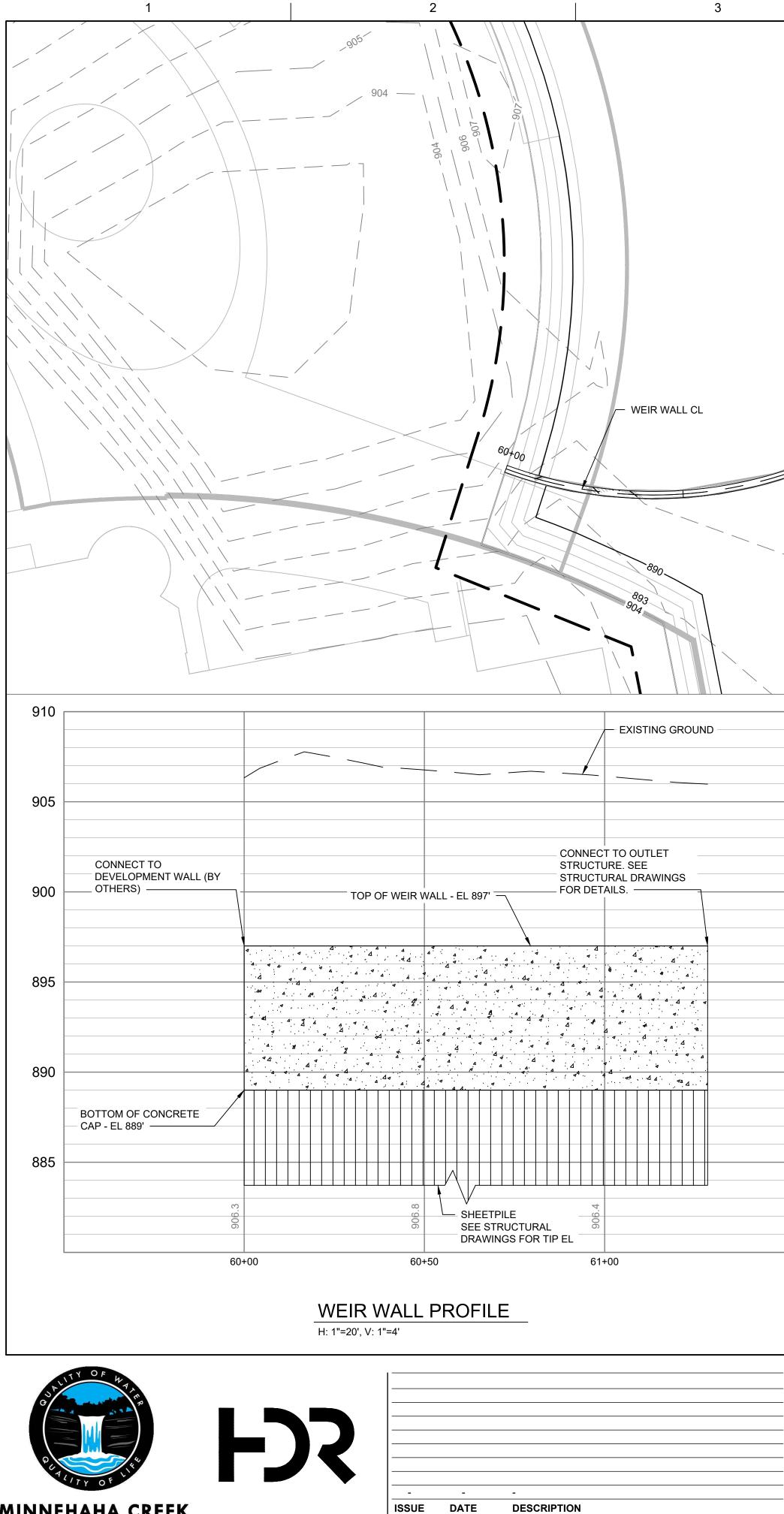
AUXILIARY OVERFLOW PROFILE H: 1"=20', V: 1"=4'

OUTLET STRUCTURE CL 920 915 915 910 EXISTING GROUND _____ 910 905 PLACE APRON WITH SAFETY BARS PLACE APRON WITH /វដ្-_29 LF 1.5'H X 4'W RC _____ BOX CULVERT @ 0% -905 900 FINISHED GROUND 900 895 — MNDOT CATEGORY 76 HP-TRM 895 890 S စ္တ 57+00 20+00 20+50 21+00 21+50

TRAIL CL AUXILIARY OVERFLOW CL



CP102



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	10+00	AUXILIARY OVERFLOW CL	5 FES19 P-20	P-10		MININE HAHA Che	21+65.86	
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905	905					FINISHE	D GROUND	FINISHED GROUND
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895	895				40 LF 4' CULVEF	'H X 6'W RC BOX		
890	890				PLAC	P WALL	MNDOT CLASS	ш
385	885			- WEIR WALL	ST	OTTOM OF OUTLET RUCTURE - EL 889.0'	WITH 9" FILTER	
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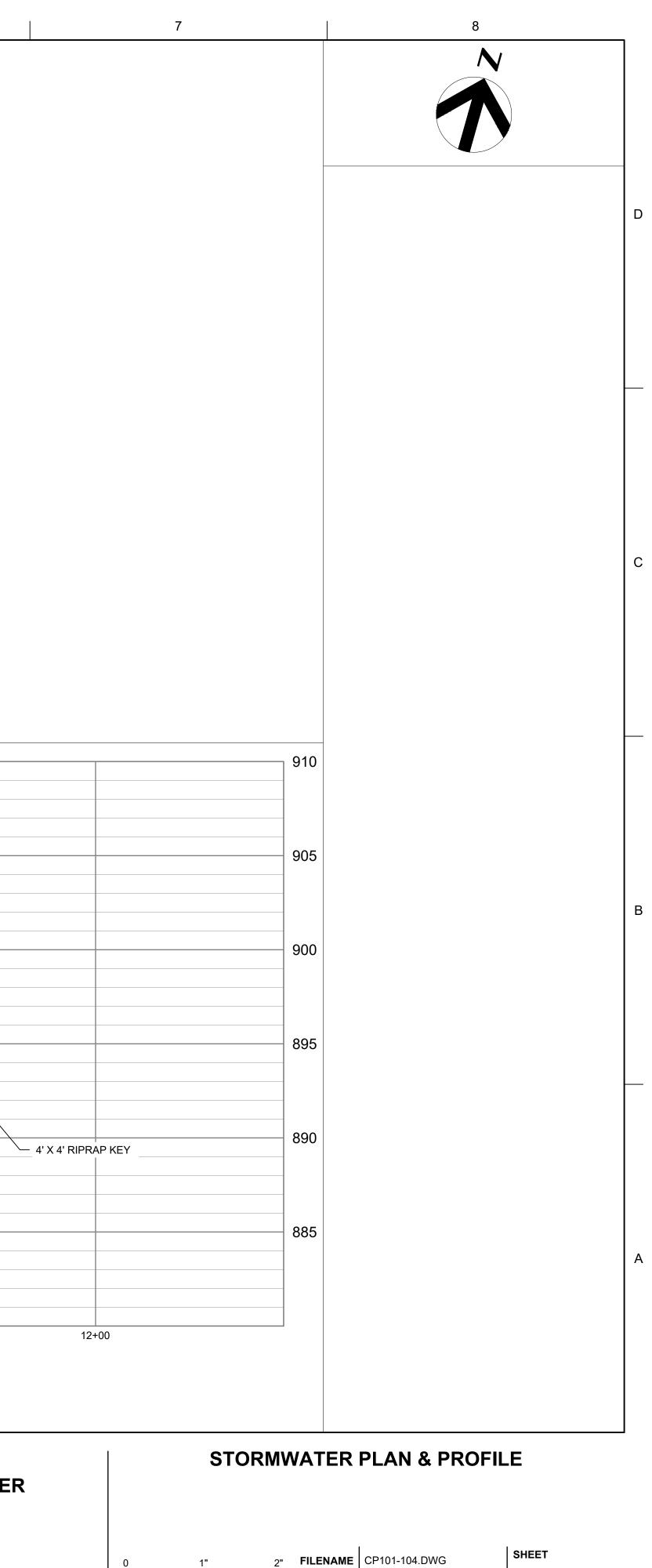
PROJECT MANAGER ANDREW F. JUDD

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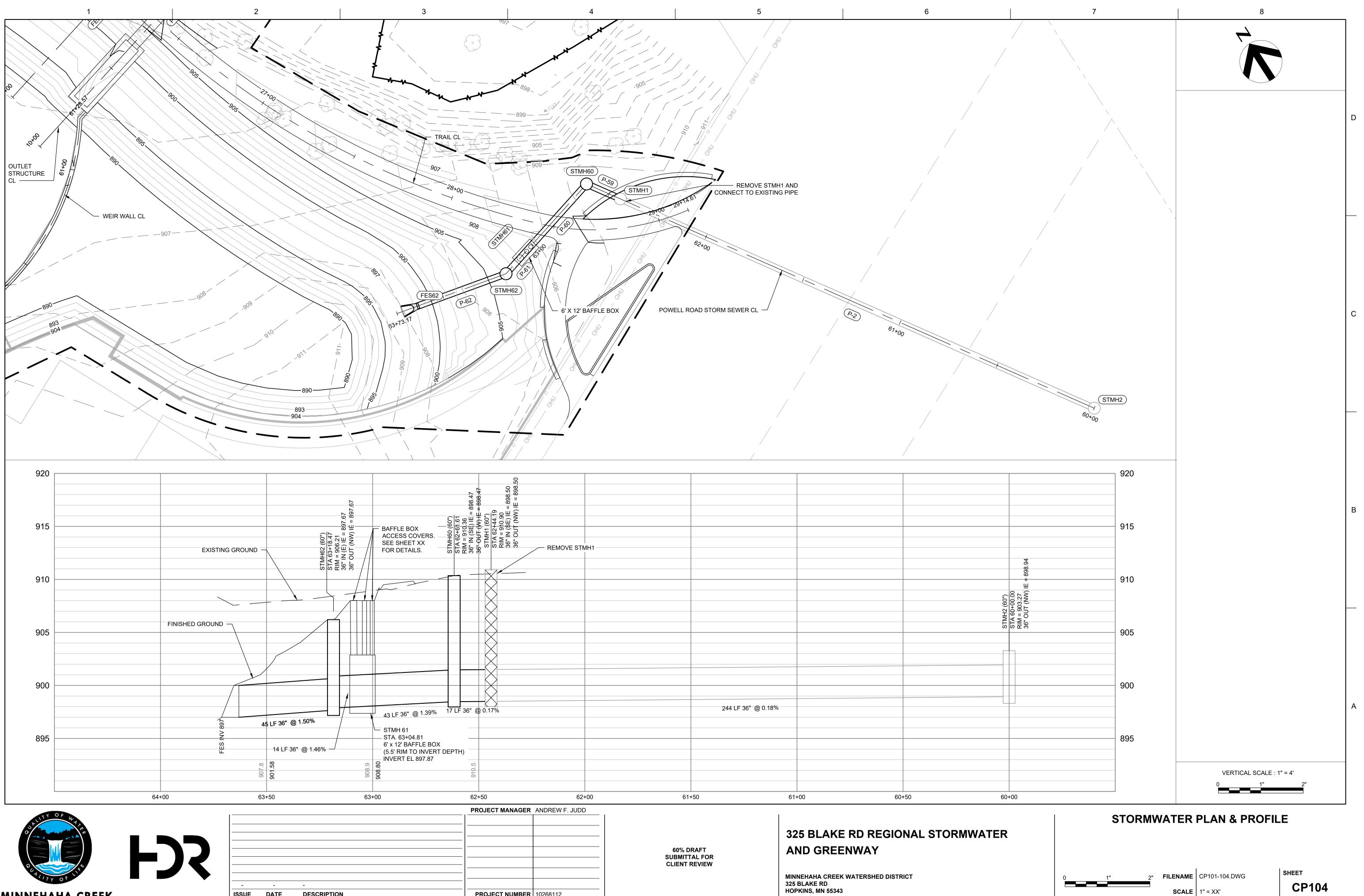
325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343



SCALE 1" = 20'

CP103

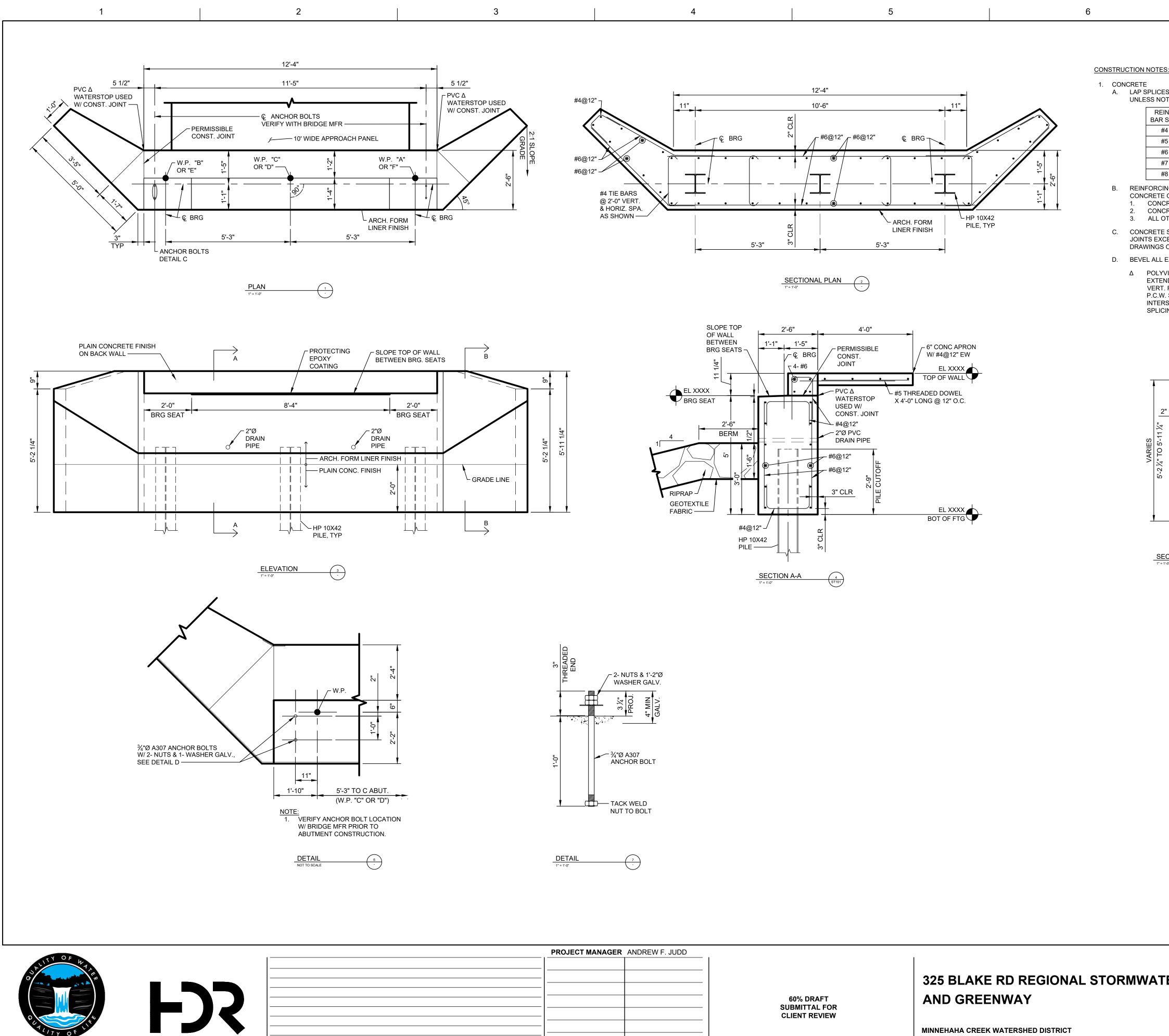


ISSUE DATE DESCRIPTION

PROJECT NUMBER	10268112

SCALE 1" = XX'

36" IN (SE) IE = 898.47 36" OUT (W) IE = 898.47 STMH1 (60") STA 62+44.19 RIM = 910.90 36" IN (SE) IE = 898.50 36" OUT (NW) IE = 898.50 36" OUT (NW) IE = 898.50				
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" @ 0.17%		244 LF 30 @ 0.10%		
910.5				
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62+50 62	+00 61+	⊧50 61 [.]	+00 60	+50



DATE DESCRIPTION

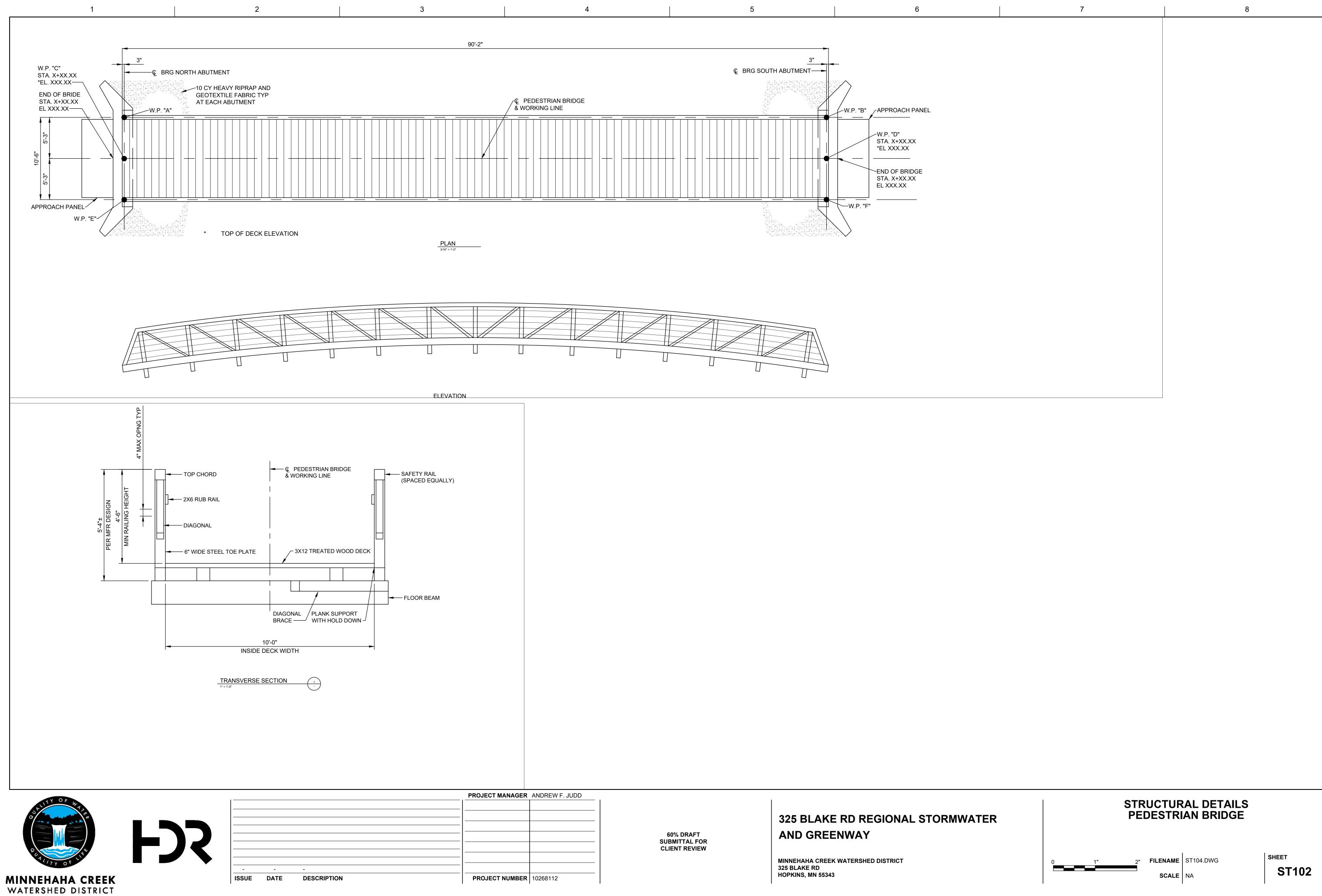
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ISSUE

PROJECT NUMBER 10268112

325 BLAKE RD HOPKINS, MN 55343

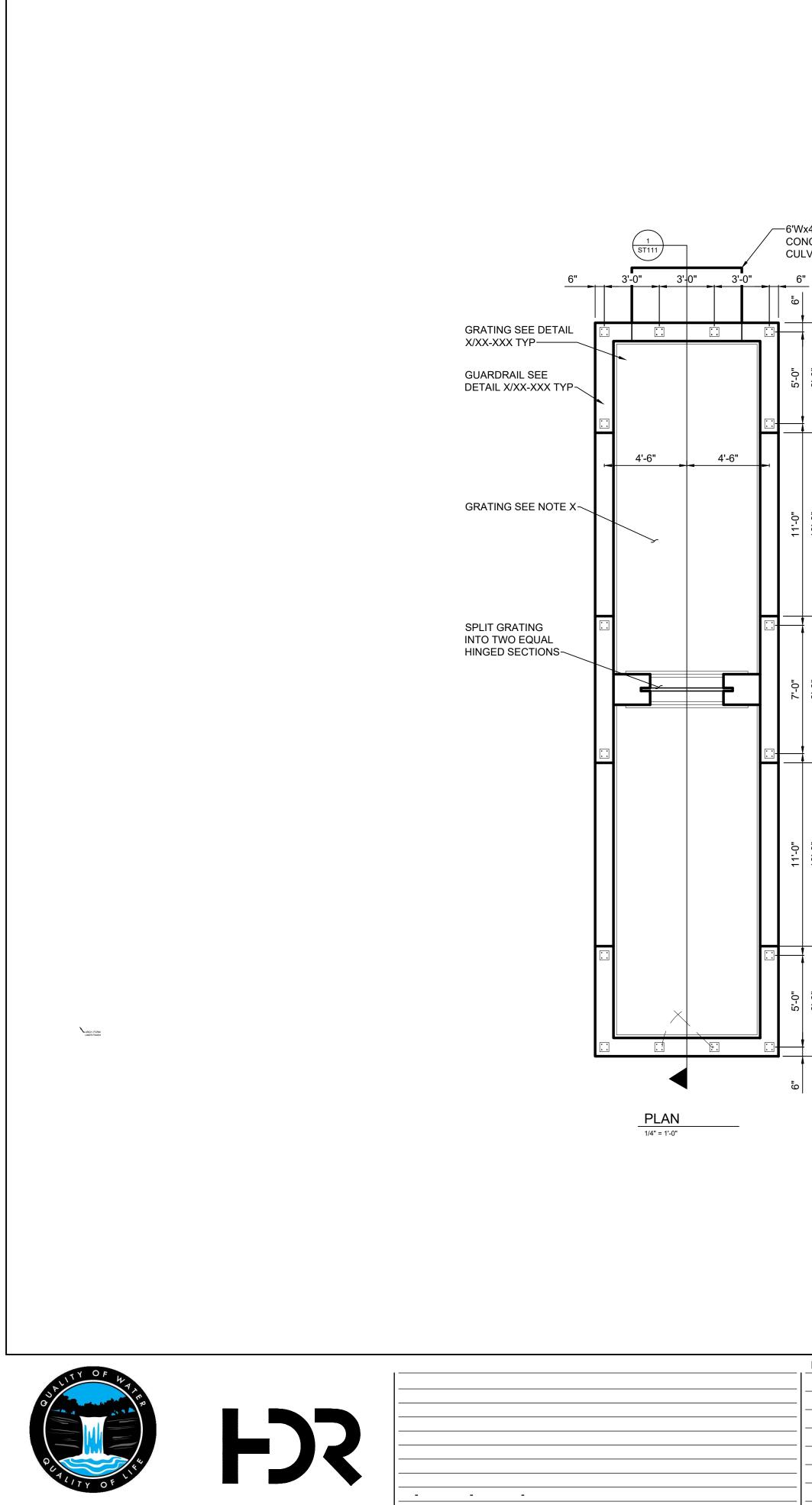
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	90° HOOKS SH	ALL BE AS S	SHOWN BELOW						
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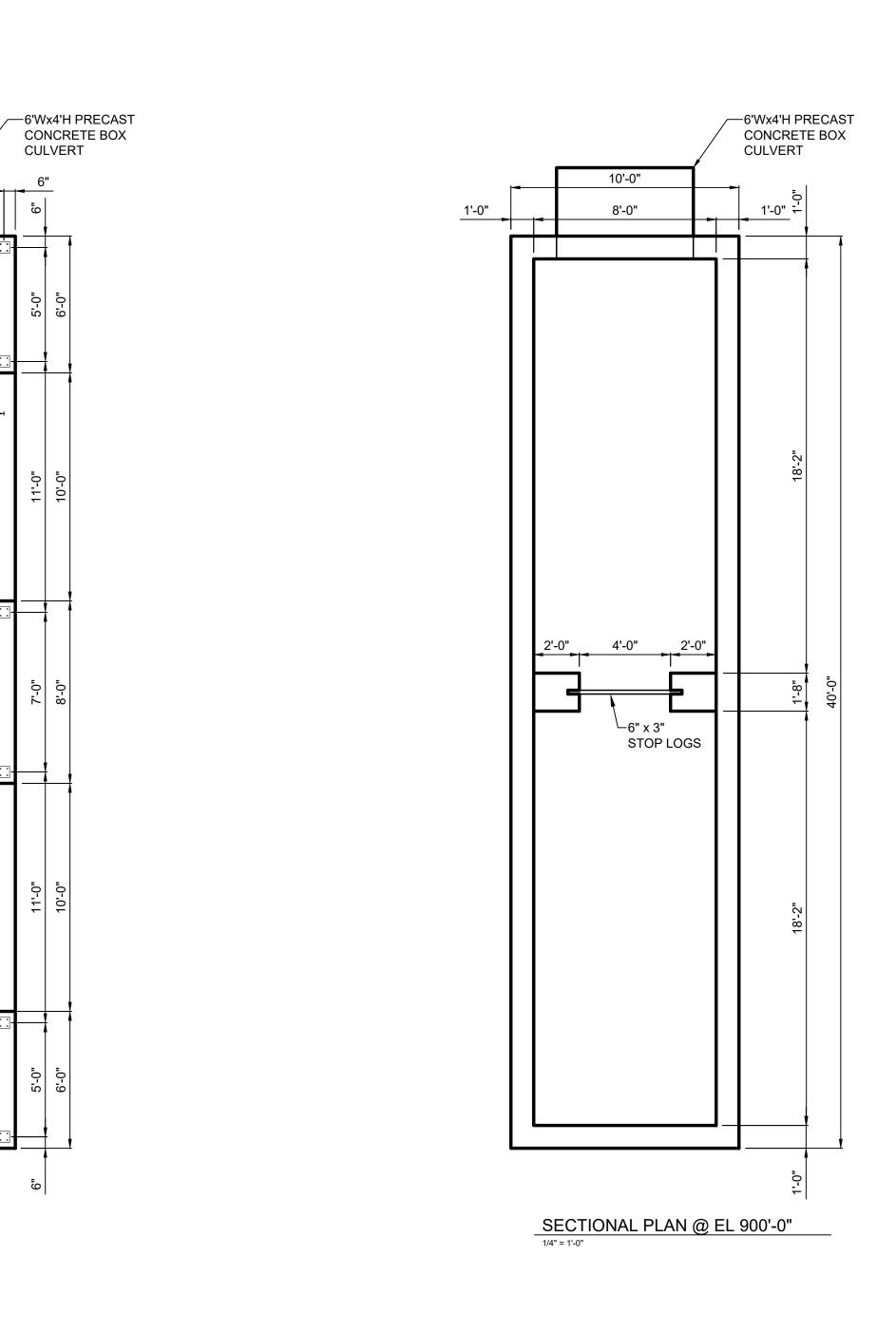
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MINNEHAHA CREEK WATERSHED DISTRICT

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ISSUE DATE DESCRIPTION



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PROJECT MANAGER	ANDREW F. JUDD
PROJECT NUMBER	10268112

60% DRAFT SUBMITTAL FOR CLIENT REVIEW

325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343 6

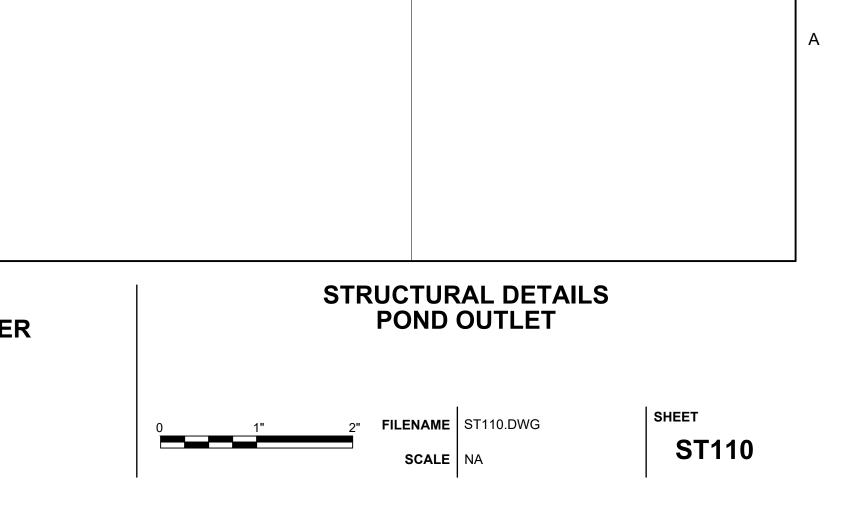
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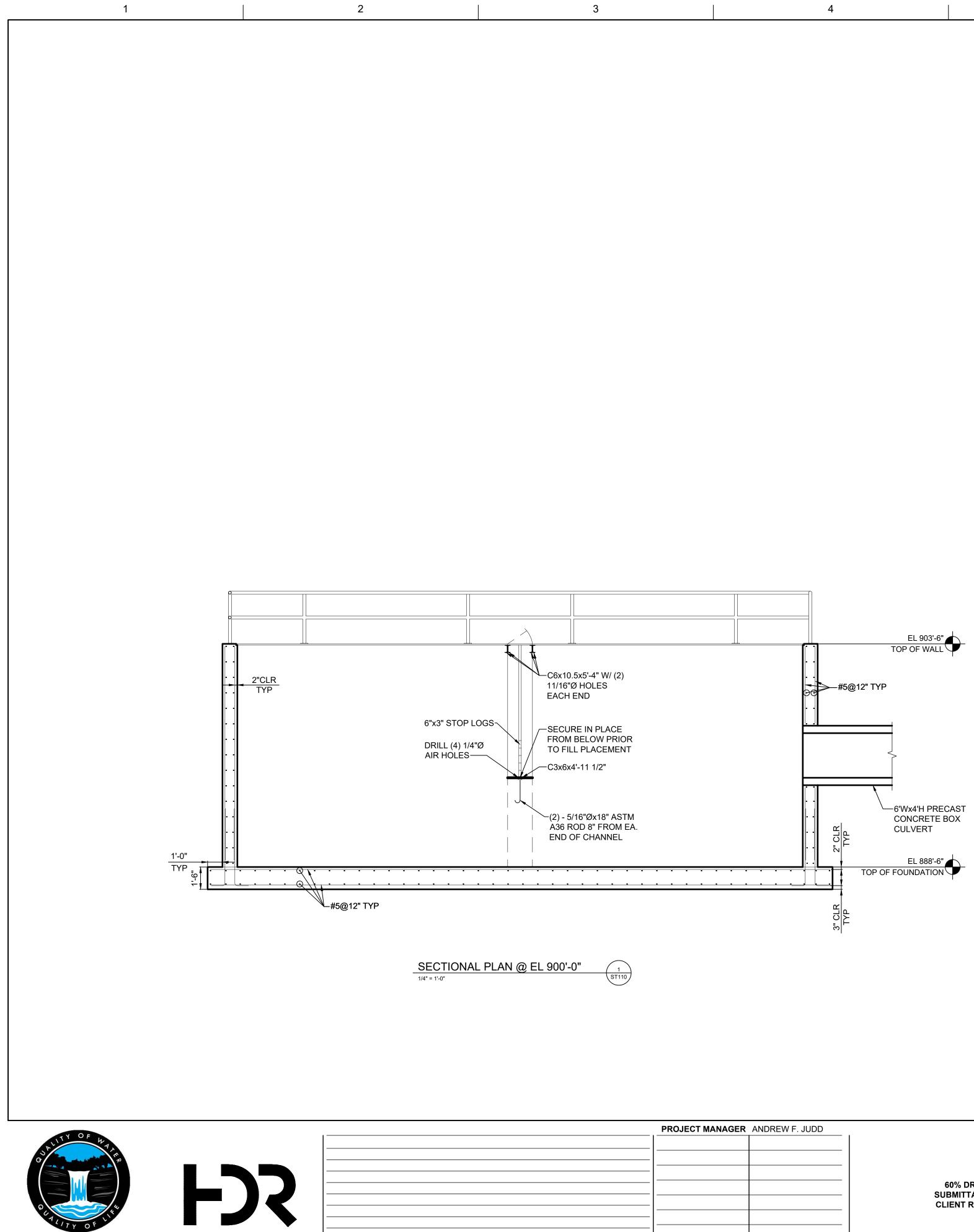
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ISSUE DATE DESCRIPTION

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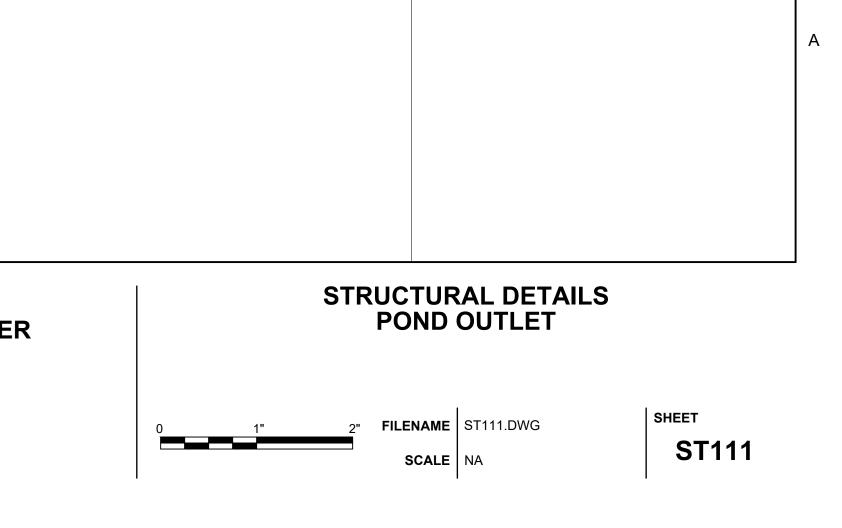
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PROJECT NUMBER	10268112

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325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

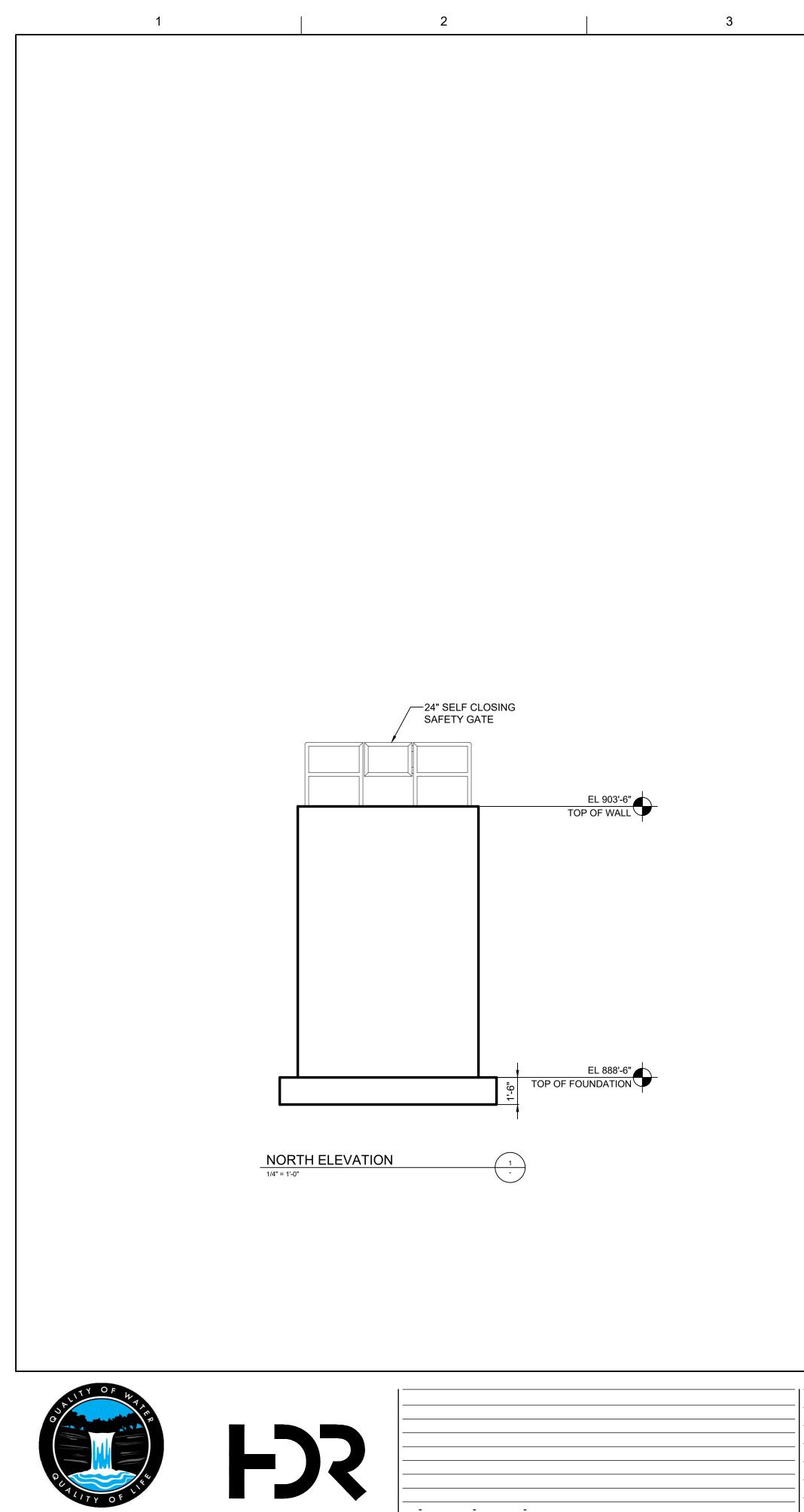
MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343



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ISSUE DATE DES

DESCRIPTION

PROJECT MANAGER ANDREW F. JUDD		
PROJECT NUMBER	10268112	

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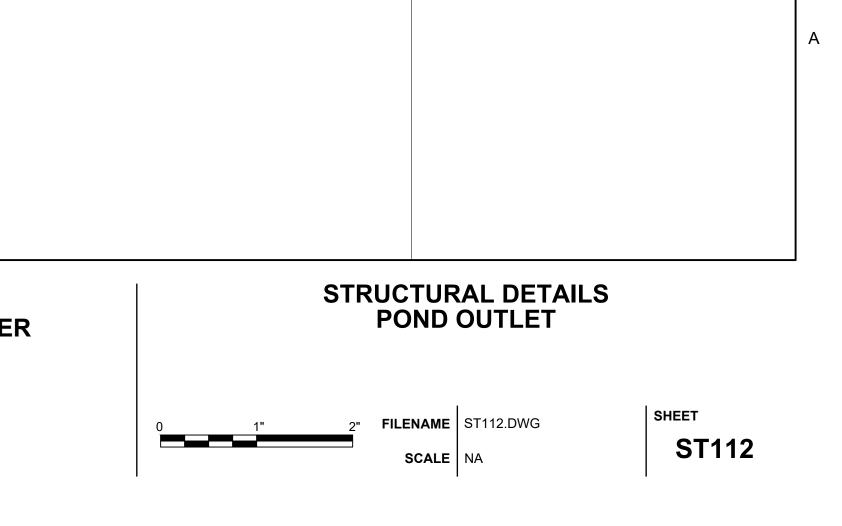
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325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

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MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343

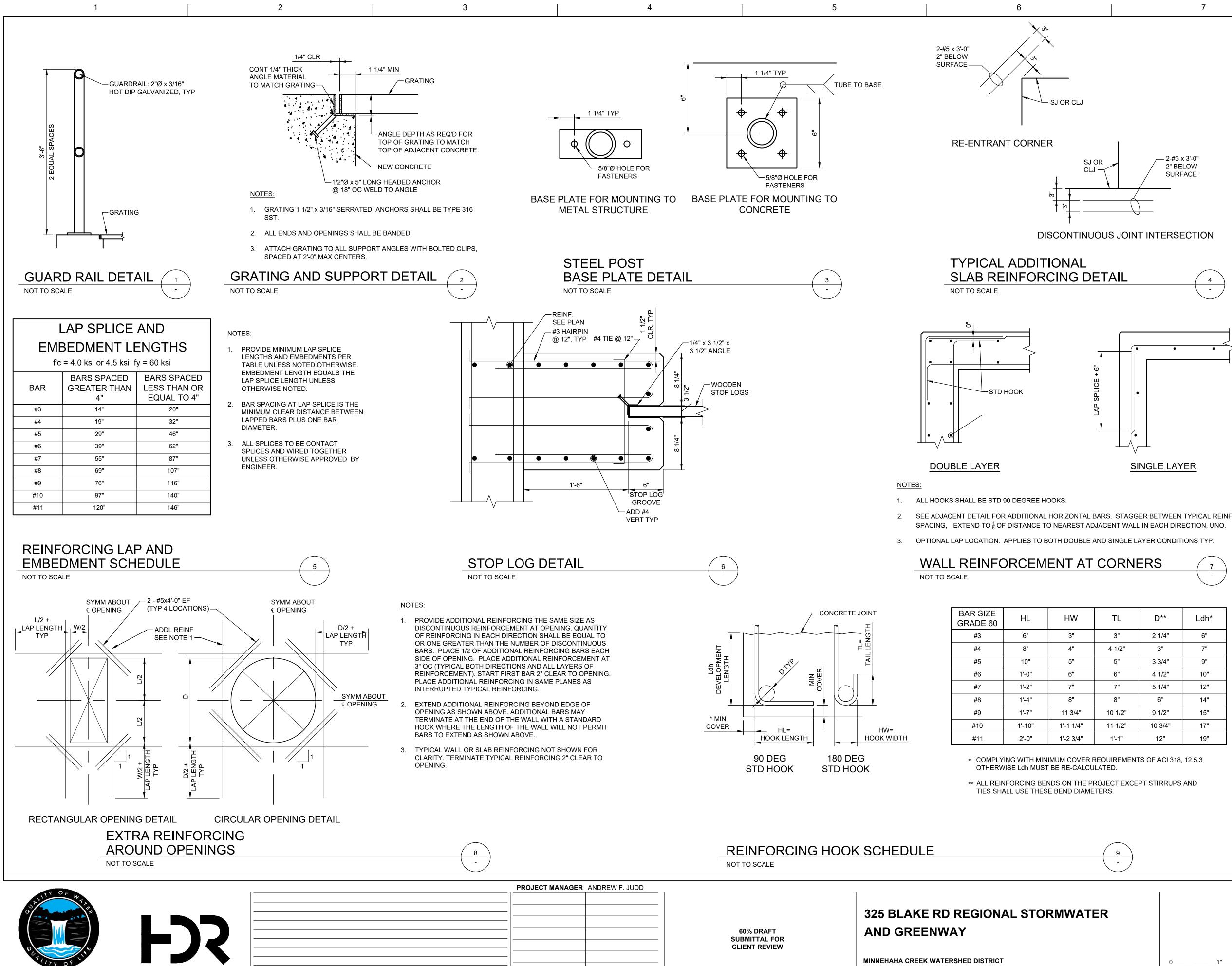


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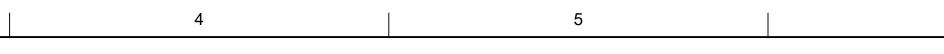
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ISSUE



- SPACING, EXTEND TO $\frac{1}{5}$ OF DISTANCE TO NEAREST ADJACENT WALL IN EACH DIRECTION, UNO.

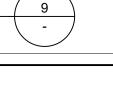
WALL REINFORCEMENT AT CORNERS

BAR SIZE GRADE 60	HL	HW	TL	D**	Ldh*
#3	6"	3"	3"	2 1/4"	6"
#4	8"	4"	4 1/2"	3"	7"
#5	10"	5"	5"	3 3/4"	9"
#6	1'-0"	6"	6"	4 1/2"	10"
#7	1'-2"	7"	7"	5 1/4"	12"
#8	1'-4"	8"	8"	6"	14"
#9	1'-7"	11 3/4"	10 1/2"	9 1/2"	15"
#10	1'-10"	1'-1 1/4"	11 1/2"	10 3/4"	17"
#11	2'-0"	1'-2 3/4"	1'-1"	12"	19"

- * COMPLYING WITH MINIMUM COVER REQUIREMENTS OF ACI 318, 12.5.3 OTHERWISE Ldh MUST BE RE-CALCULATED.
- ** ALL REINFORCING BENDS ON THE PROJECT EXCEPT STIRRUPS AND TIES SHALL USE THESE BEND DIAMETERS.

PROJECT NUMBER 10268112

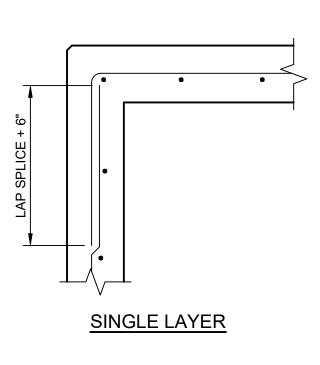
325 BLAKE RD HOPKINS, MN 55343



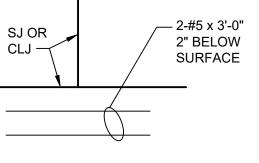
STRUCTURAL DETAILS **POND OUTLET**







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1. <u>SCOPE</u> THE NOTES ON THIS SHEET AND THE STANDARD STRUCTURAL DETAILS ARE GENERAL AND APPLY TO THE ENTIRE PROJECT WHETHER SPECIFICALLY CALLED OUT OR NOT, EXCEPT WHERE THERE	G10. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS AND ELEVATIONS OF EXISTING CONSTRUCTION AS REQUIRED TO COORDINATE NEW CONSTRUCTION. SUBMIT REQUIRED CHANGES FOR APPROVAL.	S1. DESIGN STRENGTHS: STAINLESS STEEL: WIDE FLANGE AND TEES: Fy=50 KSI	
ARE SPECIFIC INDICATIONS TO THE CONTRARY ON STRUCTURAL SHEETS. IF THERE ARE QUESTIONS, THEY SHALL BE SUBMITTED TO THE STRUCTURAL ENGINEER AND ANSWERED IN WRITING PRIOR TO CONSTRUCTION. 2. APPLICABLE SPECIFICATIONS AND CODES	G11. CONTRACTOR TO SUBMIT FOR REVIEW ALL EQUIPMENT SIZES, OPERATING WEIGHTS, VIBRATION FORCES, SUPPORT LOCATIONS, ALONG WITH ANY FLOOR OPENINGS, NOTCHES, AND RECESSES REQUIRED BY SUCH EQUIPMENT. CONCRETE SUPPORT PADS AND/OR FRAMING REQUIRED TO SUPPORT SAID EQUIPMENT SHALL NOT BE FABRICATED AND PLACED UNTIL THE CONCRETE SUPPORT PADS AND/OR FRAMING IS APPROVED TO SUPPORT THE EQUIPMENT.	PIPES: HSS: ALL OTHER PLATES AND SHAPES: 52. DIMENSIONS: Fy=35 KSI Fy=36 KSI Fy=36 KSI	
 <u>APPLICABLE SPECIFICATIONS AND CODES</u> A. 2015 MINNESOTA STATE BUILDING CODE WITH APPLICABLE EDITIONS OF THE CODE REFERENCED STANDARDS. B. ACI 318 	G12. GRANULAR BEDDING UNDER OUTLET PIPE SHALL BE FIRMLY COMPACTED FINE FILTER AGGREGATE GRADED IN ACCORDANCE WITH MNDOT SPEC 3149.2J.	TO CENTERLINES OF COLUMNS AND BEAMS, TOP SURFACES OF BEAMS AND TUBES AND BACKS OF CHANNELS AND ANGLES UNO. S3. ELEVATIONS:	
 <u>DESIGN CRITERIA</u> APPLIES TO ALL STRUCTURES (UNLESS NOTED OTHERWISE) A. DEAD LOAD: 	G13. COMPACT EMBANKMENT MATERIALS USING THE SPECIFIED DENSITY METHOD TO 100% STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D698) AROUND STRUCTURE. COMMON BORROW - EMBANKMENT SHALL HAVE MOISTURE CONTENT BETWEEN 1% BELOW OPTIMUM AND 3% ABOVE OPTIMUM MOISTURE CONTENT. THE CONTRACTOR IS FULLY RESPONSIBLE FOR PROVIDING THE WORK AND MEETING MOISTURE CONTENT AND DENSITY REQUIREMENTS.	TOP OF STEEL REFERS TO TOP SURFACE OF MEMBER OR FLANGE UNO. S4. WHEN FILLET WELD SIZE IS NOT INDICATED, PROVIDE MAXIMUM WELD SIZE BASED ON MATERIAL THICKNESS IN ACCORDANCE WITH AISC SPECIFICATIONS.	
A.1. ACTUAL TRIBUTARY STRUCTURE WEIGHT B. LIVE LOAD: B.1. WALKWAYS, STAIRS, GRATING: 60 PSF C. WIND:	<u>CONCRETE</u> C1. DESIGN STRENGTHS:	 S5. ALL BOLTED STRUCTURAL CONNECTIONS ARE BEARING TYPE CONNECTIONS UNLESS OTHERWISE SPECIFIED TO BE SLIP-CRITICAL. PROVIDE LOAD INDICATING WASHERS AT SLIP-CRITICAL CONNECTIONS. S6. CONFORM TO AISC 360, STEEL CONSTRUCTION MANUAL. 	
C.1. BASIC WIND SPEED (ULTIMATE): 105 MPH C.2. EXPOSURE: C C.3. RISK CATEGORY: III III III III	CONCRETE (28-DAY COMPRESSIVE STRENGTH)GENERAL USE STRUCTURAL CONCRETE:f'c = 4,500 PSIREINFORCING:fy = 60,000 PSILOW STRENGTH CONCRETE FILL:f'c = 3,000 PSI	<u>GRATING</u> G1. FABRICATE GRATING IN ACCORDANCE WITH NAAMM MBG 531.	
PROJECT AND IS THE BASIS OF THIS STRUCTURAL DESIGN: GEOTECHNICAL FIRM NAME: ADDRESS:	MN/DOT MIX DESIGN: 3B44 AIR ENTRAINMENT: 6.5% +/- 1.5% NOMINAL MAXIMUM AGGREGATE SIZE: 1 1/2"	G2. BEARING BARS: A. RECTANGULAR 1-1/4 X 3/16 IN UNLESS SHOWN OTHERWISE ON DRAWINGS. B. MAXIMUM 1-3/16 IN OC SPACING.	
REPORT DATE: REPORT NUMBER: 5. <u>SAFETY</u>	C2. CONCRETE COVER UNLESS OTHERWISE NOTED, PROVIDE CONCRETE COVER FOR REINFORCING AS FOLLOWS:	G3. CROSS BARS: A. WELDED, SWAGED OR PRESSURE LOCKED TO BEARING BARS. B. MAXIMUM 4 IN OC SPACING. G4. TOP EDGES OF BARS: SERRATED OR GROOVED.	
SAFETY AND STRUCTURE STABILITY DURING CONSTRUCTION ARE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. STRUCTURES HAVE BEEN DESIGNED TO RESIST THE DESIGN LIVE LOADS ONLY AS A COMPLETED STRUCTURE.	CONCRETE DEPOSITED AGAINST EARTH: 3" ALL OTHER: 2" SEE DRAWINGS FOR EXCEPTIONS C3. SEE SPECIFICATIONS FOR REINFORCING PLACEMENT REQUIREMENTS.	G5. HINGED GRATING SECTIONS: NOT WIDER THAN 2 FT AND NOT MORE THAN 35 LBS EACH. G6. FINISH: A. HOT DIP GALVANIZED IN ACCORDANCE WITH ASTM A123.	
5. <u>OPENINGS</u> OPENINGS FOR PIPES, DUCTS, CONDUITS, ETC. ARE NOT ALL SHOWN ON THE STRUCTURAL DRAWINGS. COORDINATE AND PROVIDE OPENINGS AS REQUIRED TO ACCOMMODATE ALL WORK SHOWN OR SPECIFIED IN THE CONTRACT POOL MENTS AND OTHER WISE DEDUIDED FOR THE ENDINGLING OF A FUNCTIONALLY.	C4. REFER TO OTHER DISCIPLINE DRAWINGS PRIOR TO CONSTRUCTION FOR EMBEDDED ITEMS AND PENETRATIONS NOT SHOWN ON STRUCTURAL DRAWINGS. AS REQUIRED TO ACCOMMODATE ALL WORK SHOWN OR SPECIFIED IN THE CONTRACT DOCUMENTS AND OTHERWISE REQUIRED FOR THE FURNISHING	 B. CLIPS AND BOLTS: STAINLESS STEEL OR GALVANIZED. C. SEAT ANGLES: GALVANIZED STEEL. G7. ENDS AND PERIMETER EDGES: BANDED. 	
THE CONTRACT DOCUMENTS AND OTHERWISE REQUIRED FOR THE FURNISHING OF A FUNCTIONALLY COMPLETE PROJECT. REINFORCE AROUND OPENINGS PER STANDARD STRUCTURAL DETAILS UNLESS OTHERWISE SHOWN. 7. <u>SPECIAL INSPECTIONS</u>	OF A FUNCTIONALLY COMPLETE PROJECT. REINFORCE AROUND OPENINGS PER STANDARD STRUCTURAL DETAILS UNLESS OTHERWISE SHOWN. C5. PROVIDE 3/4" CHAMFERS AT ALL EXPOSED EDGES UNLESS NOTED OTHERWISE. NOT ALL CHAMFERS ARE SHOWN ON DRAWINGS.	G8. PROVIDE JOINTS AT OPENINGS BETWEEN INDIVIDUAL GRATING SECTIONS. G9. FABRICATE GRATING SO THAT BEARING BARS AND CROSS BARS IN ADJACENT SECTIONS ARE ALIGNED.	
SPECIAL INSPECTIONS ARE REQUIRED IN ACCORDANCE WITH CHAPTER 1 AND CHAPTER 17 OF THE IBC. PAYMENT FOR THESE INSPECTIONS IS NOT THE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR SHALL PROVIDE FOR FULL ACCESS TO THE WORK BY THE SPECIAL INSPECTOR AND SHALL PROVIDE FOR THESE INSPECTIONS IN HIS CONSTRUCTION SCHEDULE IN ACCORDANCE	 FIELD ADJUST REINFORCING AT OPENINGS AND EMBEDDED ITEMS AS INDICATED. ANCHOR BOLTS NOT SPECIFIED ON THE DRAWINGS SHALL BE DESIGNED AND CERTIFIED BY A REGISTERED PROFESSIONAL ENGINEER, RETAINED BY THE CONTRACTOR, IN ACCORDANCE WITH 	G10. ANCHOR GRATING WITH SADDLE CLIPS AND 1/4" SELF-TAPPING BOLTS A. MAXIMUM SPACING OF 2'-0" WITH MINIMUM OF (2) PER SIDE. <u>GUARD RAILING</u>	
WITH THE SPECIFICATIONS. ALL ELEVATIONS REFER TO NAVD88. <u>STANDARD DETAILS</u>	APPLICABLE PROJECT AND CODE REQUIREMENTS. SUBMIT AS A SHOP DRAWING FOR REVIEW AND APPROVAL BY THE CONTRACTING OFFICER. COORDINATE LOCATION, SIZE AND EMBEDMENT PRIOR TO CASTING CONCRETE.	GR1. CUSTOM FABRICATE PIPE RAILINGS TO DIMENSIONS AND PROFILES SHOWN ON DRAWINGS. GR2. GUARD RAILS: A. TOP RAILS AND INTERMEDIATE RAILS: SCHEDULE 40, 2" IN NOMINAL DIAMETER PIPE.	
THE STANDARD DETAILS DEPICT TYPICAL DETAILING TO BE USED ON THIS PROJECT. IF CONDITIONS ARE NOT EXPLICITLY SHOWN ON THE DRAWINGS THEY SHALL BE MADE SIMILAR TO THE STANDARD DETAILS. OBTAIN APPROVAL OF ENGINEER IN WRITING FOR SIMILAR CONDITIONS PRIOR TO CONSTRUCTION.	 C8. ABSOLUTELY NO WELDING OF REINFORCING BARS OR TORCHING TO BEND REINFORCING BARS SHALL BE ALLOWED WITHOUT SPECIFIC APPROVAL FROM THE STRUCTURAL ENGINEER. C9. ALL POST-INSTALLED ADHESIVE ANCHORS INDICATED IN THE STRUCTURAL DOCUMENTS SHALL COMPLY WITH APPENDIX D OF ACI 318 AND CHAPTER 19 OF THE IBC. ALL ADHESIVE ANCHORS SHALL HAVE THE ICC REPORT SHOWING EQUIVALENT LOAD CAPACITY. SUBMIT AND INSTALL PER THE ICC EVALUATION REPORT. 	 B. VERTICAL POSTS: SCHEDULE 80, 2" IN NOMINAL DIAMETER PIPE. GR3. SPACE VERTICAL POSTS AS REQUIRED BY LOADING REQUIREMENTS BUT NOT MORE THAN 4 FT OC. AVOID LOCATING VERTICAL POSTS AT CHANGES IN DIRECTION OF RAILING. A. HOLD VERTICAL POST BACK FROM CORNER AND PROVIDE RADIUSED CORNERS. GR4. BASE PLATE FOR VERTICAL GUARDRAIL POSTS MOUNTED TO TOP OF CONCRETE SURFACE: 	
		 A. 3/8 X 6 X 6 IN SQUARE PLATE WELDED TO THE VERTICAL POST. B. PREDRILLED TO ACCEPT FOUR (4) ANCHORS. GR5. PROVIDE 1/4 X 4 IN HIGH TOE BOARDS AT ELEVATED WALKWAYS. A. CLEARANCE BETWEEN BOTTOM OF TOE BOARD AND WALKING SURFACE SHALL NOT EXCEED 1/4 IN. 	
		GR6. WELDED RAILING FABRICATION: A. ALL WELDING TO BE CONTINUOUS IN ACCORDANCE WITH AWS D1.1. 1. ALL WELDED RAILING JOINTS SHALL HAVE FULL PENETRATION WELDS. B. ALL EXPOSED WELDS TO BE GROUND AND BUFFED SMOOTH AND FLUSH TO MATCH AND	
		BLEND WITH ADJOINING SURFACES. GR7. FIT EXPOSED ENDS OF GUARDRAILS AND HANDRAILS WITH SOLID TERMINATIONS. GR8. INSTALL WEEPS TO DRAIN MOISTURE FROM HOLLOW SECTIONS OF RAILING.	
		 A. DRILL 1/4 IN WEEP HOLE IN RAILINGS CLOSED AT BOTTOM: 1. 1 IN ABOVE WALKWAY SURFACE AT BOTTOM OF POSTS. 2. DRILL HOLE PRIOR TO GALVANIZING. 3. DO NOT DRILL WEEP HOLES IN BOTTOM OF BASE PLATE. 	
		GR9. FINISH: GALVANIZED AFTER FABRICATION. GR10. GUARD RAILING BASE PLATES SHALL BE ANCHORED WITH 1/2 IN DIAMETER HILTI HIT-HY 200 + HIT-Z-R ADHESIVE ANCHORS WITH 4 IN EMBEDMENT.	

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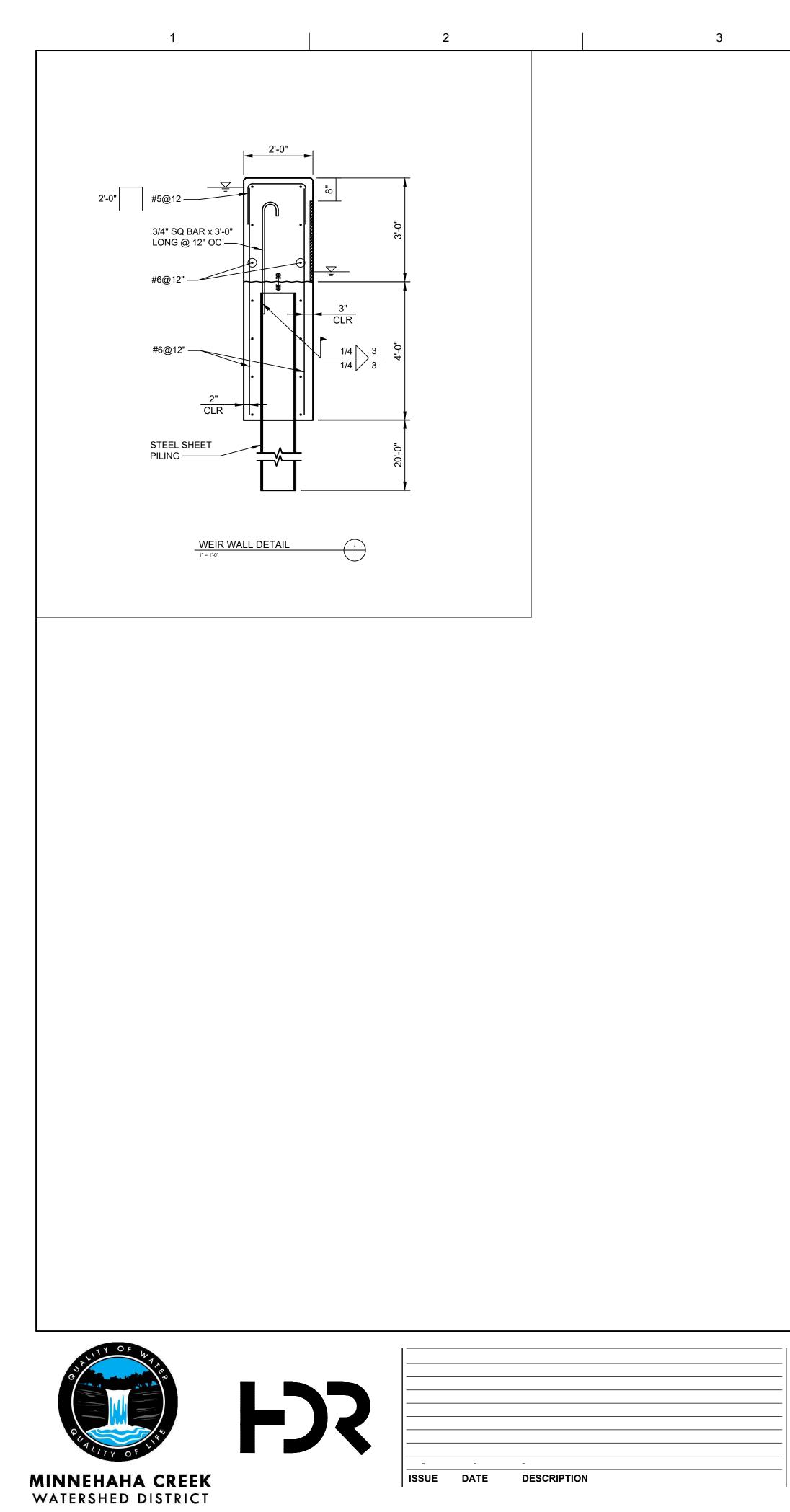
PROJECT MANAGER	ANDREW F. JUDD	
PROJECT NUMBER	10268112	

60% DRAFT SUBMITTAL FOR CLIENT REVIEW

325 BLAKE RD REGIONAL STORMWATH AND GREENWAY

MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343 FILENAME ST114.DWG

SCALE NA



PROJECT MANAGER ANDREW F. JUDD		
PROJECT NUMBER	10268112	

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60% DRAFT SUBMITTAL FOR CLIENT REVIEW

325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

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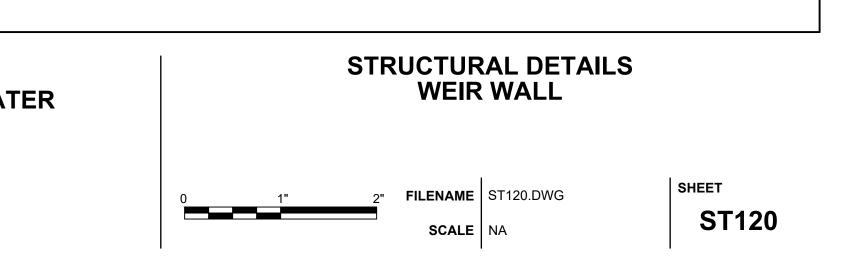
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MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343



SITE AND LANDSCAPE NOTES

SITE PREPARATION NOTES

- 1. CONTRACTOR SHALL INSPECT THE SITE AND BECOME FAMILIAR WITH EXISTING CONDITIONS RELATING TO THE NATURE AND SCOPE OF WORK.
- 2. CONTRACTOR SHALL VERIFY PLAN LAYOUT AND BRING TO THE ATTENTION OF THE LANDSCAPE ARCHITECT DISCREPANCIES WHICH MAY COMPROMISE THE DESIGN OR INTENT OF THE LAYOUT.
- 3. CONTRACTOR SHALL ASSURE COMPLIANCE WITH APPLICABLE CODES AND REGULATIONS GOVERNING THE WORK AND MATERIALS SUPPLIED.
- 4. CONTRACTOR SHALL PROTECT EXISTING ROADS, CURBS/GUTTERS, TRAILS, TREES, LAWNS AND SITE ELEMENTS DURING CONSTRUCTION OPERATIONS. DAMAGE TO SAME SHALL BE REPAIRED AT NO ADDITIONAL COST TO THE OWNER.
- 5. CONTRACTOR SHALL VERIFY ALIGNMENT AND LOCATION OF UNDERGROUND AND ABOVE GRADE UTILITIES AND PROVIDE THE NECESSARY PROTECTION FOR SAME BEFORE CONSTRUCTION BEGINS (MINIMUM 10' CLEARANCE).
- 6. CONTRACTOR SHALL COORDINATE THE PHASES OF CONSTRUCTION AND PLANTING INSTALLATION WITH OTHER CONTRACTORS WORKING ON SITE.
- 7. UNDERGROUND UTILITIES SHALL BE INSTALLED SO THAT TRENCHES DO NOT CUT THROUGH ROOT SYSTEMS OF EXISTING TREES TO REMAIN.
- 8. EXISTING CONTOURS, TRAILS, VEGETATION, CURB/GUTTER AND OTHER ELEMENTS ARE BASED UPON INFORMATION SUPPLIED TO THE LANDSCAPE ARCHITECT BY OTHERS. CONTRACTOR SHALL VERIFY DISCREPANCIES PRIOR TO CONSTRUCTION AND NOTIFY LANDSCAPE ARCHITECT OF SAME.
- 9 HORIZONTAL AND VERTICAL ALIGNMENT OF PROPOSED WALKS, TRAILS OR ROADWAYS ARE SUBJECT TO FIELD ADJUSTMENT REQUIRED TO CONFORM TO LOCALIZED TOPOGRAPHIC CONDITIONS AND TO MINIMIZE TREE REMOVAL AND GRADING. CHANGES IN ALIGNMENT AND GRADES MUST BE APPROVED BY THE LANDSCAPE ARCHITECT PRIOR TO IMPLEMENTATION.
- 10. CONTRACTOR SHALL REVIEW THE SITE FOR DEFICIENCIES IN SITE CONDITIONS WHICH MIGHT NEGATIVELY AFFECT PLANT ESTABLISHMENT, SURVIVAL OR WARRANTY. UNDESIRABLE SITE CONDITIONS SHALL BE BROUGHT TO THE ATTENTION OF THE LANDSCAPE ARCHITECT PRIOR TO COMMENCEMENT OF WORK
- 11. CONTRACTOR IS RESPONSIBLE FOR ONGOING MAINTENANCE OF NEWLY INSTALLED MATERIALS UNTIL TIME OF SUBSTANTIAL COMPLETION. REPAIR OF ACTS OF VANDALISM OR DAMAGE WHICH MAY OCCUR PRIOR TO SUBSTANTIAL COMPLETION SHALL BE THE RESPONSIBILITY OF THE LANDSCAPE CONTRACTOR.
- 12. EXISTING TREES OR SIGNIFICANT SHRUB MASSINGS FOUND ON SITE SHALL BE PROTECTED AND SAVED UNLESS NOTED TO BE REMOVED OR ARE LOCATED IN AN AREA TO BE GRADED. QUESTIONS REGARDING EXISTING PLANT MATERIAL SHALL BE BROUGHT TO THE ATTENTION OF THE LANDSCAPE ARCHITECT PRIOR TO REMOVAL.
- 13. EXISTING TREES TO REMAIN, UPON DIRECTION OF LANDSCAPE ARCHITECT, SHALL BE FERTILIZED AND PRUNED TO REMOVE DEAD WOOD, DAMAGED AND RUBBING BRANCHES.
- 14. CONTRACTOR SHALL PREPARE AND SUBMIT A WRITTEN REQUEST FOR THE SUBSTANTIAL COMPLETION INSPECTION OF LANDSCAPE AND SITE IMPROVEMENTS PRIOR TO SUBMITTING FINAL PAY REQUEST.
- 15. CONTRACTOR SHALL PREPARE AND SUBMIT REPRODUCIBLE AS-BUILT DRAWING(S) OF LANDSCAPE INSTALLATION, IRRIGATION AND SITE IMPROVEMENTS UPON COMPLETION OF CONSTRUCTION INSTALLATION AND PRIOR TO SUBSTANTIAL COMPLETION.
- 16. SYMBOLS ON PLAN DRAWING TAKE PRECEDENCE OVER SCHEDULES IF DISCREPANCIES IN QUANTITIES EXIST. SPECIFICATIONS AND DETAILS TAKE PRECEDENCE OVER NOTES.

SOIL TESTING

- CONTRACTOR SHALL OBTAIN A SOIL SAMPLE(S) FROM PROJECT SITE AND/OR SALVAGED TOPSOIL STOCKPILE AND SUBMIT TO INDEPENDENT TESTING AGENCY. ANALYSIS AND RECOMMENDATIONS FOR (INCLUDING BUT NOT LIMITED TO) MACRONUTRIENTS, MICRONUTRIENTS, COMPOSITION AND SOLUBLE SALTS SHALL BE PROVIDED.
- 2. CONTRACTOR SHALL PROVIDE TWO SERIES OF TESTS: FIRST, PRIOR



3. CONTRACTOR SHALL PROVIDE ANALYSIS RESULTS AND RECOMMENDATIONS TO THE LANDSCAPE ARCHITECT FOR REVIEW AND APPROVAL PRIOR TO SOIL AMENDMENT AND PRIOR TO PLANTING.

GRADING

- ROUGH GRADING AND FINISHED GRADING TO BE DONE BY OTHERS EXCEPT WHERE NOTED.
- 2. GRADING LIMITS ARE DEFINED AS THE JUNCTURE OF PROPOSED GRADE WITH EXISTING GRADE UNLESS NOTED OTHERWISE.
- 3. GRADING LIMITS AND LIMITS OF WORK SHOWN ON PLAN ARE ONLY APPROXIMATE AND MAY BE ADJUSTED IN FIELD BY LANDSCAPE ARCHITECT. WORK OUTSIDE OF THESE LIMITS WILL BE DONE AT LANDSCAPE CONTRACTORS EXPENSE UNLESS DIRECTED BY LANDSCAPE ARCHITECT OR OWNER IN WRITING.
- 4. FILL/CUT AS NECESSARY TO PROVIDE A 1% MINIMUM GRADE AWAY FROM BUILDINGS WITHIN LIMITS OF CONSTRUCTION.
- 5. SALVAGE TOPSOIL FROM THE EARTHWORK AREAS AS APPROPRIATE OR AS INDICATED ON PLANS AND STOCKPILE FOR REUSE
- 6. MAINTAIN A UNIFORM GRADE BETWEEN CONTOURS IN AREAS TO BE GRADED UNLESS NOTED OTHERWISE
- 7. ELEVATIONS, IF SHOWN ARE FINISHED ELEVATIONS. SPOT ELEVATIONS TAKE PRECEDENCE OVER CONTOURS.
- ADD EROSION CONTROL MEASURES IF GRADES GREATER THAN 3:1 OR IF CONDITIONS WARRANT. REFER TO MNDOT SPECIFICATIONS FOR EROSION CONTROL.
- 9. CONTRACTOR SHALL CONTACT PUBLIC UTILITIES FOR LOCATION OF UNDERGROUND WIRES, CABLES, CONDUITS, PIPES, MANHOLES, VALVES OR OTHER BURIED STRUCTURES BEFORE DIGGING. LANDSCAPE CONTRACTOR SHALL REPAIR OR REPLACE THE ABOVE IF DAMAGED DURING CONSTRUCTION AT NO ADDITIONAL COST TO THE OWNER.
- 10. CONTRACTOR SHALL PROVIDE PROPER EROSION CONTROL MEASURES AS REQUIRED TO ENSURE THAT EROSION IS KEPT TO AN ABSOLUTE MINIMUM.
- 11. PROVIDE TEMPORARY COVERING FOR CATCH BASINS AND MAN HOLES UNTIL FINISHED GRADING IS COMPLETE.
- 12. CONTRACTOR SHALL CONSTRUCT DRAINAGE BASINS AS NEEDED. 13. PERIMETER SILT FENCE AND ROCK CONSTRUCTION ENTRANCES
- SHALL BE INSTALLED PRIOR TO CONSTRUCTION. REFER TO STATE SPECIFICATIONS FOR AGGREGATE BASE AND SILT FENCE. 14. CONTRACTOR SHALL INSTALL CATCH BASIN EROSION CONTROL
- MEASURES PER LOCAL POLLUTION CONTROL AGENCY AND SPECIFICATIONS.
- 15. WITHIN TWO WEEKS OF FINISHED SITE GRADING, DISTURBED AREAS SHALL BE STABILIZED WITH SEED, SOD, MULCH OR ROCK BASE.
- 16. CONTRACTOR SHALL MAINTAIN EROSION CONTROL MEASURES, INCLUDING THE REMOVAL OF ACCUMULATED SILT IN FRONT OF SILT FENCES AND EXCESS SEDIMENT IN PROPOSED CATCH BASINS, FOR THE DURATION OF CONSTRUCTION.
- 17. CONTRACTOR SHALL REMOVE EROSION CONTROL MEASURES AFTER VEGETATION IS ESTABLISHED AND DISPOSE OF OFF SITE.
- 18. CONTRACTOR SHALL ENSURE THAT SOIL CONDITIONS AND COMPACTION ARE ADEQUATE TO ALLOW FOR PROPER DRAINAGE AROUND THE CONSTRUCTION SITE. UNDESIRABLE CONDITIONS SHALL BE BROUGHT TO THE ATTENTION OF THE LANDSCAPE ARCHITECT PRIOR TO BEGINNING OF WORK. IT SHALL BE THE LANDSCAPE CONTRACTOR'S RESPONSIBILITY TO ENSURE PROPER SURFACE AND SUBSURFACE DRAINAGE IN PLANTING AREAS.

PLANTING

- 1. SPRING PLANT MATERIAL INSTALLATION IS FROM APRIL 15 TO JUNE
- 2. FALL CONIFEROUS PLANTING IS ACCEPTABLE FROM AUGUST 21 TO SEPTEMBER 30.
- 3. FALL DECIDUOUS PLANTING IS ACCEPTABLE FROM AUGUST 15 UNTIL NOVEMBER 15.
- 4. ADJUSTMENTS TO PLANTING DATES MUST BE APPROVED IN WRITING BY THE LANDSCAPE ARCHITECT.
- 5. STAKE PROPOSED PLANTING LOCATIONS PER PLAN FOR REVIEW





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			 PROJECT MANAGER	ANDREW F. JUDD
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- AND APPROVAL BY LANDSCAPE ARCHITECT PRIOR TO INSTALL.
- PLANT MATERIAL SHALL COMPLY WITH THE CURRENT EDITION OF THE AMERICAN STANDARD FOR NURSERY STOCK, ANSI Z60.1. UNLESS NOTED OTHERWISE, DECIDUOUS SHRUBS SHALL HAVE AT LEAST 5 CANES AT THE SPECIFIED HEIGHT. ORNAMENTAL TREES SHALL HAVE NO 'V' CROTCHES AND SHALL BEGIN BRANCHING NO LOWER THAN 3' FEET ABOVE THE ROOT BALL. STREET AND BOULEVARD TREES SHALL BEGIN BRANCHING NO LOWER THAN 6' ABOVE PAVED SURFACE.
- 7. INSTALL PLANT MATERIAL AFTER FINAL GRADING AND CONSTRUCTION HAS BEEN COMPLETED IN THE IMMEDIATE AREA.
- 8. INSTALL PLANT MATERIALS PER PLANTING DETAILS.
- SUBSTITUTION REQUESTS FOR PLANT MATERIAL TYPE & SIZE SHALL BE SUBMITTED TO THE LANDSCAPE ARCHITECT FOR CONSIDERATION PRIOR TO BIDDING. SUBSTITUTIONS AFTER BIDDING MUST BE APPROVED BY LANDSCAPE ARCHITECT AND ARE SUBJECT TO CONTRACT ADJUSTMENTS
- 10. ADJUSTMENTS IN LOCATION OF PROPOSED PLANT MATERIALS MAY BE NEEDED IN FIELD. LANDSCAPE ARCHITECT MUST BE NOTIFIED PRIOR TO ADJUSTMENT OF PLANTS.
- 11. FERTILIZE PLANT MATERIALS IN ACCORDANCE WITH SOIL TEST **RECOMMENDATIONS. [FERTILIZE PLANT MATERIAL UPON** INSTALLATION WITH DRIED BONE MEAL AND OTHER APPROVED FERTILIZER MIXED IN WITH THE PLANTING SOIL (PER THE MANUFACTURER'S INSTRUCTIONS) OR TREAT FOR SUMMER AND FALL INSTALLATION WITH AN APPLICATION OF GRANULAR 10-0-5 OF 12 OZ. PER 2.5" CALIPER TREE AND 6 OZ. PER SHRUB WITH AN ADDITIONAL APPLICATION OF 10-0-10 THE FOLLOWING SPRING IN THE TREE SAUCER.1
- 12. INSTALL 18" DEPTH OF PLANTING SOIL IN AREAS RECEIVING GROUND COVER, PERENNIALS, AND ANNUALS. PLANTING SOIL SHALL CONSIST OF MnDOT 3877-B MODIFIED TO CONTAIN A MAXIMUM OF 30% SAND, A PH OF 7.1 MAX, OR AS OTHERWISE SPECIFIED IN THE PROJECT SPECIFICATIONS MANUAL.
- 13. [TREE WRAPPING MATERIAL SHALL BE PAPER APPLIED FROM TRUNK FLARE TO FIRST BRANCH. WRAP SMOOTH-BARKED DECIDUOUS TREES PLANTED IN THE FALL PRIOR TO DECEMBER 1 AND REMOVE WRAPPING AFTER MAY 1.] [DO NOT WRAP TREES.]
- 14. APPLY PRE-EMERGENT HERBICIDE (PREEN OR APPROVED EQUAL) IN ANNUAL, PERENNIAL, AND SHRUB BEDS FOLLOWED BY SHREDDED HARDWOOD MULCH. REFER TO SPECIFICATIONS FOR ADDITIONAL INFORMATION REGARDING USE OF HERBICIDES.

MULCHING

- 1. INSTALL [4" DEEP FINELY SHREDDED HARDWOOD MULCH] RINGS AT **CONIFEROUS & DECIDUOUS TREES WITH NO MULCH IN DIRECT** CONTACT WITH TREE TRUNK.
- 2. INSTALL [3" DEEP FINELY SHREDDED HARDWOOD MULCH] RINGS AT SHRUB PLANTING AREAS WITH NO MULCH IN DIRECT CONTACT WITH SHRUB STEMS.
- 3. INSTALL [3" DEEP FINELY SHREDDED MULCH] IN PERENNIAL PLANTING BEDS. REMOVE ALL MULCH FROM STEMS OF PERENNIALS; PLANT STEMS SHOULD NOT BE IN DIRECT CONTACT WITH MULCH.

WATERING

- 1. PLANTED MATERIALS SHALL BE WATERED BY TEMPORARY MEANS UNTIL PLANTS ARE ESTABLISHED.
- 2. TEMPORARY WATERING MEANS, METHODS, AND SCHEDULING SHALL BE THE CONTRACTOR'S RESPONSIBILITY. REMOVE TEMPORARY WATERING EQUIPMENT UPON PLANT ESTABLISHMENT.

WARRANTY

WARRANTY NEW PLANT MATERIAL THROUGH ONE CALENDAR YEAR FROM THE DATE OF SUBSTANTIAL COMPLETION. NO PARTIAL ACCEPTANCE WILL BE CONSIDERED.

> 60% DRAFT SUBMITTAL FOR **CLIENT REVIEW**

325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343

IRRIGATION NOTES

- **BUILDING FOUNDATION.**
- DESIGN.
- 3. **OPERABILITY PRIOR TO SYSTEM DESIGN.**]
- DRAWINGS.
- IRRIGATION PRIOR TO INSTALLATION OF MULCH.
- 6 MATERIAL GROWTH REQUIREMENTS.

CONTRACTOR SHALL BE RESPONSIBLE FOR PROVIDING AN IRRIGATION LAYOUT PLAN AND SPECIFICATION THAT MEETS THE REQUIREMENTS OF THE PROVIDED PERFORMANCE SPECIFICATION AS PART OF THE SCOPE OF WORK. SUBMIT LAYOUT PLAN AND SPECIFICATIONS FOR APPROVAL BY THE LANDSCAPE ARCHITECT PRIOR TO ORDER AND/OR CONSTRUCTION. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO ENSURE THAT SODDED/SEEDED AND PLANTED AREAS ARE IRRIGATED PROPERLY, INCLUDING THOSE AREAS DIRECTLY AROUND AND ABUTTING

CONTRACTOR SHALL FIELD VERIFY WATER SUPPLY, VOLUME PRESSURE AND LOCATION FOR SYSTEM TAP PRIOR TO SYSTEM

[CONTRACTOR SHALL FIELD VERIFY AND INSPECT EXISTING IRRIGATION SYSTEM LAYOUT, EQUIPMENT, CONDITION AND

4. CONTRACTOR SHALL CONFIRM COMPLETE LIMITS OF IRRIGATION WITH LANDSCAPE ARCHITECT PRIOR TO SUPPLYING SHOP

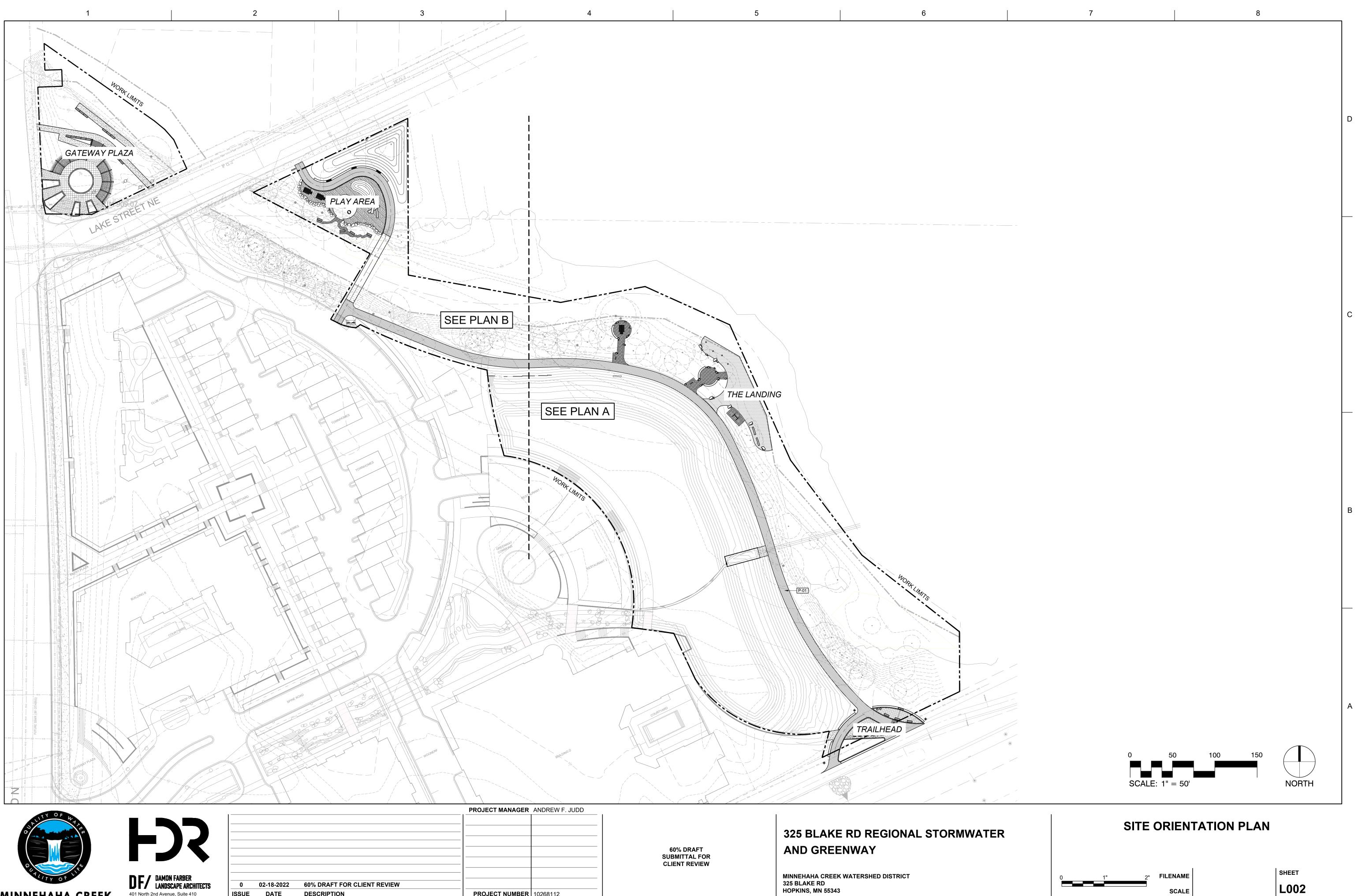
CONTRACTOR SHALL CONTACT LANDSCAPE ARCHITECT FOR INSPECTION AND APPROVAL OF AREAS RECEIVING DRIP

CONTRACTOR SHALL PROVIDE THE OWNER AND LANDSCAPE ARCHITECT WITH AS-BUILT DRAWINGS, DETAILED SYSTEM **OPERATION INSTRUCTIONS AND AN IRRIGATION SCHEDULE** APPROPRIATE TO THE PROJECT SITE CONDITIONS AND PLANTED

LANDSCAPE GENERAL NOTES

FILENAME SCALE SHEET L001 D

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ISSUE	DATE	DESCRIPTION

PROJECT MANAGER	ANDREW F. JUDD
PROJECT NUMBER	10268112

	RIALS SCHEDULE				
ODE	AMENTLY DESCRIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	MANUFACTURER
M-01	AMENITY TYPE 01 - TRAIL KIOSK	2	1/L580	THREE RIVERS PARK DISTRICT TRAIL KIOSK	
M-02	AMENITY TYPE 02 - SYSTEM KIOSK	1	1/L581	THREE RIVERS PARK DISTRICT SYSTEM KIOSKI	
M-03A	AMENITY TYPE 03A - INTERPRETIVE FEATURE	1		TBD	
M-03B	AMENITY TYPE 03B - INTERPRETIVE FEATURE	2			
M-05	AMENITY TYPE 05 - PERGOLA	2		HSS FRAME WITH WOOD PERLINS OVER CONCRETE FOOTINGS	CUSTOM
M-06	AMENITY TYPE 06 - CANOE RACK	1	1/L584	GALVANIZED STEEL STRUCTURE OVER	CUSTOM
M-08	AMENITY TYPE 08 - DRINKING FOUNTAIN	1	2/L583	CONCRETE FOOTINGS	
		1		FIX IT STATION WITH AIR KIT 2, SURFACE	DERO
AM-09	AMENITY TYPE 09 - BIKE FIX-IT STATION	I	3/L583	MOUNT TO CONC. BELOW	DERO
ODE	CURB DESCRIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	
				8" W X 6" H REINFORCED CONCRETE CURB,	
B-01	CURB TYPE 01 - CIP CONCRETE PLANTER CURB	229 LF	1/L520	OVER COMPACTED AGGREGATE, COMPACTED SUBGRADE	
CB-02	CURB TYPE 02 - CIP CONCRETE RIBBON CURB	296 LF	2/L520	8" WIDTH AT GRADE REINFORCED CONCRETE CURB OVER COMPACTED AGGREGATE BASE	
B-03	CURB TYPE 03 - CIP CONCRETE PLAY AREA CURB	163 LF	3/L520	6" WIDTH AT GRADE REINFORCED CONCRETE CURB OVER COMPACTED AGGREGATE BASE	
	EDGING				
ODE	DESCRIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	COLOR/FINISH
D-01	EDGING TYPE 01 - STONE EDGING	261 LF	1/L530	LIMESTONE EDGING, 4" WIDTH X 8" LENGTHS,	TBD
		0515		OVER COMPACTED AGGRETATE BASE 1/8" X 3" X 3" ANGLE IRON EDGE RESTRAINT W/	
D-02	EDGING TYPE 02 - PAVER RESTRAINT	25 LF	3/L530	12" STAKE	
ODE	FENCE & GUARDRAIL DESCRIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	MANUFACTURER
E-01	GUARDRAIL TYPE 01 - OUTLET STRUCTURE				CUSTOM
E-01	GUARDRAIL	104 LF	1/L551	42" HEIGHT GALVANIZED STEEL	CUSTOM
ODE	HANDRAIL DESCRIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	MANUFACTURER
IR-01	HANDRAIL TYPE 01 - STAIR HANDRAIL	31 LF	1/L550	1 1/2" DIA. GALV STEEL RAIL	CUSTOM
	LIGHTING				
	DESCRIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	MANUFACTURER
.T-01	LIGHT TYPE 01 - PEDESTRIAN SCALE POLE LIGHT	3	3/L572	PEDESTRIAN SCALE POLE LIGHT	TBD
ODE	PAVING DESCRIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	MANUFACTURER
P-01	PAVING TYPE 01 - BITUMINOUS PAVING	12,162 SF	DEMAE	SEE CIVIL	
-02	PAVING TYPE 02 - PERMEABLE CONCRETE UNIT	5,878 SF	1/L510	3" THK, 6" X 12" OVER COMPACTED	WAUSAU TILE / TECTURA DESIGN
	PAVERS	-,		AGGREGATE BASE, COMPACTED SUBGRADE	
-03	PAVING TYPE 03 - CONCRETE PAVING	2,604 SF	2/L510	SEE CIVIL	
9-04	PAVING TYPE 04 - CRUSHED STONE SURFACING	18.56 CY	3/L510	3/8" AGGREGATE, 4" DEPTH	
P-05	PAVING TYPE 05 - BEACH SURFACING	3,945 SF		4" DEPTH SAND SALVAGED FROM CONSTRUCTION	
P-07	PAVING TYPE 07 - DECORATIVE CONCRETE PAVING	1,256 SF		4" REINFORCED CONCRETE PAVING	
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ODE	DESCRIPTION PLAY EQUIPMENT TYPE 01 - WOOD FIBER	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY ENGINEERED WOOD FIBER, DEPTH PER ASTM	MANUFACTURER
PE-01	SURFACING (EWF)	2,484 SF		STND. WITH SUBSURFACE DRAINGE SYSTEM	
PE-03	PLAY EQUIPMENT TYPE 03 - LOG STACK	1		LOG STACK ANCHORED IN PLACE OVER	TBD
	PLAY EQUIPMENT TYPE 05 - PRECAST CONCRETE			CONCRETE FOOTINGS PRECAST CONCRETE ACORNS OVER	
'E-06	ACORNS	3		AGGREGATE BASE	CUSTOM
-	ROCK				
ODE		QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY DOLOMITIC LIMESTONE OUTCROPPING, 12"-48"	
RO-01	ROCK TYPE 01 - LANDSCAPE BOULDER	38	4/L510	SIZES	
ODE F-01	DESCRIPTION SITE FURNITURE TYPE 01 - LINEAR BENCH	QTY 21	DETAIL 1/L570	MATERIAL PROFILE/ASSEMBLY 2` X 6` LINEAR BENCH	MANUFACTURER ANOVA
				10" DIA. 5`-6` HEIGHT WOODEN POST,	
F-02	SITE FURNITURE TYPE 02 - HAMMOCK POLE	4	2/L570	EMBEDDED IN WASHED AGGREGATE	SALVAGE FROM SITE
F-03	SITE FURNITURE TYPE 03 - BIKE RACK	3	3/L570	BIKE RACK EMBEDDED IN CIP CONCRETE FOOTING	DERO
F-04	SITE FURNITURE TYPE 04 - LOG BENCH	2	4/L570	6` LONG WOODEN BENCH WITH FLAT TOP	SALVAGE FROM SITE
F-05	SITE FURNITURE TYPE 05 - PICNIC TABLE	3	1/L571	OVER COMPACTED AGGREGATE BASE ACCESSIBLE PICNIC TABLE WITH SEATS	COLUMBIA CASCADE COMPANY
SF-06	SITE FURNITURE TYPE 07 - WASTE RECEPTACLE	2	1/L572	TBD	
	STAIRS				
-	DESCRIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	
		6 LF	1/L540	CIP CONCRETE STAIR	
	STAIR TYPE 01 - RADIAL STAIR @ GATEWAY				
ST-01	STAIR TYPE 01 - RADIAL STAIR @ GATEWAY WALL DESCRIPTION	QTY	DETAII	MATERIAL PROFILE/ASSEMBLY	PRODUCT/MODEI
ST-01 CODE	WALL DESCRIPTION WALL TYPE 01 - LIMESTONE SEATWALL @	QTY 111 F	DETAIL	2` WIDTH X 1.5` HEIGHT X 4` LENGTHS, RADIAL	PRODUCT/MODEL
CODE ST-01 CODE VL-01	WALL DESCRIPTION	111 LF	1/L560	2` WIDTH X 1.5` HEIGHT X 4` LENGTHS, RADIAL LAYOUT PER PLAN 1.5` HEIGHT X RANDOM WIDTHS & LENGTHS	DOLOMITIC LIMESTONE
ODE	WALL DESCRIPTION WALL TYPE 01 - LIMESTONE SEATWALL @ TRAILHEAD			2` WIDTH X 1.5' HEIGHT X 4` LENGTHS, RADIAL LAYOUT PER PLAN 1.5' HEIGHT X RANDOM WIDTHS & LENGTHS LIMESTONE OUTCROPPINGS OVER AGGREGATE BASE	
T-01 ODE VL-01 VL-02	WALL DESCRIPTION WALL TYPE 01 - LIMESTONE SEATWALL @ TRAILHEAD WALL TYPE 02 - LIMESTONE SEATWALL @ PLAY	111 LF	1/L560	2` WIDTH X 1.5` HEIGHT X 4` LENGTHS, RADIAL LAYOUT PER PLAN 1.5` HEIGHT X RANDOM WIDTHS & LENGTHS LIMESTONE OUTCROPPINGS OVER	DOLOMITIC LIMESTONE
CODE VL-01 VL-02 VL-03	WALL DESCRIPTION WALL TYPE 01 - LIMESTONE SEATWALL @ TRAILHEAD WALL TYPE 02 - LIMESTONE SEATWALL @ PLAY AREA WALL TYPE 03 - LIMESTONE SEATWALL @ PICNIC	111 LF 117 LF	1/L560 2/L560	 2` WIDTH X 1.5` HEIGHT X 4` LENGTHS, RADIAL LAYOUT PER PLAN 1.5` HEIGHT X RANDOM WIDTHS & LENGTHS LIMESTONE OUTCROPPINGS OVER AGGREGATE BASE 1.5` HEIGHT X RANDOM WIDTHS & LENGTHS LIMESTONE OUTCROPPINGS OVER 	DOLOMITIC LIMESTONE
CODE VL-01 VL-02 VL-03 VL-04	WALL DESCRIPTION WALL TYPE 01 - LIMESTONE SEATWALL @ TRAILHEAD WALL TYPE 02 - LIMESTONE SEATWALL @ PLAY AREA WALL TYPE 03 - LIMESTONE SEATWALL @ PICNIC AREA WALL TYPE 04 - CIP CONCRETE WALL WALL TYPE 05 - CIP CONCRETE SEATWALL @ PLAY	111 LF 117 LF 52 LF	1/L560 2/L560 1/L561 2/L562	2' WIDTH X 1.5' HEIGHT X 4' LENGTHS, RADIAL LAYOUT PER PLAN 1.5' HEIGHT X RANDOM WIDTHS & LENGTHS LIMESTONE OUTCROPPINGS OVER AGGREGATE BASE 1.5' HEIGHT X RANDOM WIDTHS & LENGTHS LIMESTONE OUTCROPPINGS OVER AGGREGATE BASE 8" WIDTH CIP CONCRETE WALL 2' WIDTH, 1.5' HEIGHT CIP CONC WALL W	DOLOMITIC LIMESTONE
CODE VL-01 VL-02 VL-03 VL-04 VL-05	WALL DESCRIPTION WALL TYPE 01 - LIMESTONE SEATWALL @ TRAILHEAD WALL TYPE 02 - LIMESTONE SEATWALL @ PLAY AREA WALL TYPE 03 - LIMESTONE SEATWALL @ PICNIC AREA WALL TYPE 04 - CIP CONCRETE WALL WALL TYPE 05 - CIP CONCRETE SEATWALL @ PLAY AREA	111 LF 117 LF 52 LF 107 LF 98 LF	1/L560 2/L560 1/L561 2/L562 2/L561	2' WIDTH X 1.5' HEIGHT X 4' LENGTHS, RADIAL LAYOUT PER PLAN 1.5' HEIGHT X RANDOM WIDTHS & LENGTHS LIMESTONE OUTCROPPINGS OVER AGGREGATE BASE 1.5' HEIGHT X RANDOM WIDTHS & LENGTHS LIMESTONE OUTCROPPINGS OVER AGGREGATE BASE 8" WIDTH CIP CONCRETE WALL 2' WIDTH, 1.5' HEIGHT CIP CONC WALL W INTEGRAL WOOD SEATING	DOLOMITIC LIMESTONE
CODE VL-01	WALL DESCRIPTION WALL TYPE 01 - LIMESTONE SEATWALL @ TRAILHEAD WALL TYPE 02 - LIMESTONE SEATWALL @ PLAY AREA WALL TYPE 03 - LIMESTONE SEATWALL @ PICNIC AREA WALL TYPE 04 - CIP CONCRETE WALL WALL TYPE 05 - CIP CONCRETE SEATWALL @ PLAY	111 LF 117 LF 52 LF 107 LF	1/L560 2/L560 1/L561 2/L562	2' WIDTH X 1.5' HEIGHT X 4' LENGTHS, RADIAL LAYOUT PER PLAN 1.5' HEIGHT X RANDOM WIDTHS & LENGTHS LIMESTONE OUTCROPPINGS OVER AGGREGATE BASE 1.5' HEIGHT X RANDOM WIDTHS & LENGTHS LIMESTONE OUTCROPPINGS OVER AGGREGATE BASE 8" WIDTH CIP CONCRETE WALL 2' WIDTH, 1.5' HEIGHT CIP CONC WALL W	DOLOMITIC LIMESTONE





DF/ DAMON FARBER LANDSCAPE ARCHITECTS 401 North 2nd Avenue, Suite 410 Minneapolis, MN 55401 p: 612.332.7522

0 02-18-2022 ISSUE DATE

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SCHEDULE								
TY								
	QTY	DETAIL		MANUFACTURER	CC	DLOR/FINISH		
TY TYPE 01 - TRAIL KIOSK	2	1/L580	THREE RIVERS PARK DISTRICT TRAIL KIOSK					
TY TYPE 02 - SYSTEM KIOSK TY TYPE 03A - INTERPRETIVE FEATURE	1	1/L581	THREE RIVERS PARK DISTRICT SYSTEM KIOSK TBD	KI				
TY TYPE 03B - INTERPRETIVE FEATURE	2		TBD					
TY TYPE 05 - PERGOLA	2		HSS FRAME WITH WOOD PERLINS OVER	CUSTOM				
	2		CONCRETE FOOTINGS GALVANIZED STEEL STRUCTURE OVER					
TY TYPE 06 - CANOE RACK	1	1/L584	CONCRETE FOOTINGS	CUSTOM				
TY TYPE 08 - DRINKING FOUNTAIN	1	2/L583						
TY TYPE 09 - BIKE FIX-IT STATION	1	3/L583	FIX IT STATION WITH AIR KIT 2, SURFACE MOUNT TO CONC. BELOW	DERO	ТВ	D		
RIPTION	QTY	DETAIL						
TYPE 01 - CIP CONCRETE PLANTER CURB	229 LF	1/L520	8" W X 6" H REINFORCED CONCRETE CURB, OVER COMPACTED AGGREGATE, COMPACTED	D				
			SUBGRADE					
TYPE 02 - CIP CONCRETE RIBBON CURB	296 LF	2/L520	8" WIDTH AT GRADE REINFORCED CONCRETE CURB OVER COMPACTED AGGREGATE BASE	<u>-</u>				
TYPE 03 - CIP CONCRETE PLAY AREA CURB	163 LF	3/L520	6" WIDTH AT GRADE REINFORCED CONCRETE	1				
		-	CURB OVER COMPACTED AGGREGATE BASE					
G								
RIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	COLOR/FINISH				
G TYPE 01 - STONE EDGING	261 LF	1/L530	LIMESTONE EDGING, 4" WIDTH X 8" LENGTHS, OVER COMPACTED AGGRETATE BASE	TBD				
	25 LF	2// 520	1/8" X 3" X 3" ANGLE IRON EDGE RESTRAINT W	V/				
G TYPE 02 - PAVER RESTRAINT	20 LF	3/L530	12" STAKE					
& GUARDRAIL								
RIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	MANUFACTURER	CC	DLOR/FINISH		
DRAIL TYPE 01 - OUTLET STRUCTURE	104 LF	1/L551		CUSTOM		T-DIPPED GALVANIZED		
DRAIL								
RAIL								
RIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	MANUFACTURER				
RAIL TYPE 01 - STAIR HANDRAIL	31 LF	1/L550	1 1/2" DIA. GALV STEEL RAIL	CUSTOM				
NG		DETAU						
	QTY 3	DETAIL	MATERIAL PROFILE/ASSEMBLY			OMMENTS		
TYPE 01 - PEDESTRIAN SCALE POLE LIGHT	3	3/L572	PEDESTRIAN SCALE POLE LIGHT	TBD	SE	E ELECTRICAL PLANS		
3								
RIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	MANUFACTURER	PR	ODUCT/MODEL	COLOR/FINISH	COMMENTS
G TYPE 01 - BITUMINOUS PAVING	12,162 SF		SEE CIVIL					
G TYPE 02 - PERMEABLE CONCRETE UNIT	5,878 SF	1/L510	3" THK, 6" X 12" OVER COMPACTED AGGREGATE BASE, COMPACTED SUBGRADE	WAUSAU TILE / TEC	CTURA DESIGNS EC	OPREMIER	HEP-60	
G TYPE 03 - CONCRETE PAVING	2,604 SF	2/1 510	SEE CIVIL				GRAY, MEDIUM BROOM FINISH	REFER TO LA DETAIL FOR TYP JOINTING, SEE
								CIVIL FOR DEPTH / BASE MATERIALS
G TYPE 04 - CRUSHED STONE SURFACING	18.56 CY	3/L510	3/8" AGGREGATE, 4" DEPTH 4" DEPTH SAND SALVAGED FROM					
G TYPE 05 - BEACH SURFACING	3,945 SF		CONSTRUCTION					
G TYPE 07 - DECORATIVE CONCRETE PAVING	1,256 SF		4" REINFORCED CONCRETE PAVING				SANDBLAST WITH PATTERN, PATTERN T	BD
QUIPMENT								
RIPTION	QTY	DETAIL	MATERIAL PROFILE/ASSEMBLY	MANUFACTURER				
QUIPMENT TYPE 01 - WOOD FIBER		BEIME	ENGINEERED WOOD FIBER, DEPTH PER ASTM					
CING (EWF)	2,484 SF		STND. WITH SUBSURFACE DRAINGE SYSTEM					
QUIPMENT TYPE 03 - LOG STACK	1		LOG STACK ANCHORED IN PLACE OVER CONCRETE FOOTINGS	TBD				

PRODUCT/MODEL INF24L6T

COLOR/FINISH THERMORY SLAT

GALVANIZED STEEL

COMMENTS SURFACE MOUNT

ROLLING RACK

2165-6

GALVANIZED STEEL FRAME

COLOR/FINISH

CUT TOP AND BUTT ENDS, SPLIT FACES

NATURAL TOP AND FACES

SAWN TOP & ENDS, AND FRONT FACES

STANDARD GRAY CONC/ SMOOTH FINISH

PROJECT MANAGER	ANDREW F. JUDD
PROJECT NUMBER	10268112

60% DRAFT SUBMITTAL FOR CLIENT REVIEW

325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343



SITE MATERIALS SCHEDULE



SHEET L010 D

С

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CONCEPT PLANT SCHEDULE

1 |

C.	<u>CONIFEROUS TREE</u> PICEA GLAUCA `DENSATA` / BLACK HILLS SPRUCE	6
- And	DECIDUOUS CANOPY TREE BETULA PAPYRIFERA `VAREN` TM / PRAIRIE DREAM BIRCH CARPINUS CAROLINIANA / AMERICAN HORNBEAM CELTIS OCCIDENTALIS / COMMON HACKBERRY OSTRYA VIRGINIANA / AMERICAN HOPHORNBEAM QUERCUS BICOLOR / SWAMP WHITE OAK QUERCUS MACROCARPA / BUR OAK QUERCUS X `HERITAGE` / HERITAGE ENGLISH OAK ULMUS AMERICANA `ST. CROIX` / ST. CROIX AMERICAN ELM	44
Ø	ORNAMENTAL TREE AMELANCHIER X GRANDIFLORA / APPLE SERVICEBERRY BETULA NIGRA `CULLY` TM / HERITAGE RIVER BIRCH BETULA PAPYRIFERA `RENCI` TM / RENAISSANCE REFLECTION PAPER BIRCH BETULA PAPYRIFERA `VAREN` TM / PRAIRIE DREAM BIRCH CARPINUS CAROLINIANA / AMERICAN HORNBEAM	13
	DECIDUOUS COLUMNAR TREE POPULUS TREMULOIDES `NE ARB` / PRAIRIE GOLD ASPEN	6
	DECIDUOUS SHRUB	2,048 SF
 ψ ψ	<u>SEED MIX - TURF</u> TBD LOW MOW TURF MIX -	695 SF
	SEED MIX - WET MEADOW BSWR - 34-271 WET MEADOW SOUTH & WEST -	5,770 SF
	<u>SEED MIX - WOODLAND EDGE</u> BWSR MIX 36-211 WOODLAND EDGE SOUTH & WEST -	11,938 SF
	<u>SEED MIX - MESIC PRAIRIE</u> BWSR PILOT MIXES: "LITTLE BLUESTEM URBAN PRAIRIE" -	32,253 SF



MINNEHAHA CREEK WATERSHED DISTRICT



DF/ DAMON FARBER LANDSCAPE ARCHITECTS 401 North 2nd Avenue, Suite 410 Minneapolis, MN 55401 p: 612.332.7522

ISSUE DATE

0 02-18-2022 60% DRAFT FOR CLIENT REVIEW DESCRIPTION

PRO

ANDREW F. JUDD

3 4 5

PROJECT NUMBER	10268112

60% DRAFT SUBMITTAL FOR CLIENT REVIEW

325 BLAKE RD REGIONAL STORMWATER AND GREENWAY

6

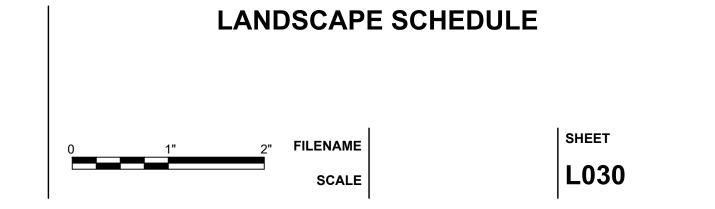
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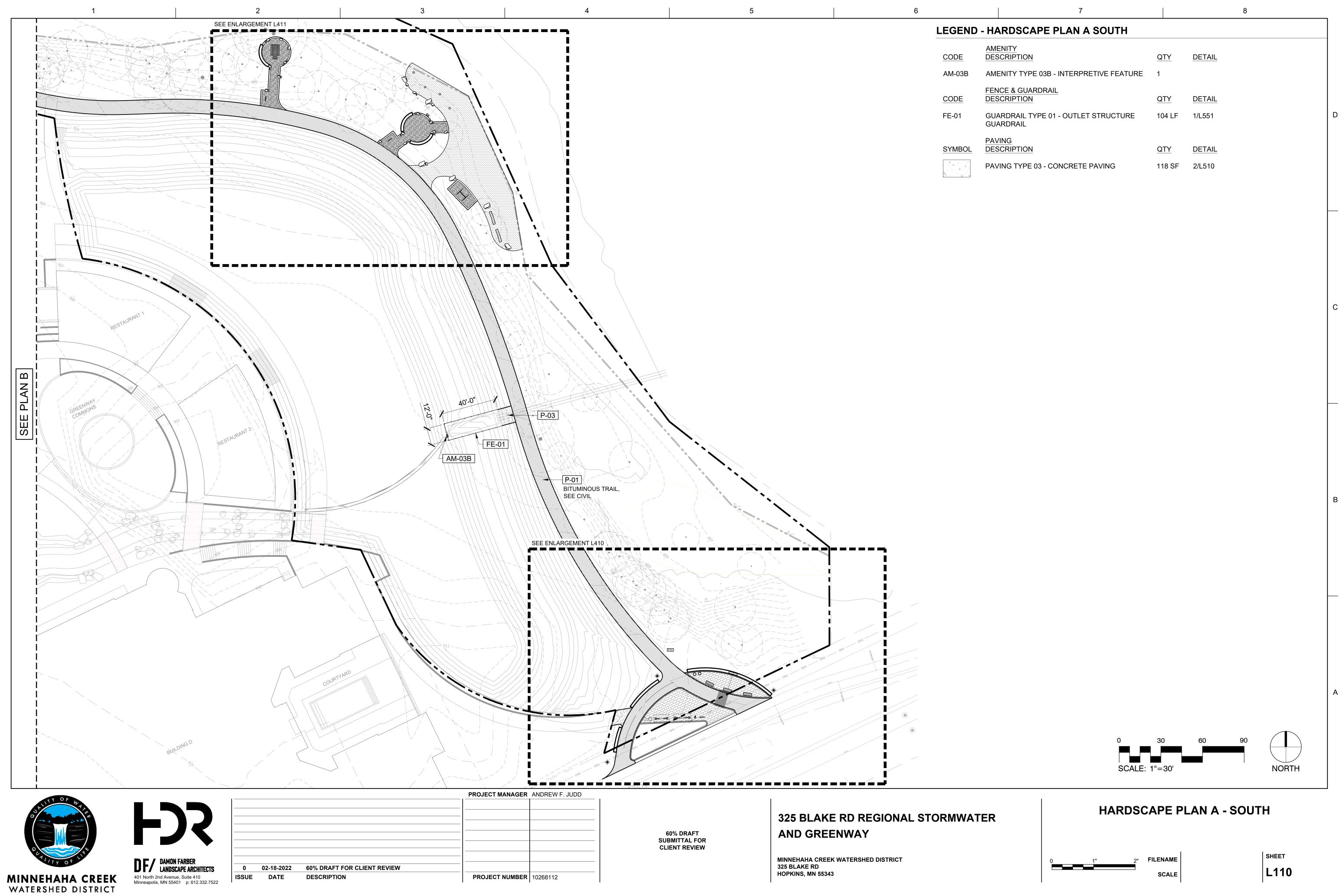
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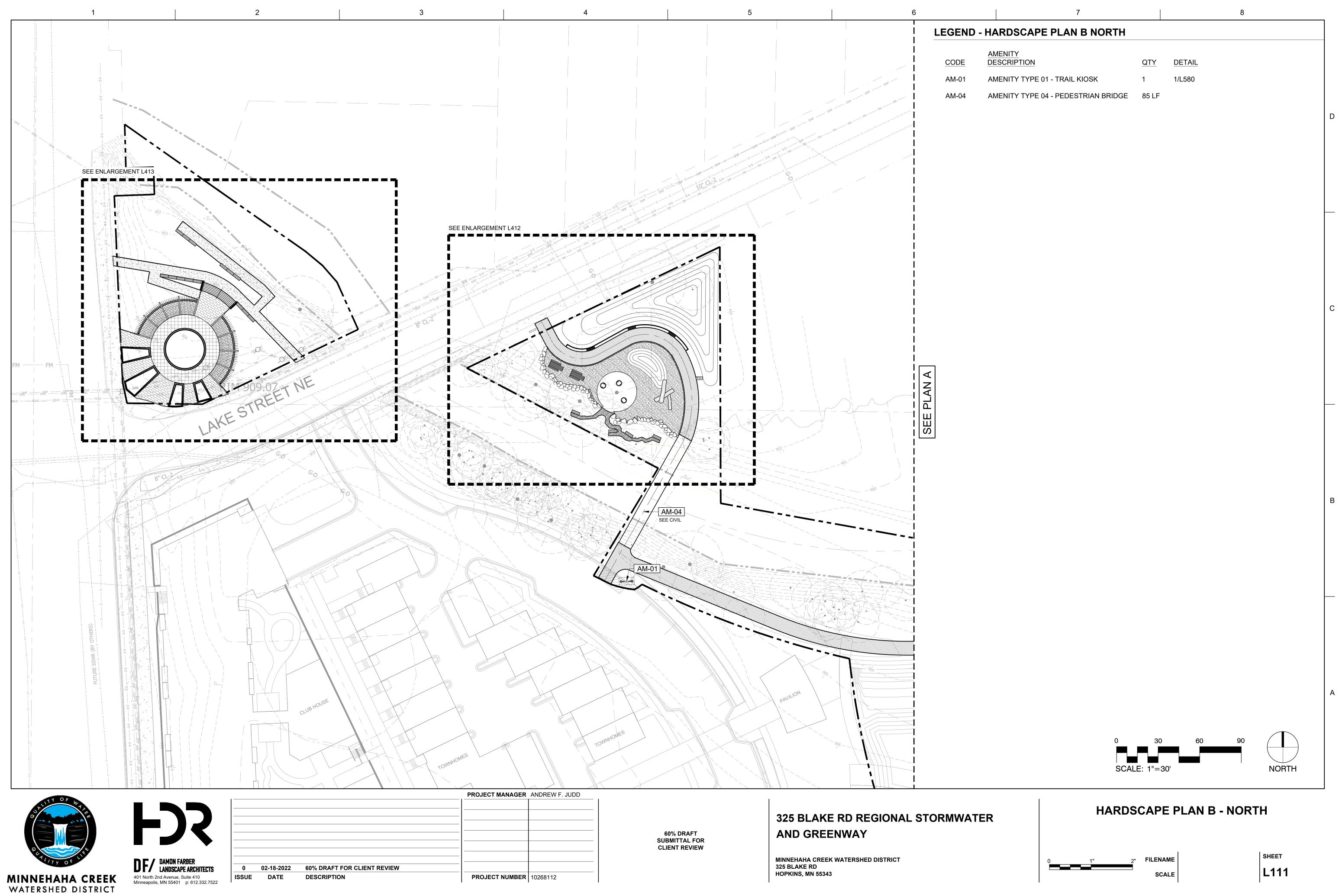
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MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343

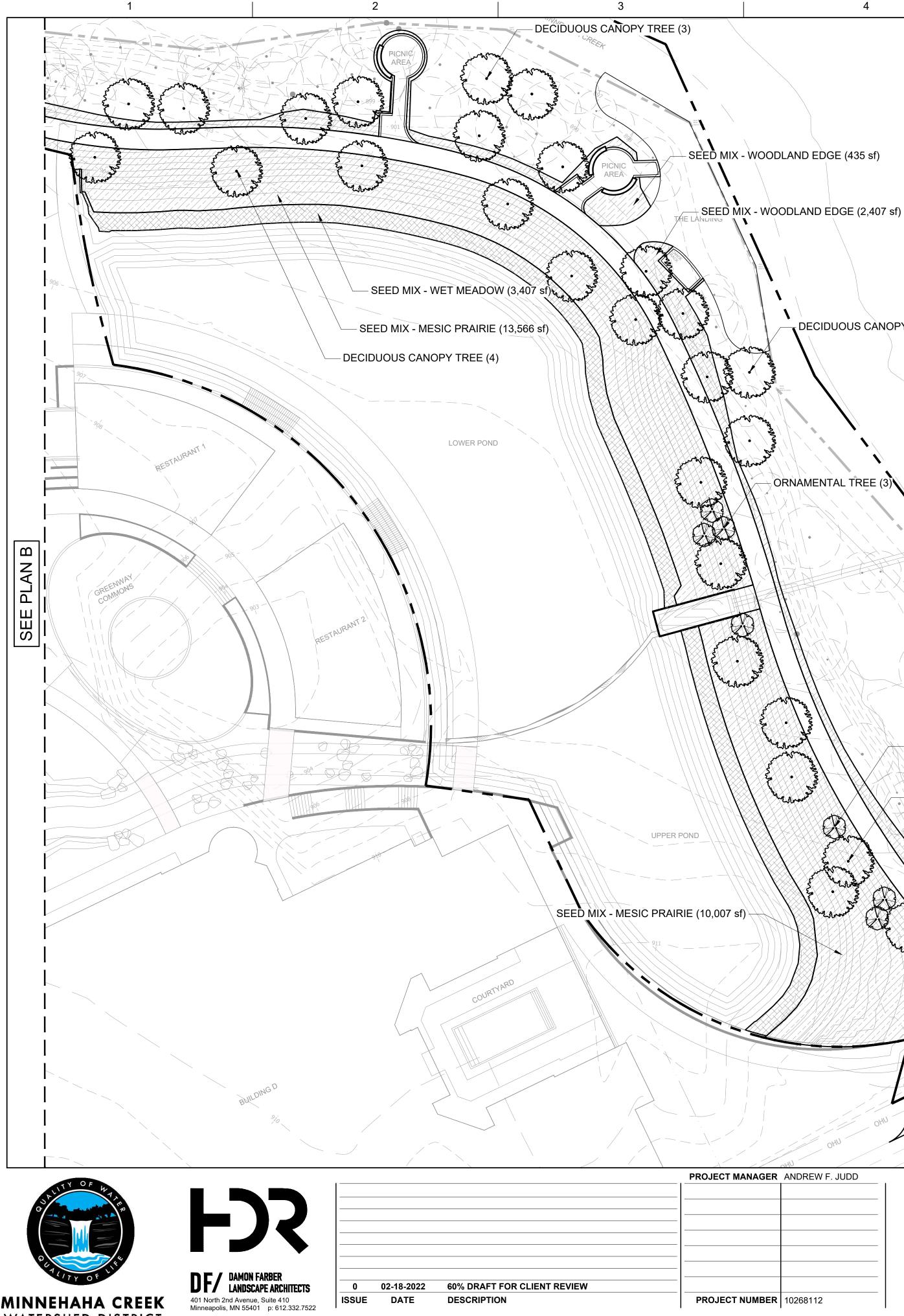




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- HARDSCAPE PLAN A SOUTH				
AMENITY DESCRIPTION	QTY	DETAIL		
AMENITY TYPE 03B - INTERPRETIVE FEATUR	RE 1			
FENCE & GUARDRAIL DESCRIPTION	QTY	DETAIL		
GUARDRAIL TYPE 01 - OUTLET STRUCTURE GUARDRAIL	104 LF	1/L551		D
PAVING DESCRIPTION	QTY	DETAIL		
PAVING TYPE 03 - CONCRETE PAVING	118 SF	2/L510		



		0	
HARDSCAPE PLAN B NORTH			
AMENITY DESCRIPTION	QTY	DETAIL	
AMENITY TYPE 01 - TRAIL KIOSK	1	1/L580	
AMENITY TYPE 04 - PEDESTRIAN BRIDGE	85 LF		



MINNEHAHA CREEK WATERSHED DISTRICT

ISSUE DATE

DESCRIPTION

PR

DING		
DECIDUOUS CANOPY TREE (5)		
Almond Land Andrew		
ORNAMENTAL TREE (3)		
Mr. Arwania		
And the second s		
ORNAMENTAL TREE (4)		
DECIDUOUS CANOPY TREE (4)		
Level a set of the set		
0,007 sf)		
the second	OHU OHU	
	OHU	
TRAILHEAD		
DECIDUOUS COLUM		
DECIDUOUS SHRUB (741 sf)		
DJECT MANAGER ANDREW F. JUDD		
60% DRAFT	325 BLAKE RD REGIONAL ST AND GREENWAY	ORMWATER
SUBMITTAL FOR CLIENT REVIEW		
ROJECT NUMBER 10268112	MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343	

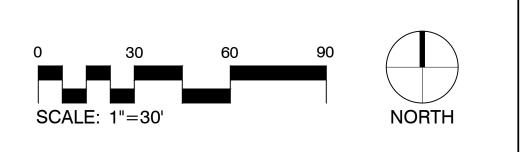
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SEED MIX - WOODLAND EDGE (435 sf)

4

6		7	8		_
	LEGEND - P	LANTING PLAN A			_
	Some Constant	DECIDUOUS CANOPY TREE BETULA PAPYRIFERA 'VAREN' TM / PRAIRIE DRE CARPINUS CAROLINIANA / AMERICAN HORNBEA CELTIS OCCIDENTALIS / COMMON HACKBERRY OSTRYA VIRGINIANA / AMERICAN HOPHORNBEA QUERCUS BICOLOR / SWAMP WHITE OAK QUERCUS MACROCARPA / BUR OAK QUERCUS X 'HERITAGE' / HERITAGE ENGLISH O ULMUS AMERICANA 'ST. CROIX' / ST. CROIX AMI	M M AK	30	D
		ORNAMENTAL TREE AMELANCHIER X GRANDIFLORA / APPLE SERVIO BETULA NIGRA `CULLY` TM / HERITAGE RIVER B BETULA PAPYRIFERA `RENCI` TM / RENAISSANO BETULA PAPYRIFERA `VAREN` TM / PRAIRIE DRE CARPINUS CAROLINIANA / AMERICAN HORNBEA	IRCH E REFLECTION PAPER BIRCH EAM BIRCH	7	
		DECIDUOUS COLUMNAR TREE POPULUS TREMULOIDES `NE ARB` / PRAIRIE GO	LD ASPEN	6	
		DECIDUOUS SHRUB -		741 SF	
		<u>SEED MIX - WET MEADOW</u> BSWR - 34-271 WET MEADOW SOUTH & WEST -		5,260 SF	С
		<u>SEED MIX - WOODLAND EDGE</u> BWSR MIX 36-211 WOODLAND EDGE SOUTH & W -	'EST	5,075 SF	

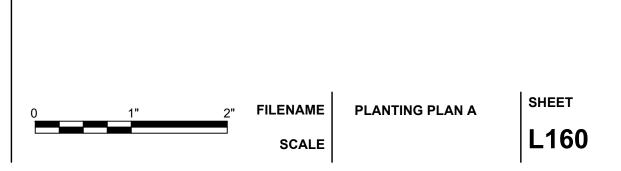
SEED MIX - MESIC PRAIRIE BWSR PILOT MIXES: "LITTLE BLUESTEM URBAN PRAIRIE" -

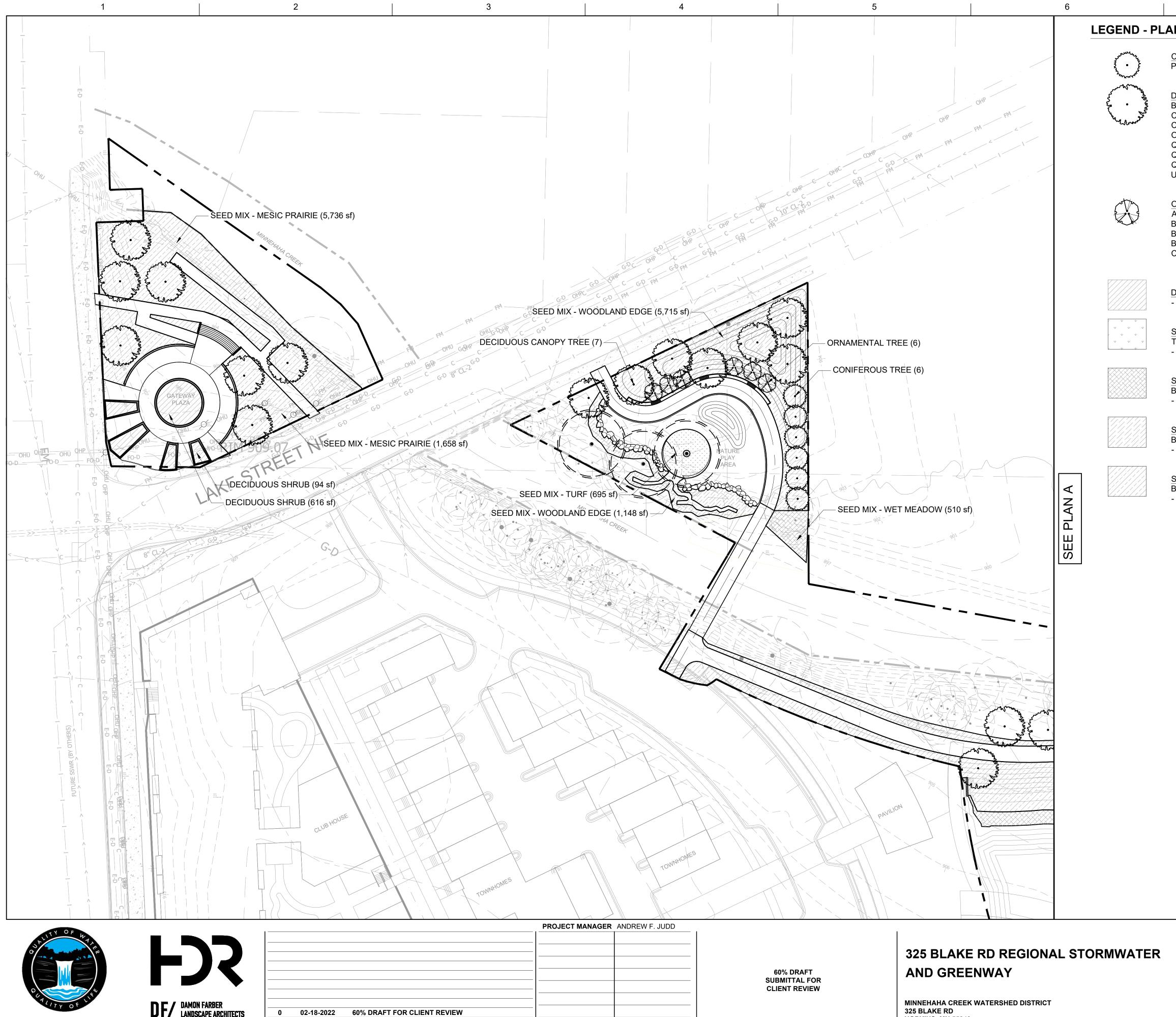


23,573 SF

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PLANTING PLAN A





MINNEHAHA CREEK WATERSHED DISTRICT

DF/ DAMON FARBER LANDSCAPE ARCHITECTS 401 North 2nd Avenue, Suite 410 Minneapolis, MN 55401 p: 612.332.7522

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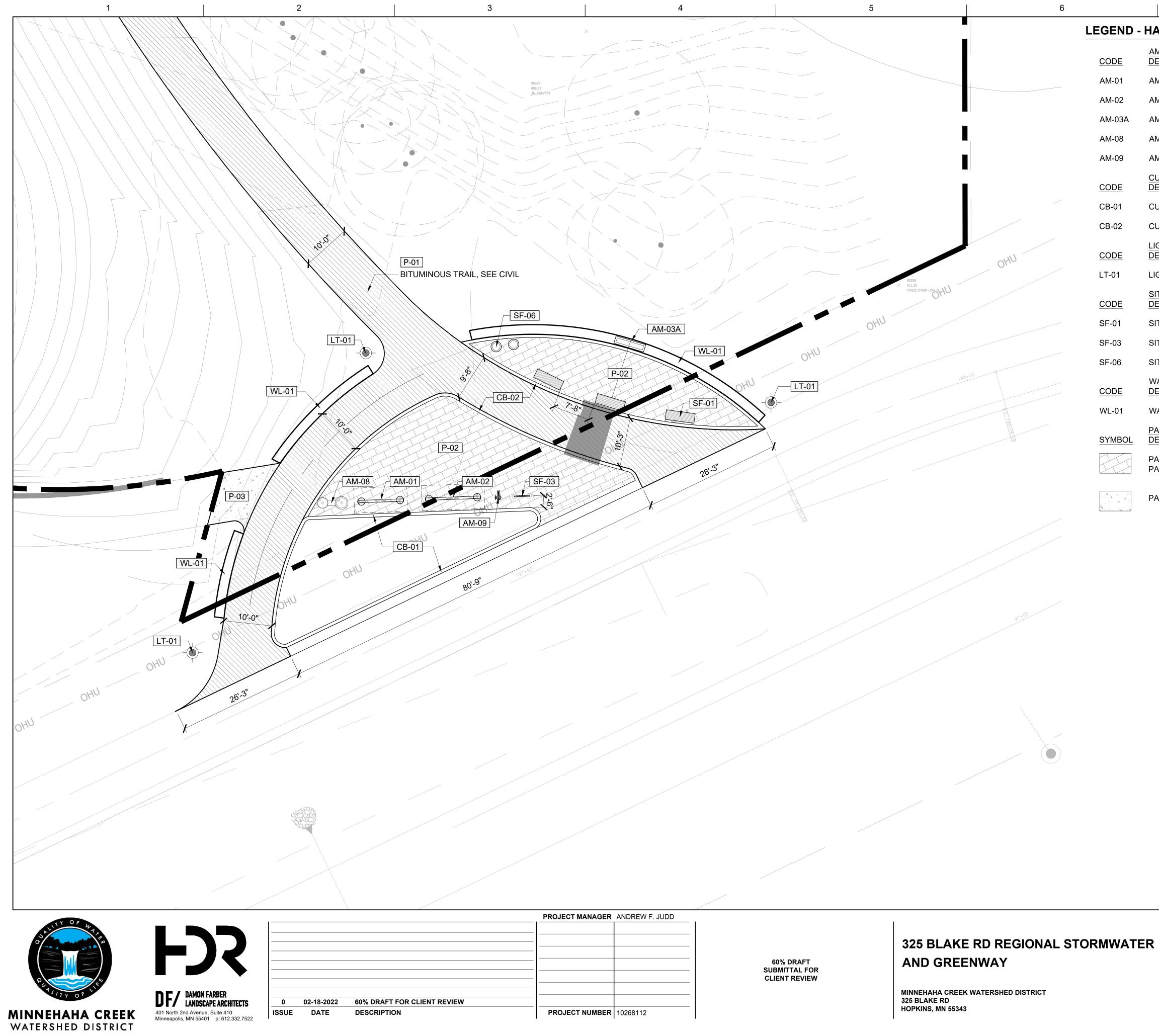
DESCRIPTION

PROJECT NUMBER 10268112

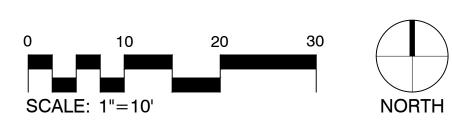
MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343

7 8	
<u>CONIFEROUS TREE</u> PICEA GLAUCA `DENSATA` / BLACK HILLS SPRUCE	6
DECIDUOUS CANOPY TREE BETULA PAPYRIFERA 'VAREN' TM / PRAIRIE DREAM BIRCH CARPINUS CAROLINIANA / AMERICAN HORNBEAM CELTIS OCCIDENTALIS / COMMON HACKBERRY OSTRYA VIRGINIANA / AMERICAN HOPHORNBEAM QUERCUS BICOLOR / SWAMP WHITE OAK QUERCUS MACROCARPA / BUR OAK QUERCUS X `HERITAGE` / HERITAGE ENGLISH OAK ULMUS AMERICANA `ST. CROIX` / ST. CROIX AMERICAN ELM	14
ORNAMENTAL TREE AMELANCHIER X GRANDIFLORA / APPLE SERVICEBERRY BETULA NIGRA `CULLY` TM / HERITAGE RIVER BIRCH BETULA PAPYRIFERA `RENCI` TM / RENAISSANCE REFLECTION PAPER BIR BETULA PAPYRIFERA `VAREN` TM / PRAIRIE DREAM BIRCH CARPINUS CAROLINIANA / AMERICAN HORNBEAM	6 RCH
DECIDUOUS SHRUB -	1,307 SF
SEED MIX - TURF TBD LOW MOW TURF MIX -	695 SF
<u>SEED MIX - WET MEADOW</u> BSWR - 34-271 WET MEADOW SOUTH & WEST -	510 SF
<u>SEED MIX - WOODLAND EDGE</u> BWSR MIX 36-211 WOODLAND EDGE SOUTH & WEST -	6,863 SF
<u>SEED MIX - MESIC PRAIRIE</u> BWSR PILOT MIXES: "LITTLE BLUESTEM URBAN PRAIRIE" -	8,680 SF
0 30 60 90 SCALE: 1"=30'	NORTH
PLANTING PLAN B	





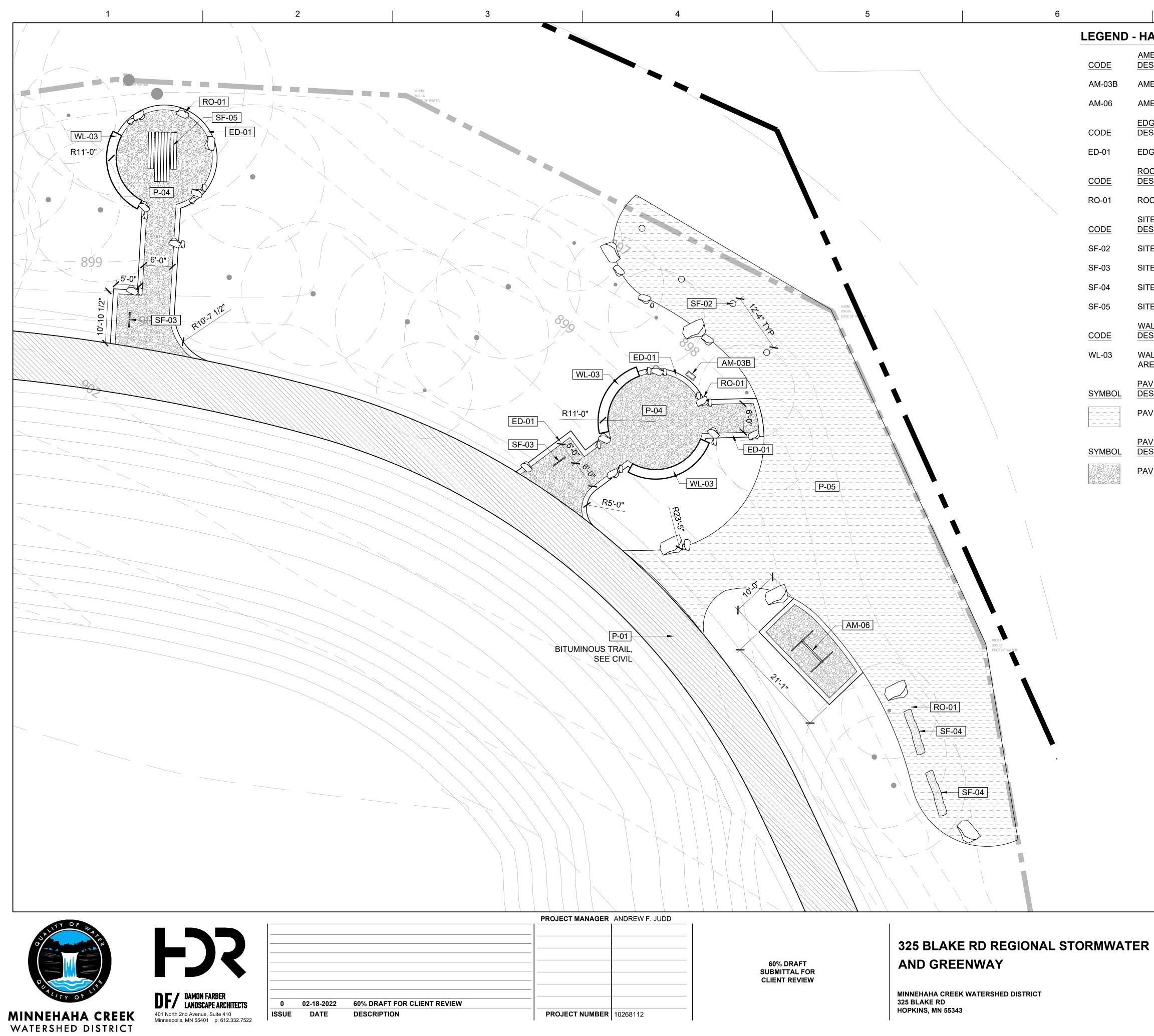
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HA	HARDSCAPE ENLARGEMENT PLAN TRAILHEAD				
	<u>IENITY</u> SCRIPTION	QTY	DETAIL		
AN	IENITY TYPE 01 - TRAIL KIOSK	1	1/L580		
٨N	IENITY TYPE 02 - SYSTEM KIOSK	1	1/L581		
٨N	IENITY TYPE 03A - INTERPRETIVE FEATURE	1		D	
٨N	IENITY TYPE 08 - DRINKING FOUNTAIN	1	2/L583		
AN	IENITY TYPE 09 - BIKE FIX-IT STATION	1	3/L583		
	IRB SCRIPTION	QTY	DETAIL		
CL	IRB TYPE 01 - CIP CONCRETE PLANTER CURB	138 LF	1/L520		
CL	IRB TYPE 02 - CIP CONCRETE RIBBON CURB	296 LF	2/L520		
	<u>SHTING</u> SCRIPTION	QTY	DETAIL		
LIC	GHT TYPE 01 - PEDESTRIAN SCALE POLE LIGHT	3	3/L572		
	TE FURNITURE SCRIPTION	QTY	DETAIL		
SI	TE FURNITURE TYPE 01 - LINEAR BENCH	3	1/L570		
SI	TE FURNITURE TYPE 03 - BIKE RACK	1	3/L570	С	
SI	TE FURNITURE TYPE 07 - WASTE RECEPTACLE	2	1/L572		
	ALL SCRIPTION	QTY	DETAIL		
W	ALL TYPE 01 - LIMESTONE SEATWALL @ TRAILHE	EAD 111 LF	1/L560		
	VING SCRIPTION	QTY	DETAIL		
	VING TYPE 02 - PERMEABLE CONCRETE UNIT VERS	1,500 SF	1/L510		
PA	VING TYPE 03 - CONCRETE PAVING	414 SF	2/L510		



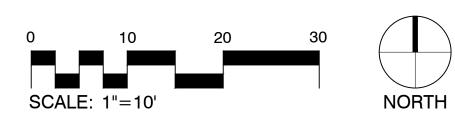








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- HARDSCAPE ENLARGEMENT PLAN		6	
AMENITY DESCRIPTION	QTY	DETAIL	
AMENITY TYPE 03B - INTERPRETIVE FEATURE	1		
AMENITY TYPE 06 - CANOE RACK	1	1/L584	
EDGING DESCRIPTION	QTY	DETAIL	D
EDGING TYPE 01 - STONE EDGING	261 LF	1/L530	
ROCK DESCRIPTION	QTY	DETAIL	
ROCK TYPE 01 - LANDSCAPE BOULDER	38	4/L510	
SITE FURNITURE DESCRIPTION	QTY	DETAIL	
SITE FURNITURE TYPE 02 - HAMMOCK POLE	4	2/L570	<u> </u>
SITE FURNITURE TYPE 03 - BIKE RACK	2	3/L570	
SITE FURNITURE TYPE 04 - LOG BENCH	2	4/L570	
SITE FURNITURE TYPE 05 - PICNIC TABLE	1	1/L571	
WALL DESCRIPTION	QTY	DETAIL	
WALL TYPE 03 - LIMESTONE SEATWALL @ PICNIC AREA	52 LF	1/L561	С
PAVING DESCRIPTION	QTY	DETAIL	
PAVING TYPE 05 - BEACH SURFACING	3,945 SF		
PAVING DESCRIPTION	QTY	DETAIL	
PAVING TYPE 04 - CRUSHED STONE SURFACING	<u> </u>	3/L510	<u> </u>

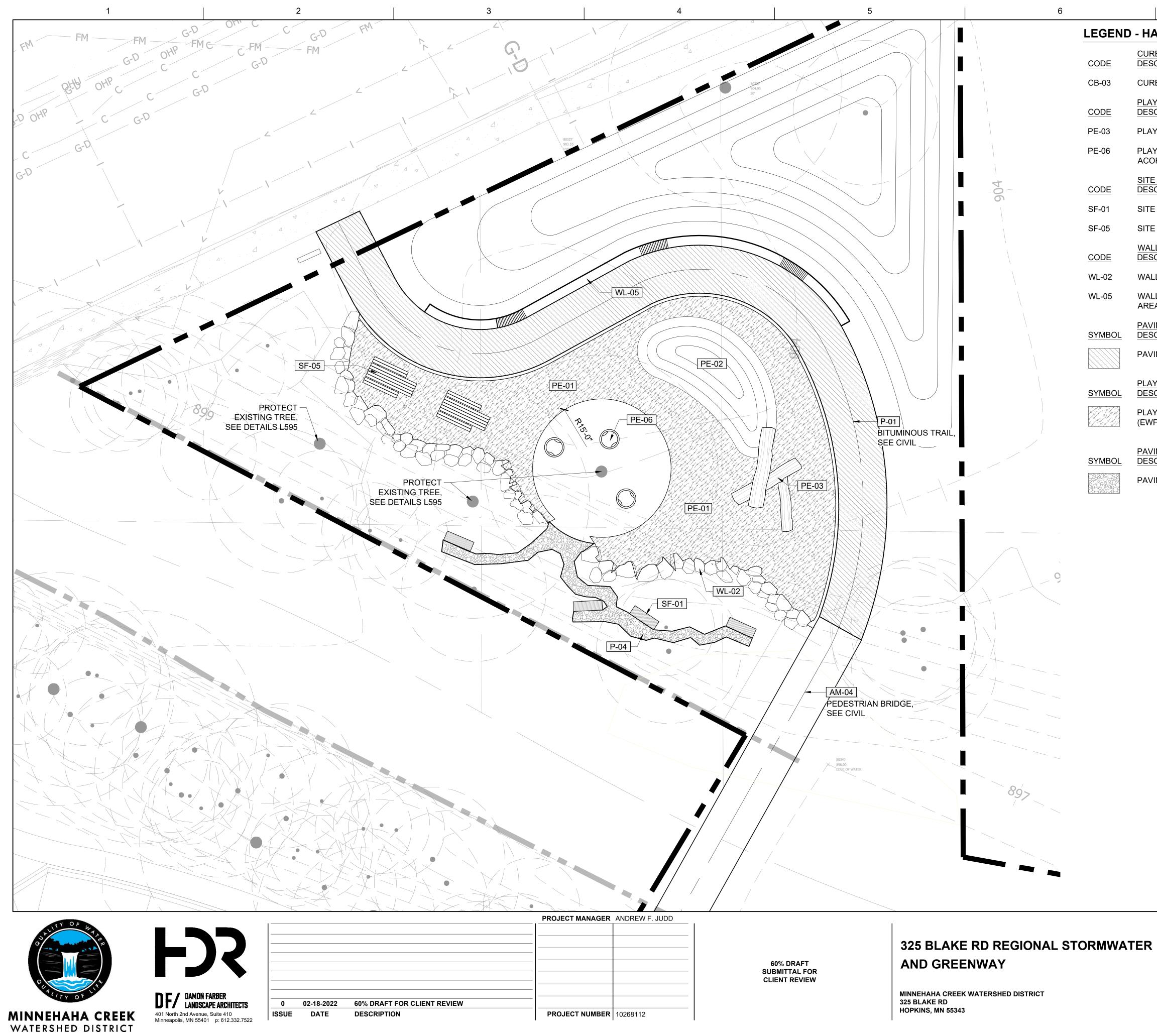




HARDSCAPE ENLARGEMENT P	LAN
LANDING	





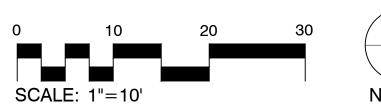






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SSUE	DATE	D

	7		8	
- HAR	DSCAPE ENLARGEMENT PLAN	NATURE PL	AY	
<u>CURB</u> DESCRI	PTION	QTY	DETAIL	
CURB T	YPE 03 - CIP CONCRETE PLAY AREA CURB	163 LF	3/L520	
PLAY EC DESCRI	QUIPMENT PTION	QTY	DETAIL	
PLAY EC	QUIPMENT TYPE 03 - LOG STACK	1		D
PLAY EC	QUIPMENT TYPE 05 - PRECAST CONCRETE S	3		
SITE FU DESCRI	RNITURE PTION	QTY	DETAIL	
SITE FU	RNITURE TYPE 01 - LINEAR BENCH	4	1/L570	
SITE FU	RNITURE TYPE 05 - PICNIC TABLE	2	1/L571	
<u>WALL</u> DESCRI	PTION	QTY	DETAIL	
WALL T	YPE 02 - LIMESTONE SEATWALL @ PLAY ARE	A 117 LF	2/L560	
WALL T` AREA	YPE 05 - CIP CONCRETE SEATWALL @ PLAY	98 LF	2/L561	
PAVING DESCRI	PTION	QTY	DETAIL	
PAVING	TYPE 01 - BITUMINOUS PAVING	1,854 SF		С
PLAY EC DESCRI	QUIPMENT PTION	<u>QTY</u>	DETAIL	
PLAY EC (EWF)	QUIPMENT TYPE 01 - WOOD FIBER SURFACIN	G 2,484 SF		
PAVING DESCRI	PTION	QTY	DETAIL	
PAVING	TYPE 04 - CRUSHED STONE SURFACING	2.81 CY	3/L510	
				1

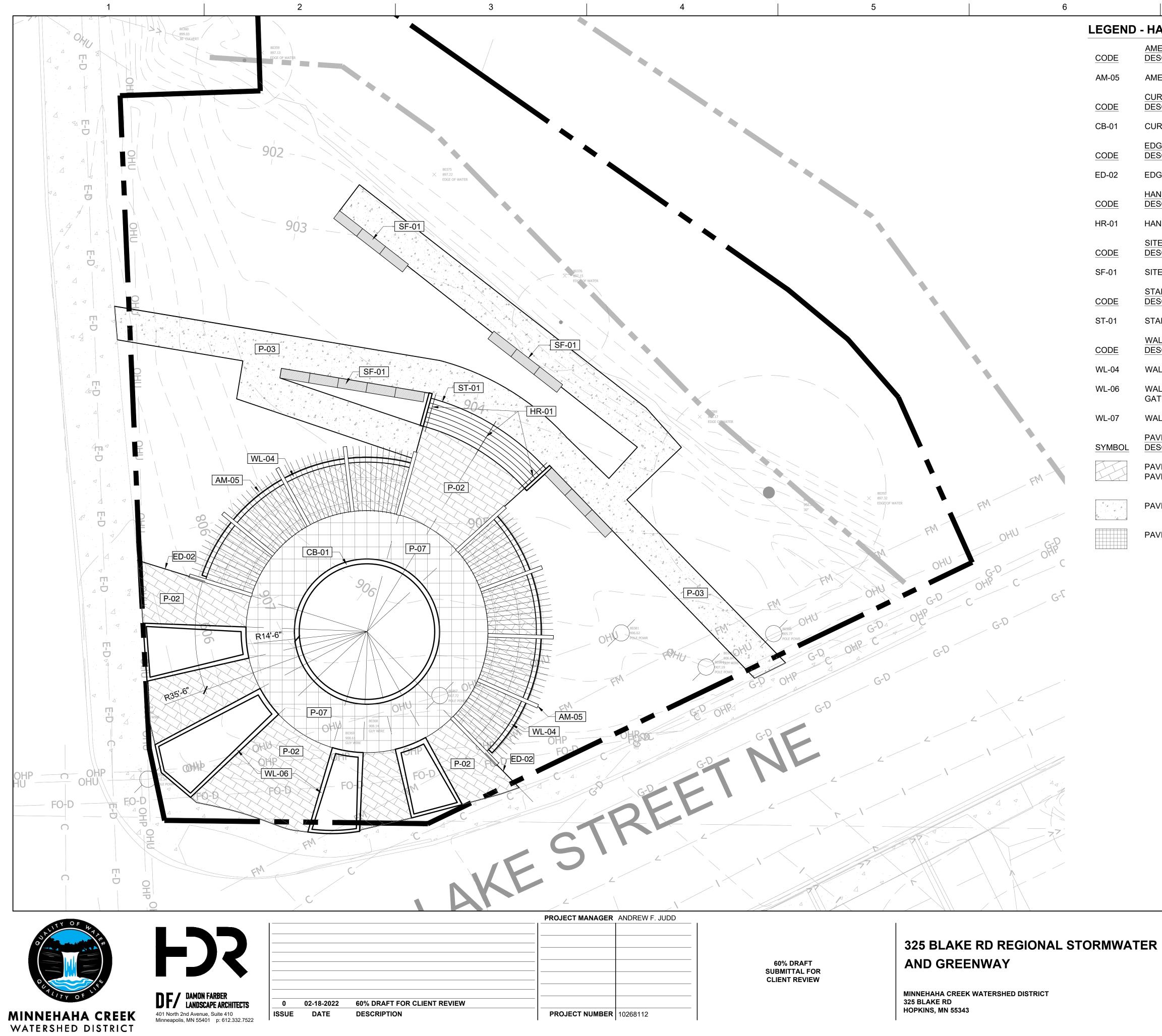






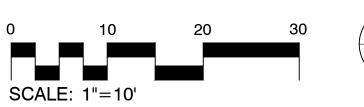






PROJECT MANAGER	ANDREW F. JUDD
	10269112

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- HARDSCAPE ENLARGEMENT PLAN G	ATEWAY PI	_AZA	
AMENITY DESCRIPTION	QTY	DETAIL	
AMENITY TYPE 05 - PERGOLA	2		
CURB DESCRIPTION	QTY	DETAIL	
CURB TYPE 01 - CIP CONCRETE PLANTER CURB	91 LF	1/L520	D
EDGING DESCRIPTION	QTY	DETAIL	
EDGING TYPE 02 - PAVER RESTRAINT	25 LF	3/L530	
HANDRAIL DESCRIPTION	QTY	DETAIL	
HANDRAIL TYPE 01 - STAIR HANDRAIL	24 LF	1/L550	
SITE FURNITURE DESCRIPTION	QTY	DETAIL	
SITE FURNITURE TYPE 01 - LINEAR BENCH	14	1/L570	
STAIRS DESCRIPTION	QTY	DETAIL	
STAIR TYPE 01 - RADIAL STAIR @ GATEWAY	6 LF	1/L540	
WALL DESCRIPTION	QTY	DETAIL	с
WALL TYPE 04 - CIP CONCRETE WALL	107 LF	2/L562	
WALL TYPE 06 - CIP CONCRETE PITCHED SEATWALL @ GATEWAY) 218 LF	1/L562	
WALL TYPE 07 - CIP CONCRETE CHEEK WALL	14 LF	2/L540	
PAVING DESCRIPTION	QTY	DETAIL	
PAVING TYPE 02 - PERMEABLE CONCRETE UNIT PAVERS	4,378 SF	1/L510	-
PAVING TYPE 03 - CONCRETE PAVING	2,071 SF	2/L510	
PAVING TYPE 07 - DECORATIVE CONCRETE PAVING	1,256 SF		

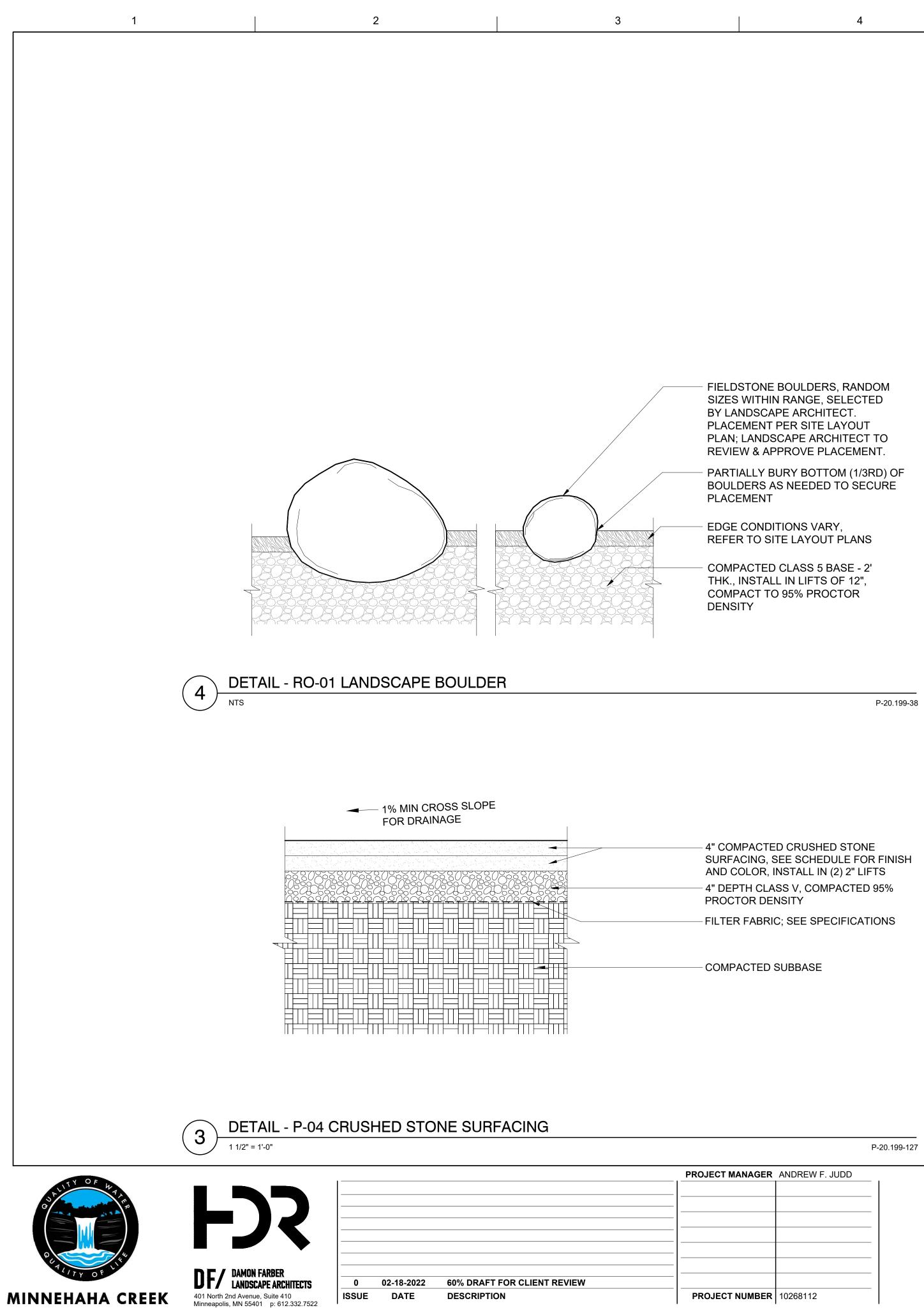












WATERSHED DISTRICT

- DEPTH OF CUT TO BE 1/3 THE DEPTH OF SLAB; MAKE FIELDSTONE BOULDERS, RANDOM ALL SAW CUTS WITHIN 12 HR. OF CONCRETE POUR - 1/4" THICK CUT PLAN; LANDSCAPE ARCHITECT TO PARTIALLY BURY BOTTOM (1/3RD) OF BOULDERS AS NEEDED TO SECURE A **TYPICAL SAWCUT CONTROL JOINT** CONCRETE FINISH TO BE XXX SEE CIVIL DETAILS FOR TYPICAL **TYPICAL EXPANSION JOINT - ENLARGED** CONCRETE AND BASE MATERIAL PROFILES DETAIL - P-03 CONCRETE PAVING TYPICAL JOINTING 2 NTS

5

- SURFACING, SEE SCHEDULE FOR FINISH 4" DEPTH CLASS V, COMPACTED 95%
- FILTER FABRIC; SEE SPECIFICATIONS

CROSS SLOPE <u>│</u>╞═╡║┃╞═╪**┽**╎┇



DETAIL - P-02 PERMEABLE CONCRETE UNIT PAVERS 1 1/2" = 1'-0"

60% DRAFT SUBMITTAL FOR CLIENT REVIEW

325 BLAKE RD REGIONAL STORMWATER **AND GREENWAY**

MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343





— MASTIC SEALANT, PER SPECIFICATIONS;
COLOR TO MATCH ADJACENT PAVING. WIDTH
TO DEPTH RATIO OF MASTIC TO BE PER
MANUFACTURER'S RECOMMENDATIONS.

7

- CLOSED CELL FOAM BACKER ROD
- TYPICAL EDGE, FORM AT 90 DEGREES TO APPEAR SIM. TO CONTROL JOINT EDGE PREMOLDED EXPANSION JOINT FILLER PER SPECIFICATIONS
- EXPANSION JOINT TO OCCUR 20' O.C. MAX. AND AT CONSTRUCTION JOINTS, RAMPS, WALLS, AND OTHER VERTICAL OBSTRUCTIONS. REFER TO PLAN FOR LOCATIONS

P-20.199-106

- SEE PLAN FOR ADJACENT CONDITIONS
- PERMEABLE PAVER WITH 3/8" JOINTS FILLED TO TOP SURFACE, TYP. - 2" BEDDING COURSE OF 3/8" OPEN-GRADED AGGREGATE (ASTM NO. 8) 4" BASE COURSE OF 3/4" TO 1"
- OPEN-GRADED AGGREGATE (ASTM NO. 57 CRUSHED) 12" SUB-BASE COURSE OF 2" TO 3"
- OPEN-GRADED AGGREGATE (ASTM NO. 2)
- SUB-GRADE SOIL (NON-COMPACTED, ZERO SLOPE)

P-20.199-126

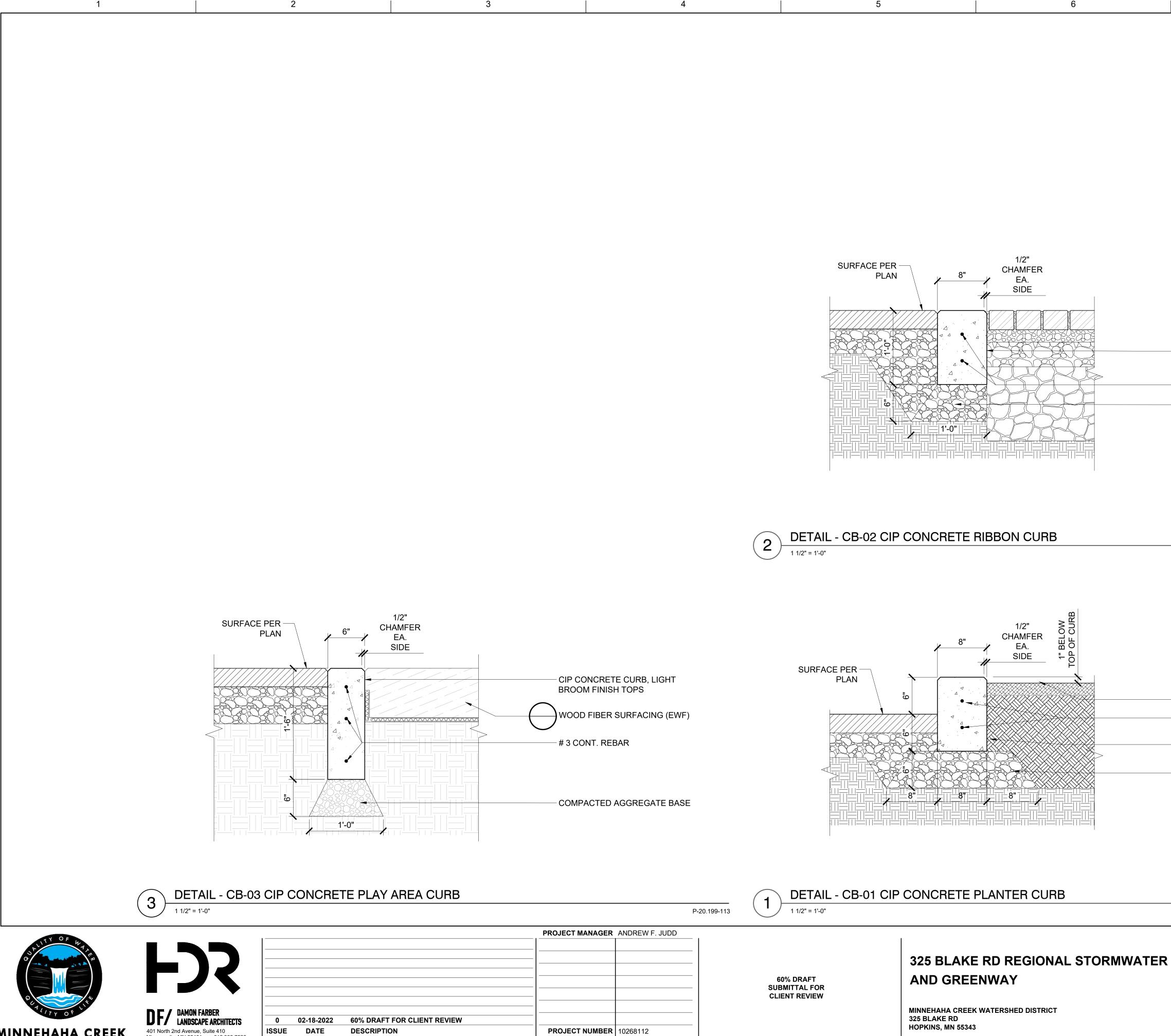


LANDSCAPE DETAILS PAVING

FILENAME SCALE SHEET L510

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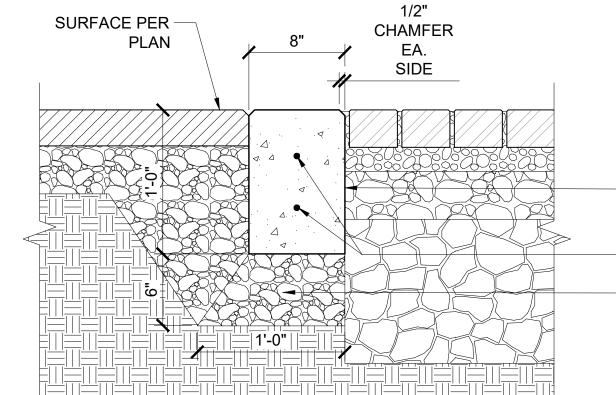
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MINNEHAHA CREEK WATERSHED DISTRICT

401 North 2nd Avenue, Suite 410 Minneapolis, MN 55401 p: 612.332.7522

2022	60% DRAFT FOR CLIENT REVIEW	
ΓE	DESCRIPTION	





- CIP CONCRETE CURB, LIGHT **BROOM FINISH TOPS**

-#3 CONT. REBAR

- COMPACTED AGGREGATE BASE

P-20.199-111

- MULCH & PLANTING SOIL DEPTH PER SPEC.

-# 3 CONT. REBAR

- CIP CONCRETE CURB, LIGHT **BROOM FINISH TOPS**

- COMPACTED AGGREGATE BASE

P-20.199-110



FILENAME

SCALE



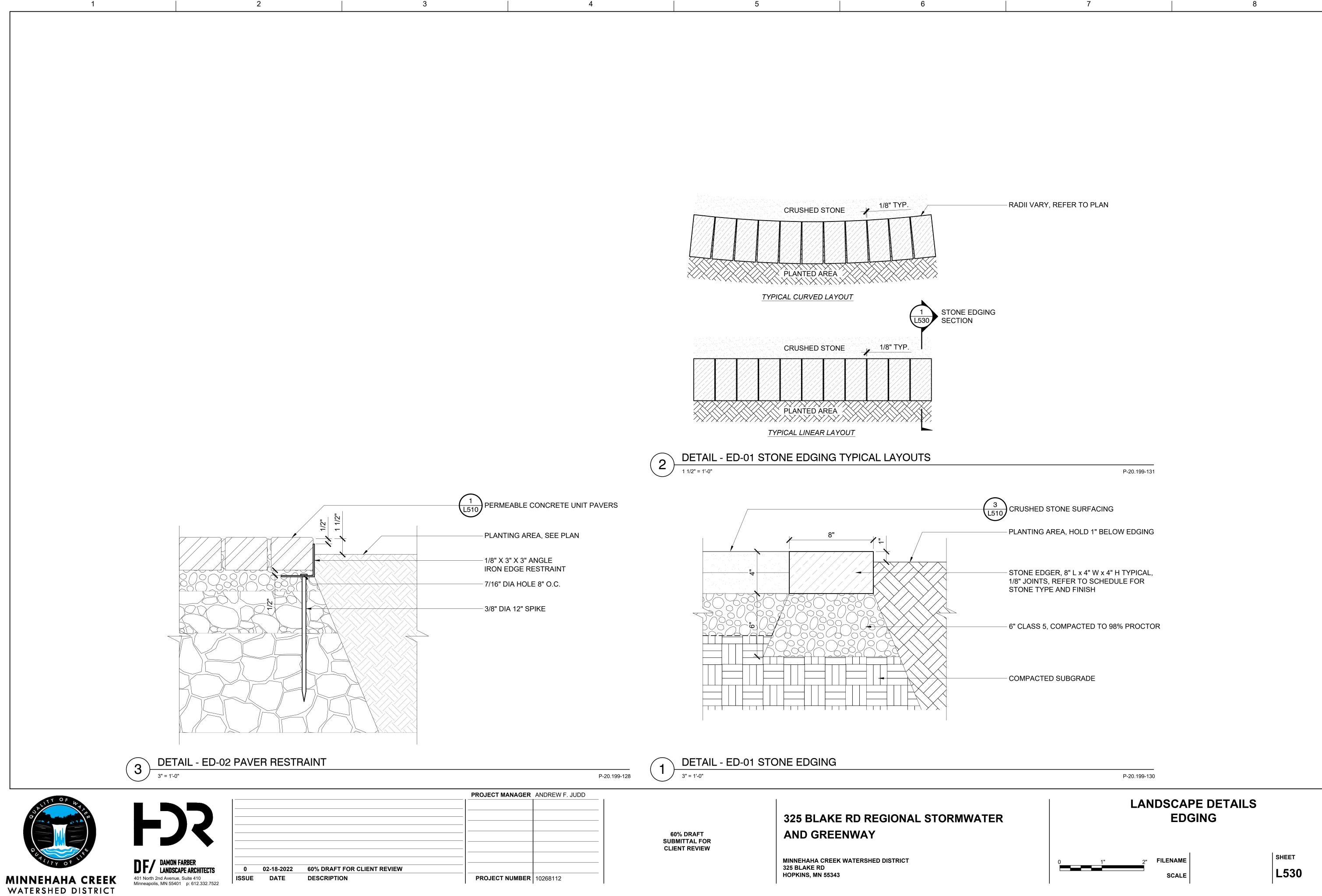
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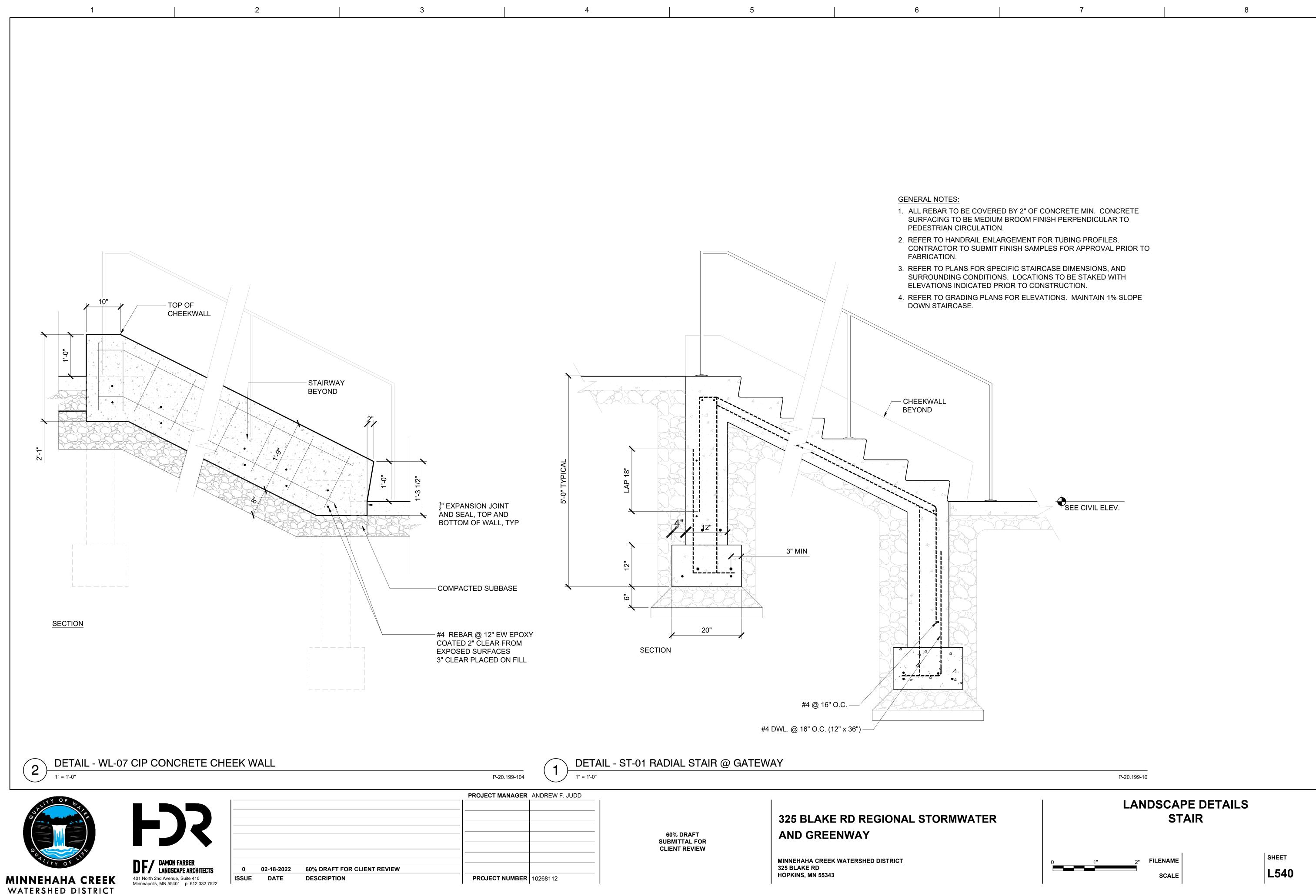
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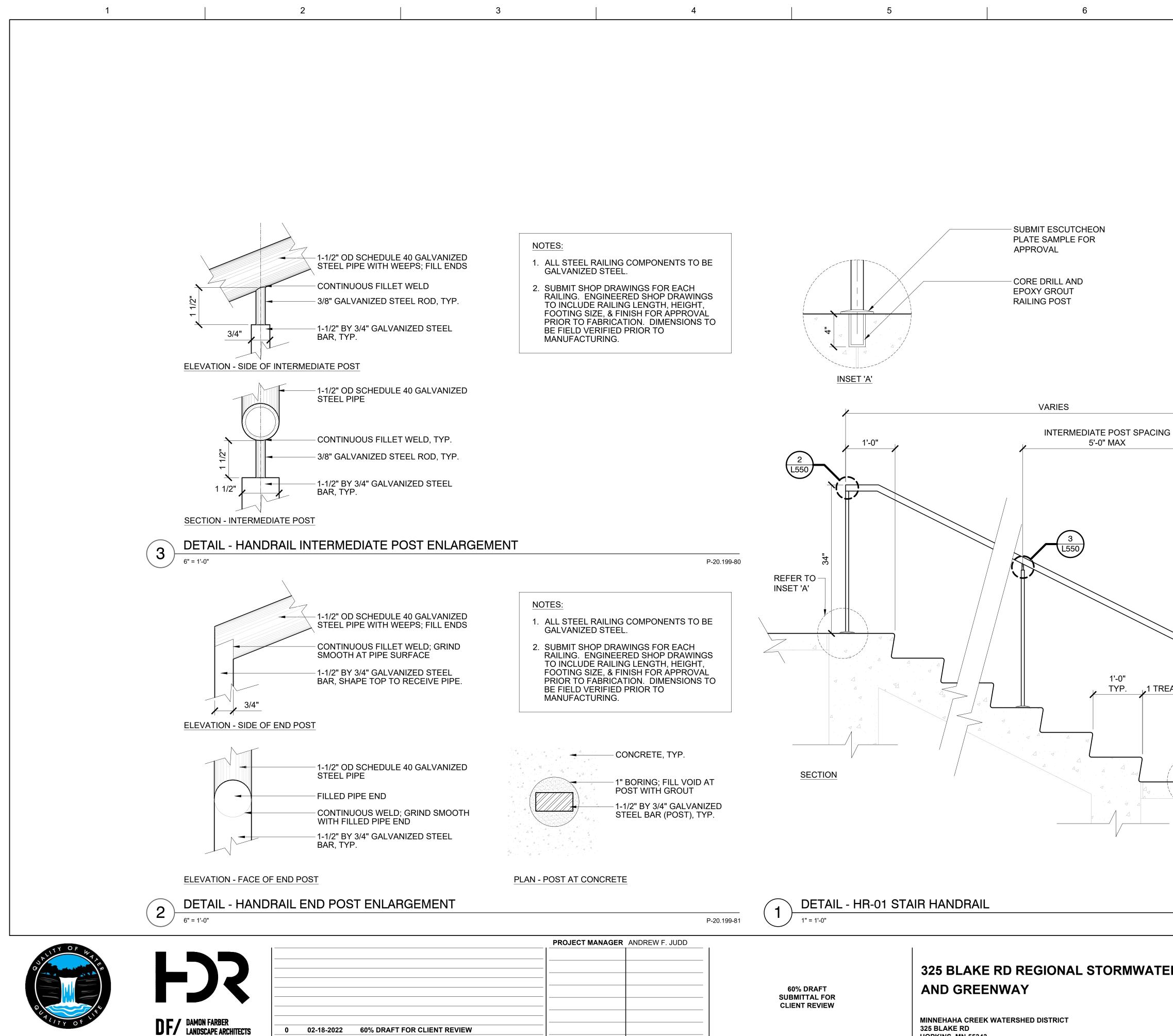
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MINNEHAHA CREEK WATERSHED DISTRICT

401 North 2nd Avenue, Suite 410 Minneapolis, MN 55401 p: 612.332.7522

02-18-2022 60% DRAFT FOR CLIENT REVIEW ISSUE DATE DESCRIPTION

325 BLAKE RD REGIONAL STORMWATER 325 BLAKE RD HOPKINS, MN 55343 PROJECT NUMBER 10268112

1'-0"

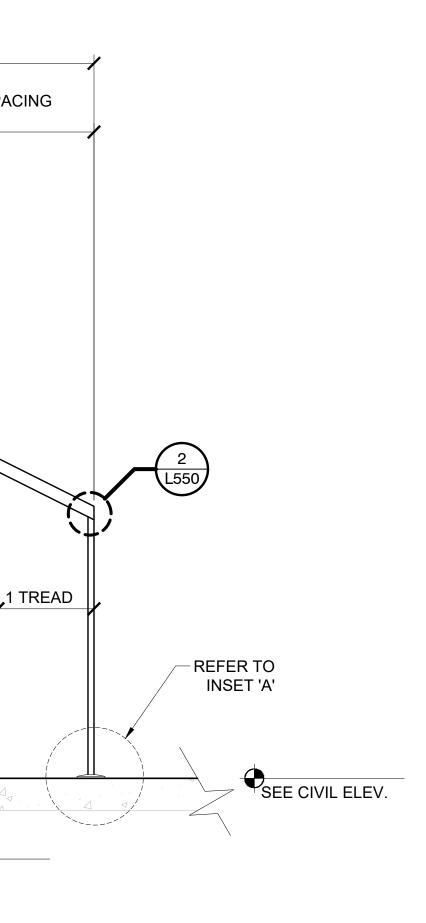
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GENERAL NOTES:

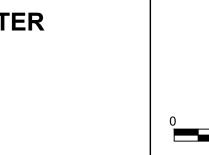
1. REFER TO HANDRAIL ENLARGEMENT FOR TUBING PROFILES. CONTRACTOR TO SUBMIT FINISH SAMPLES FOR APPROVAL PRIOR TO FABRICATION.

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- 2. REFER TO PLANS FOR SPECIFIC STAIRCASE DIMENSIONS, AND SURROUNDING CONDITIONS.
- 3. REFER TO GRADING PLANS FOR ELEVATIONS.



P-20.199-82

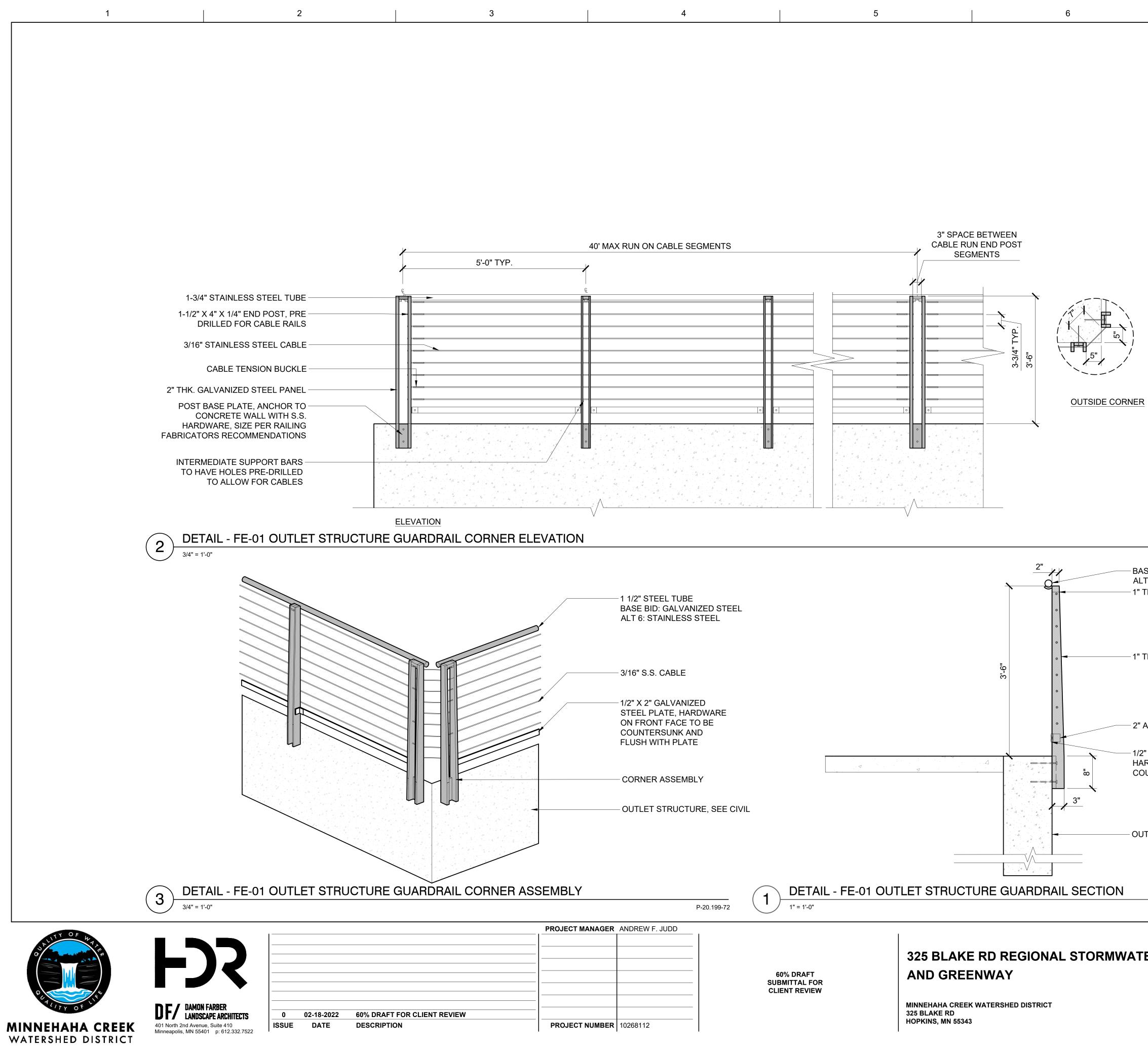


LANDSCAPE DETAILS HANDRAIL & GUARDRAIL

FILENAME SCALE SHEET L550

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	- 1/2" X 2" GALVANIZE STEEL PLATE, HARE ON FRONT FACE TO COUNTERSUNK AND FLUSH WITH PLATE - CORNER ASSEMBLY	DWARE) BE D	· · · · · · · · · · · · · · · · · · ·			2" / 1/2 HA CC
EMBLY	P	DETA 1 -20.199-72	NIL - FE-01 OU7	LET STRUCTURE G	JUARDRAIL SECT	
PROJECT MANAGER		60% DRAFT SUBMITTAL FO CLIENT REVIEW		325 BLAKE RD R AND GREENWA MINNEHAHA CREEK WATERSH 325 BLAKE RD HOPKINS, MN 55343	Y	RWMT

NOTE:

1. ALL METAL BARS & TUBES ARE TO BE GALVANIZED, WELDED PRIOR TO GALVINIZATION. SUBMIT SAMPLES FOR APPROVAL.

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- 2. JOINTS TO BE WELDED BETWEEN BARS & TUBES, CUSTOM CUT ANGLE OF POST TO TOP RAIL CONNECTIONS ON SLOPED WALLS.
- 3. ALL POSTS TO BE SET PLUMB, WELDED TO BASE PLATE AND ANCHORED TO CONCRETE WALLS WITH FABRICATOR RECOMMENDED FASTENERS.
- 4. CONTRACTOR TO SUBMIT SHOP DRAWINGS FOR REVIEW PRIOR TO APPROVING FABRICATION OF ANY GUARDRAIL COMPONENTS.
- 5. TENSION & ANCHOR HARDWARE TO BE STAINLESS STEEL, SIZE PER FABRICATORS **RECOMMENDATIONS.**

P-20.199-33

- BASE BID: 1 1/2" GALVANIZED HANDRAIL ALTERNATE 6: STAINLESS STEEL - 1" THICK BRACKET WELDED TO POST

-1" THICK GALVANIZED STEEL PLATE

ANGLE IRON BOTTOM RAIL BRACKET

/2" X 2" GALVANIZED STEEL PLATE, ARDWARE ON FRONT FACE TO BE OUNTERSUNK AND FLUSH WITH PLATE

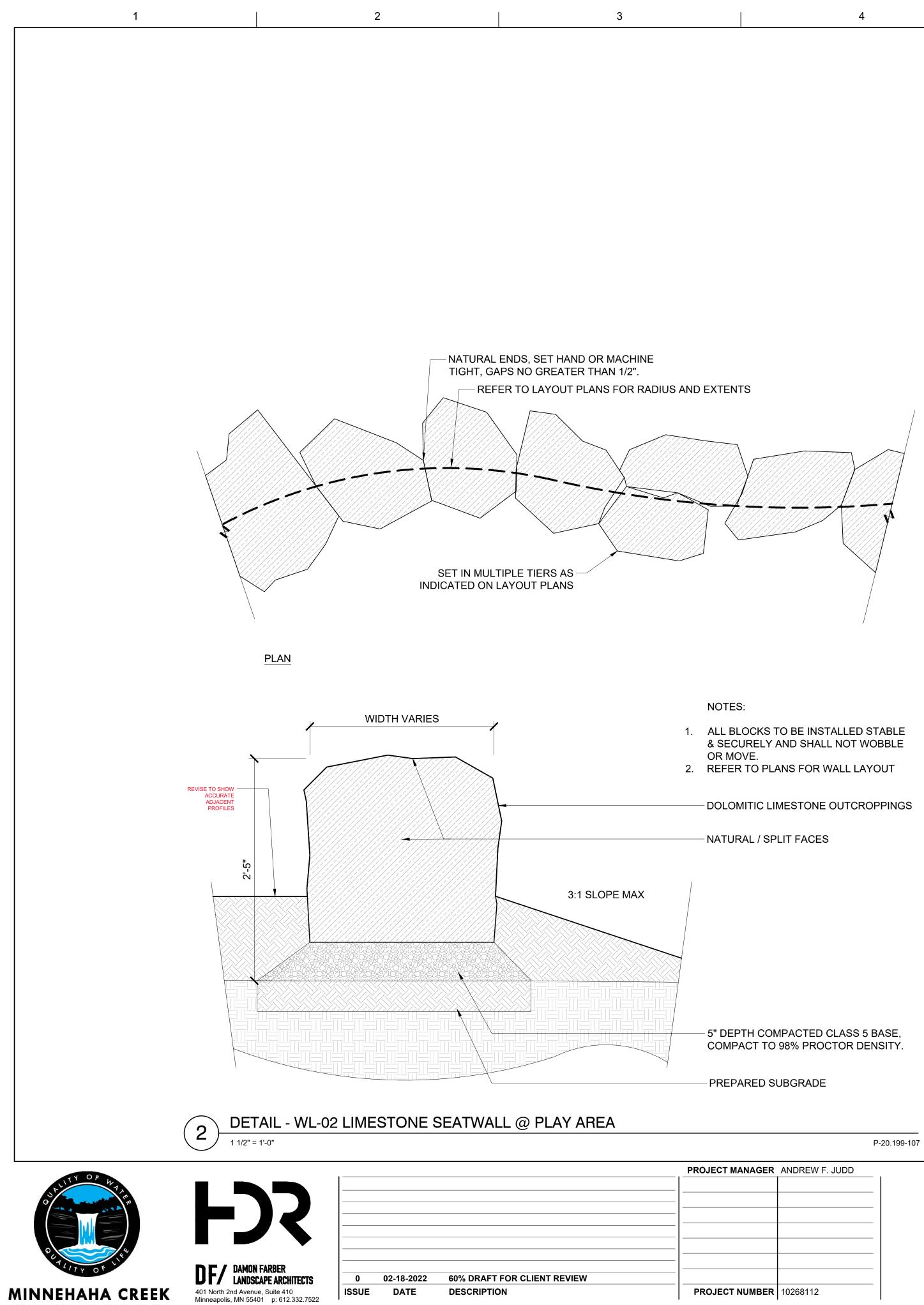
UTLET STRUCTURE, SEE CIVIL

P-20.199-34 LANDSCAPE DETAILS HANDRAIL & GUARDRAIL TER SHEET FILENAME L551 SCALE

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WATERSHED DISTRICT

COMPACT TO 9	PACTED CLASS 5 BA 8% PROCTOR DENS		
PREPARED SUI	BGRADE		
		DETAIL - WL-01 LIN	IESTONE SEATWALL @ TRAILHEAD
	P-	20.199-107 1 1/2" = 1'-0"	
	ANDREW F. JUDD	I	
			325 BLAKE RD REGIONAL STORMWAT
		60% DRAFT SUBMITTAL FOR	AND GREENWAY
		CLIENT REVIEW	
			MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD
PROJECT NUMBER 1	10268112		HOPKINS, MN 55343
•	·	•	

PLAN

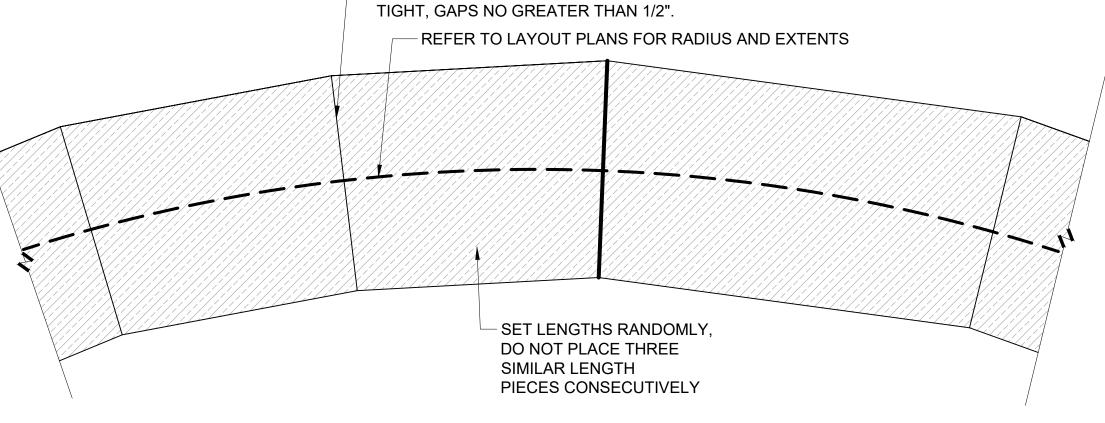
REVISE TO SHOW PREFERRED PERMEABLE PAVING DETAIL

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2'-0"

SLOPE 1/4" / FT

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3:1 SLOPE MAX

– SAW CUT ENDS, SET HAND OR MACHINE

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NOTES:

1. ALL BLOCKS TO BE INSTALLED STABLE & SECURELY AND SHALL NOT WOBBLE OR MOVE. 2. REFER TO PLANS FOR WALL LAYOUT

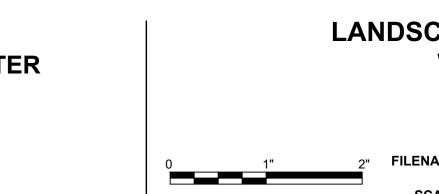
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- DOLOMITIC LIMESTONE BLOCKS
- SAWN TOP AND BUTT ENDS
- SPLIT FRONT FACE

5" DEPTH COMPACTED CLASS 5 BASE, COMPACT TO 98% PROCTOR DENSITY.

PREPARED SUBGRADE

P-20.199-21



LANDSCAPE DETAILS WALL

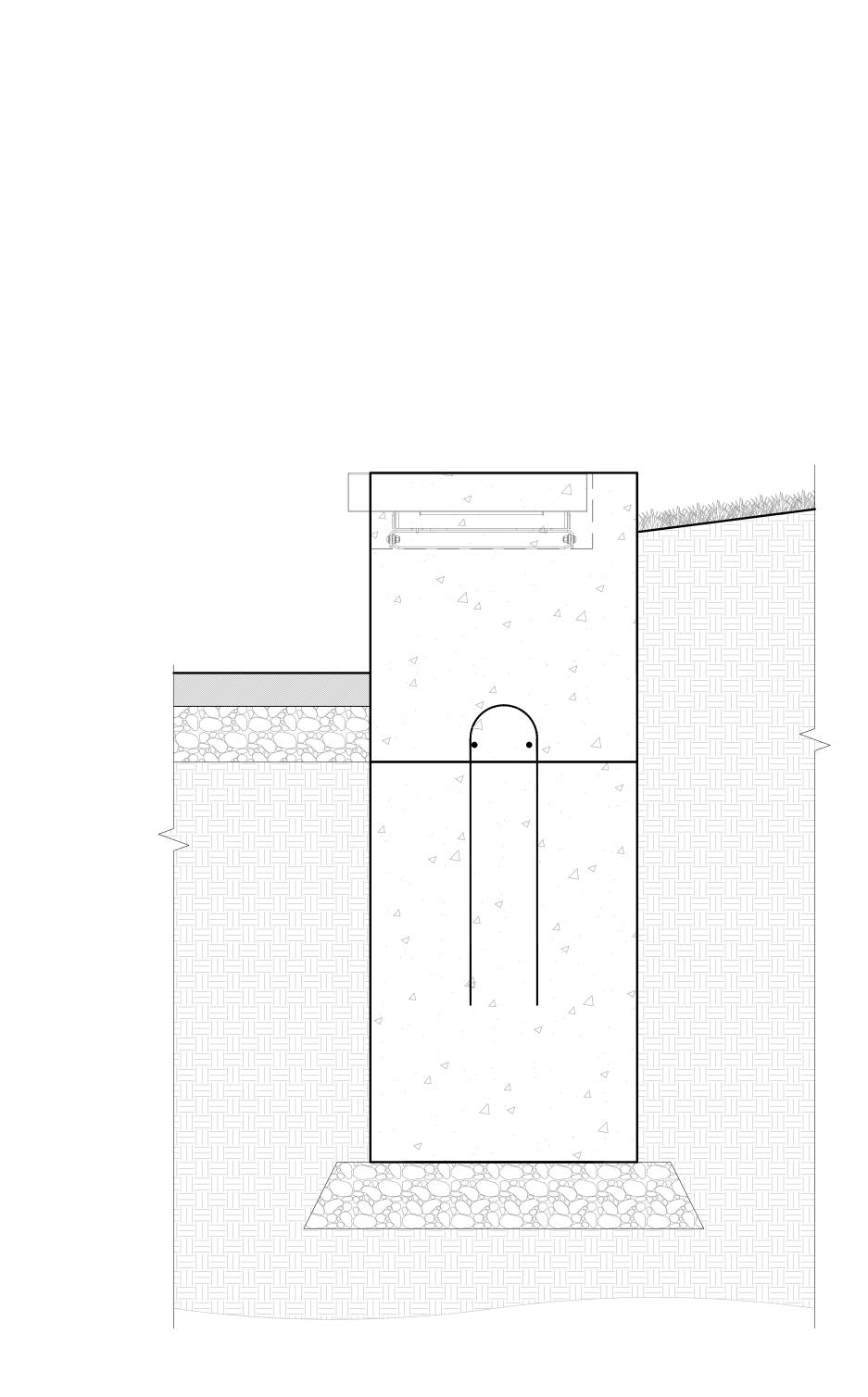
FILENAME SCALE SHEET L560

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DETAIL - WL-04 CIP CONCRETE SEATWALL @ PLAY AREA 2 1 1/2" = 1'-0"



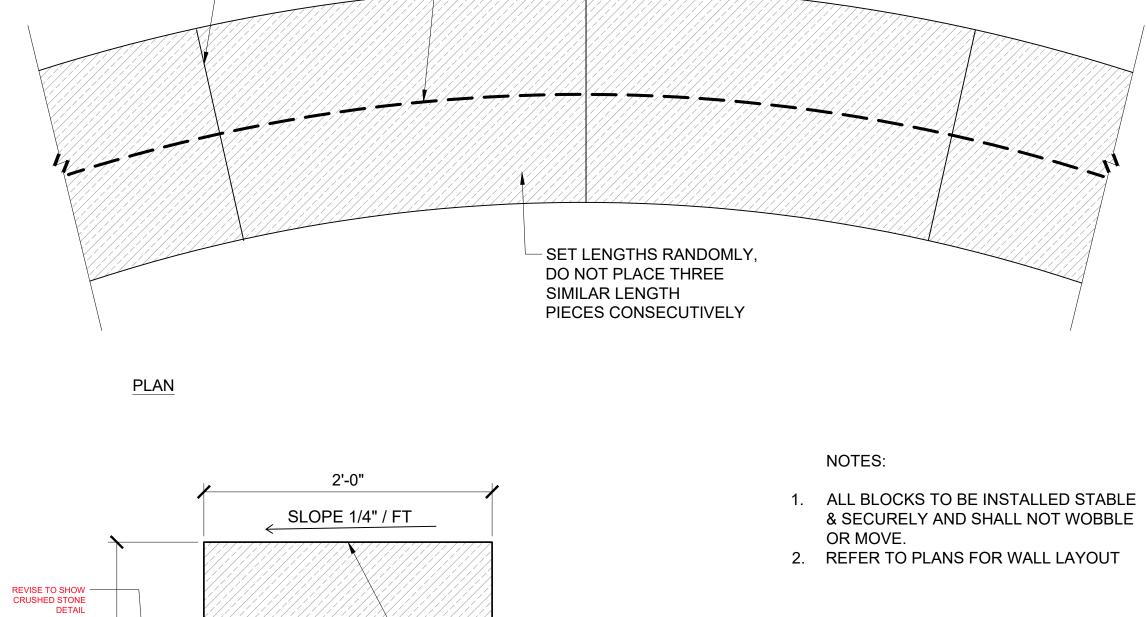


0	02-18-2022	60% DRAFT FOR CLIENT REVIEW
		DESCRIPTION

		P-20.199-108	1 1/2" = 1'-0"	
PROJECT MANAGER	ANDREW F. JUDD	- 1		
			60% DRAFT SUBMITTAL FOR CLIENT REVIEW	325 BLAKE RD REGIONAL STORMWATER AND GREENWAY
		_		MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD
PROJECT NUMBER	10268112	-		HOPKINS, MN 55343

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3:1 SLOPE MAX

- SAW CUT ENDS, SET HAND OR MACHINE TIGHT, GAPS NO GREATER THAN 1/2". - REFER TO LAYOUT PLANS FOR RADIUS AND EXTENTS

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DETAIL - WL-03 LIMESTONE SEATWALL @ PICNIC AREA

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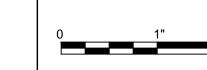
- DOLOMITIC LIMESTONE BLOCKS
- ALL FACES AND ENDS TO BE SAW CUT

- 5" DEPTH COMPACTED CLASS 5 BASE, COMPACT TO 98% PROCTOR DENSITY.

- PREPARED SUBGRADE

P-20.199-133





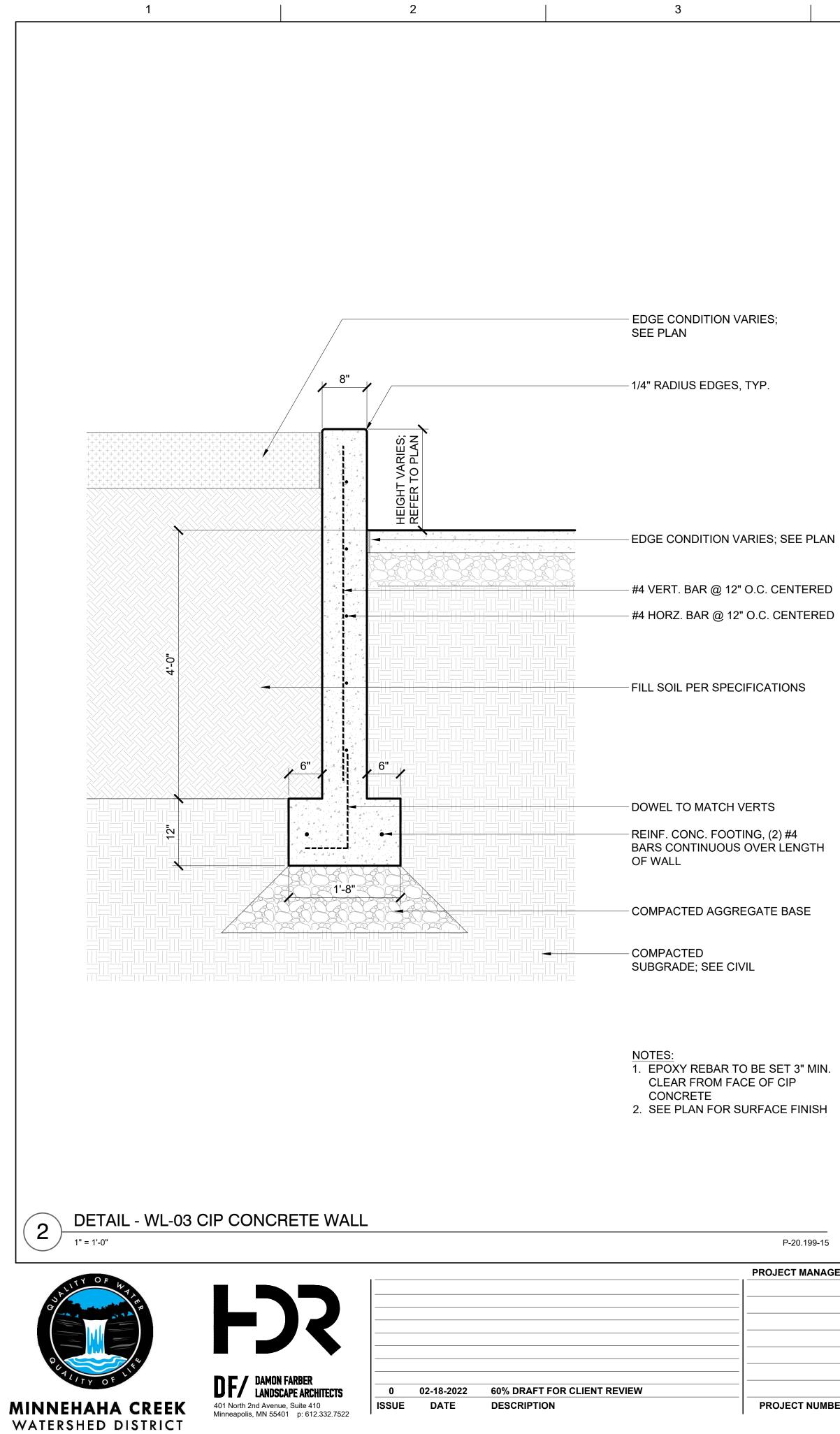
FILENAME SCALE SHEET L561

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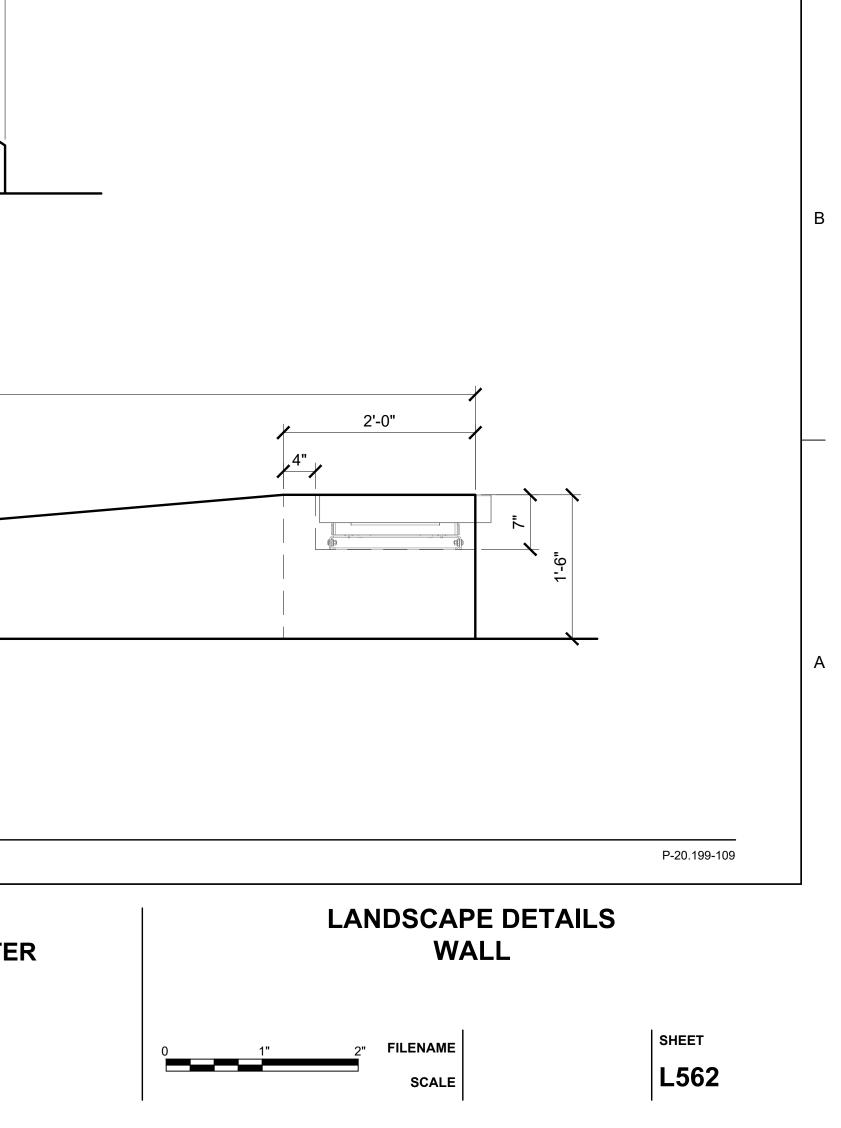
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GATE BASE VARIES, SEE LAYOUT PL	_AN
BE SET 3" MIN.	
JRFACE FINISH	
DETAIL - WL-05 CIP CONCRETE PITCHED SEATWALL @ GATEWAY	
P-20.199-15 1" = 1'-0"	
PROJECT MANAGER ANDREW F. JUDD	TORMWAT
60% DRAFT SUBMITTAL FOR CLIENT REVIEW	
MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343	

VARIOUS, SEE LAYOUT PLAN 6'-6" 5'-10" Tofo

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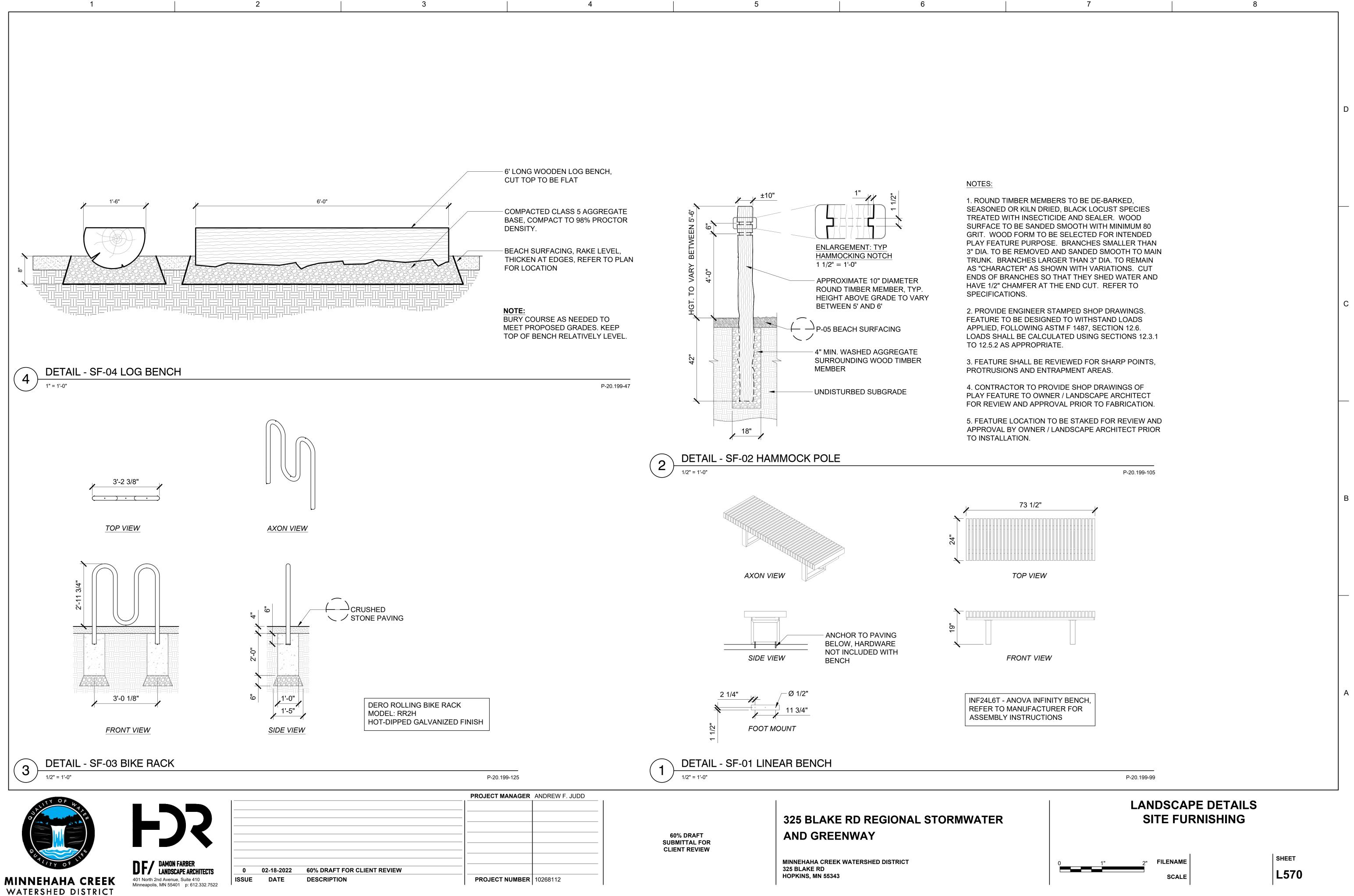


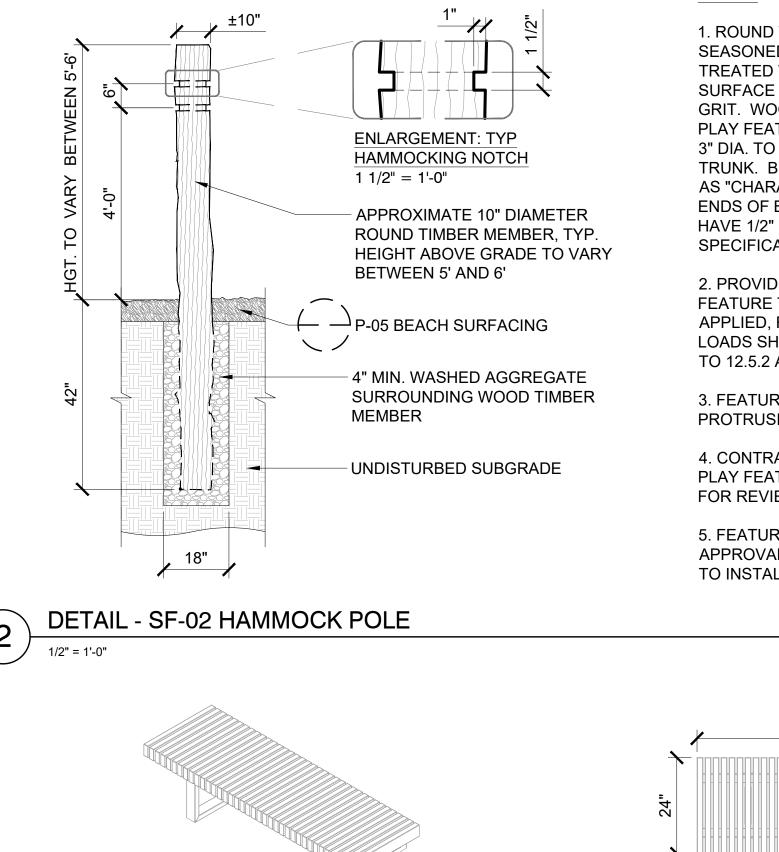
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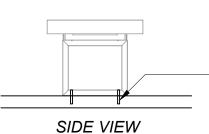
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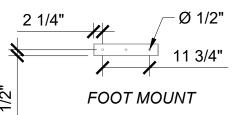
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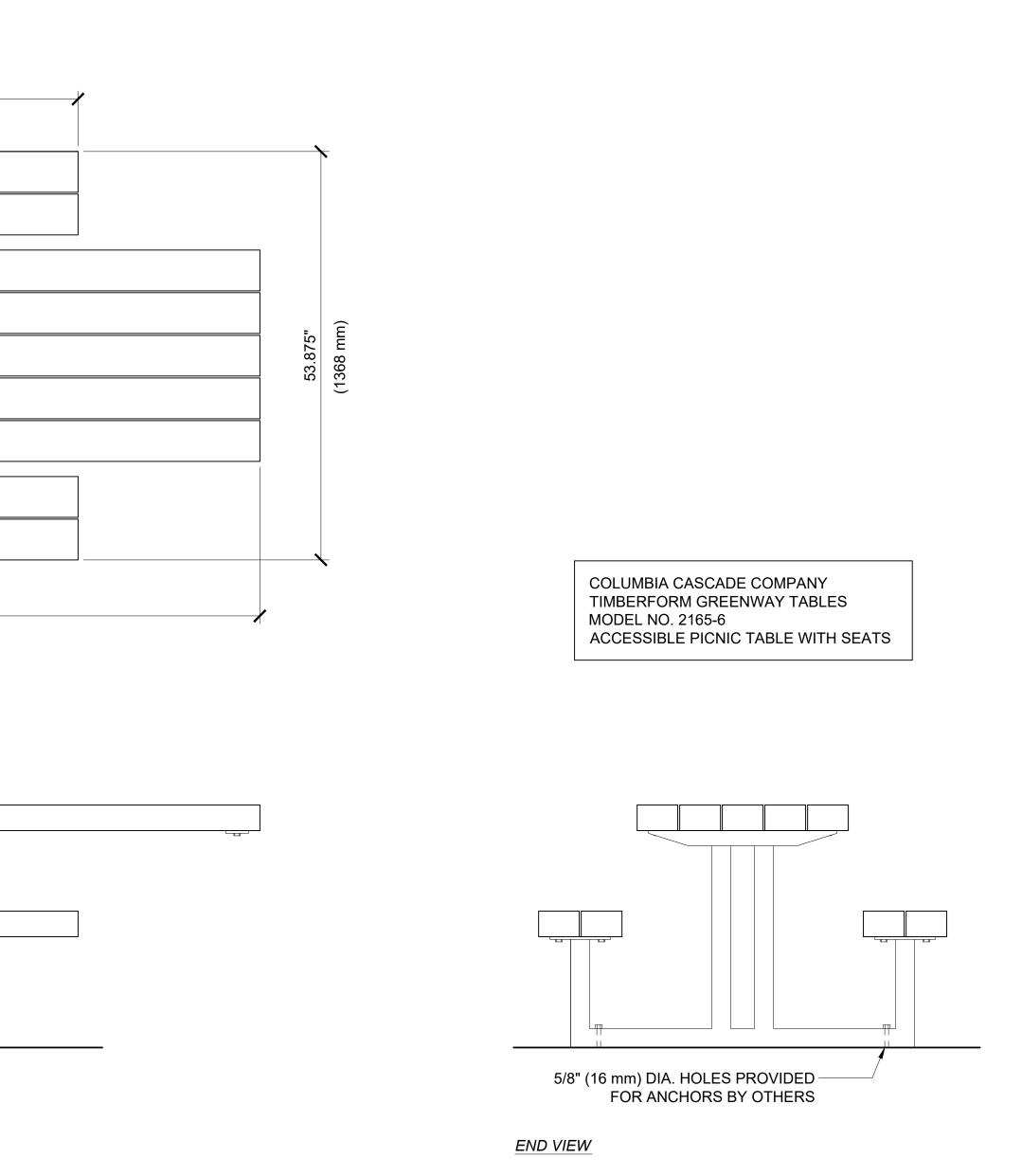


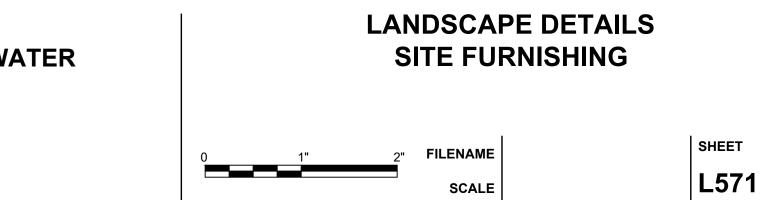


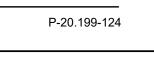
	P-20.199-105
73 1/2"	
TOP VIEW	
FRONT VIEW	
L6T - ANOVA INFINITY BENCH, R TO MANUFACTURER FOR MBLY INSTRUCTIONS	

		94 (2388		TIMBERF MODEL N	IA CASCADE COMPANY FORM GREENWAY TABLES NO. 2165-6 IBLE PICNIC TABLE WITH SEATS
		TOP VIEW		ACCESS	IDLE FICINIC TADLE WITH SEATS
	2'-8" (813 mm)				
	<u>1'-6"</u> (457 mm)				
	0'-0" FINISHED GRADE				DIA. HOLES PROVIDED
		FRONT VIEW		END VIEW	
	1 DETAIL - SF-05	5 PICNIC TABLE			
TY OF			PROJECT MANAGER ANDREW F. J	JUDD	
SUPER THE PARTY OF					
	トノく			60% DRAFT SUBMITTAL FOR CLIENT REVIEW	325 BLAKE RD REGIONAL STORMWA AND GREENWAY
ALITYOF	DF / DAMON FARBER LANDSCAPE ARCHITECTS	0 02-18-2022 60% DRAFT FOR CLIENT REVIEW			MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD
MINNEHAHA CREEK WATERSHED DISTRICT	401 North 2nd Avenue, Suite 410 Minneapolis, MN 55401 p: 612.332.7522	ISSUE DATE DESCRIPTION	PROJECT NUMBER 10268112		HOPKINS, MN 55343

	70"	
	(1778 mm)	
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	0.4"	

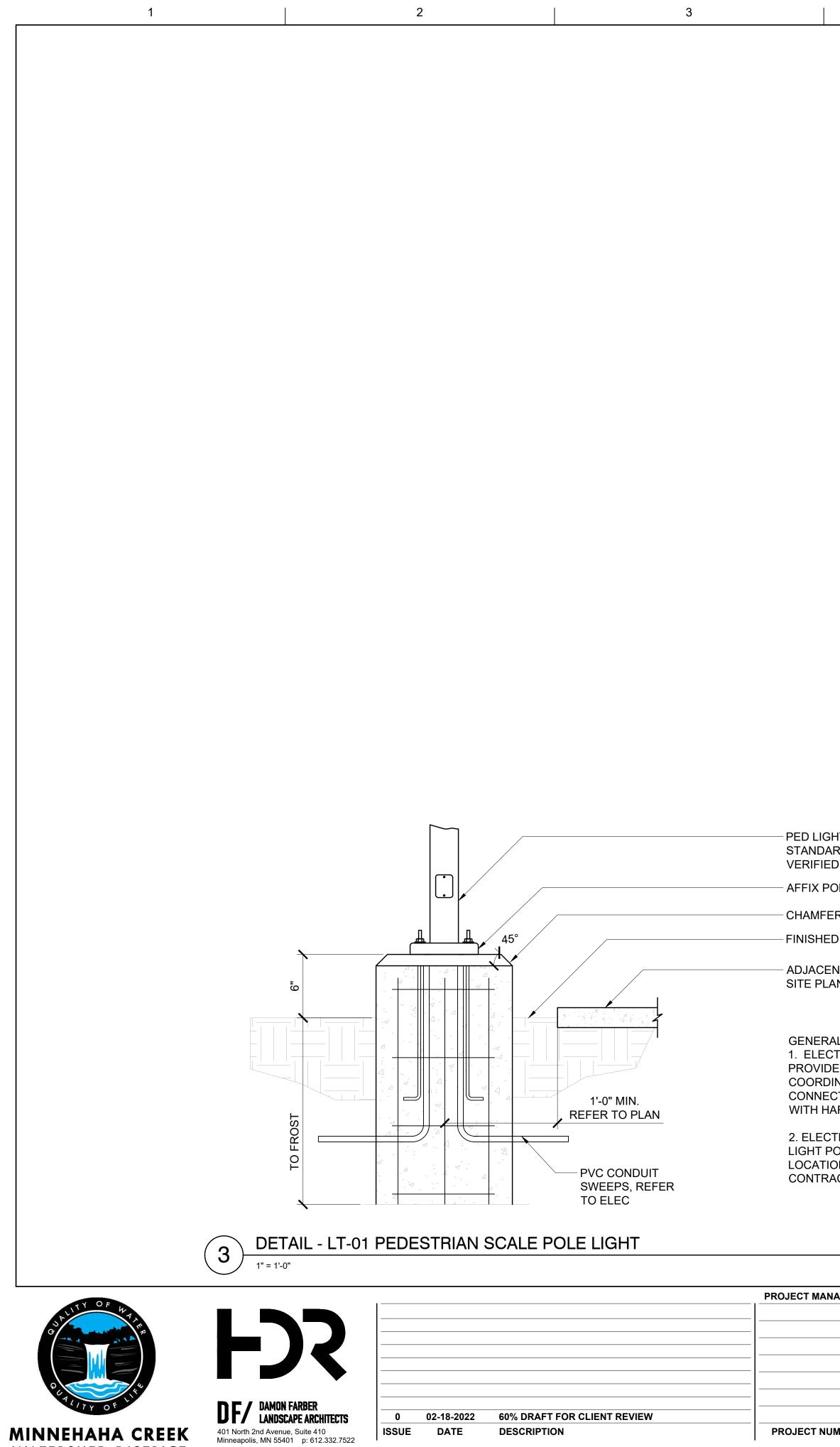






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WATERSHED DISTRICT

GENERAL NOTES: 1. ELECTRICAL CONTRACTOR TO PROVIDE CONDUIT & WIRING, COORDINATE SLEEVING, UTILITY CONNECTIONS, AND WIRING LAYOUT WITH HARDSCAPE CONTRACTOR. 2. ELECTRICAL CONTRACT TO PROVIDE LIGHT POLE BASES. COORDINATE LOCATIONS WITH HARDSCAPE CONTRACTOR.		DRAIN HOLES, TYP.		RODS, INCLUDED BY VENDOR 4" THK. CONC. BASE COMPACTED AGGREGATE BASE
P-20.199-95	1 DETAIL - SF-06 \ 3/4" = 1'-0"	WASTE RECEPT	ACLE	
ROJECT MANAGER ANDREW F. JUDD	60% DRAFT SUBMITTAL FOR CLIENT REVIEW		E RD REGIONAL STORMWAT ENWAY	ER
PROJECT NUMBER 10268112		325 BLAKE RD HOPKINS, MN 5534		

PED LIGHT POLE TO MATCH COMMUNITY STANDARD. COLOR TO BE SELECTED & VERIFIED BY LANDSCAPE ARCHITECT.

AFFIX POLE TO BASE PER MFR

- FINISHED GRADE, CONDITION VARIES

- ADJACENT CONDITIONS VARY, REFER TO

- CHAMFER EDGE

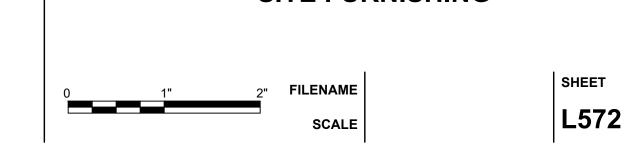
SITE PLANS

- TOP LOCATION (3 PLACES) TOP VIEW

> ANCHOR HOLES

2'-0" NOM.

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- SIDE DECAL LOCATION

(3 PLACES)

PAVER THICKNESS

- CONCRETE PAVERS, CONFIRM

P-20.199-79

LANDSCAPE DETAILS SITE FURNISHING

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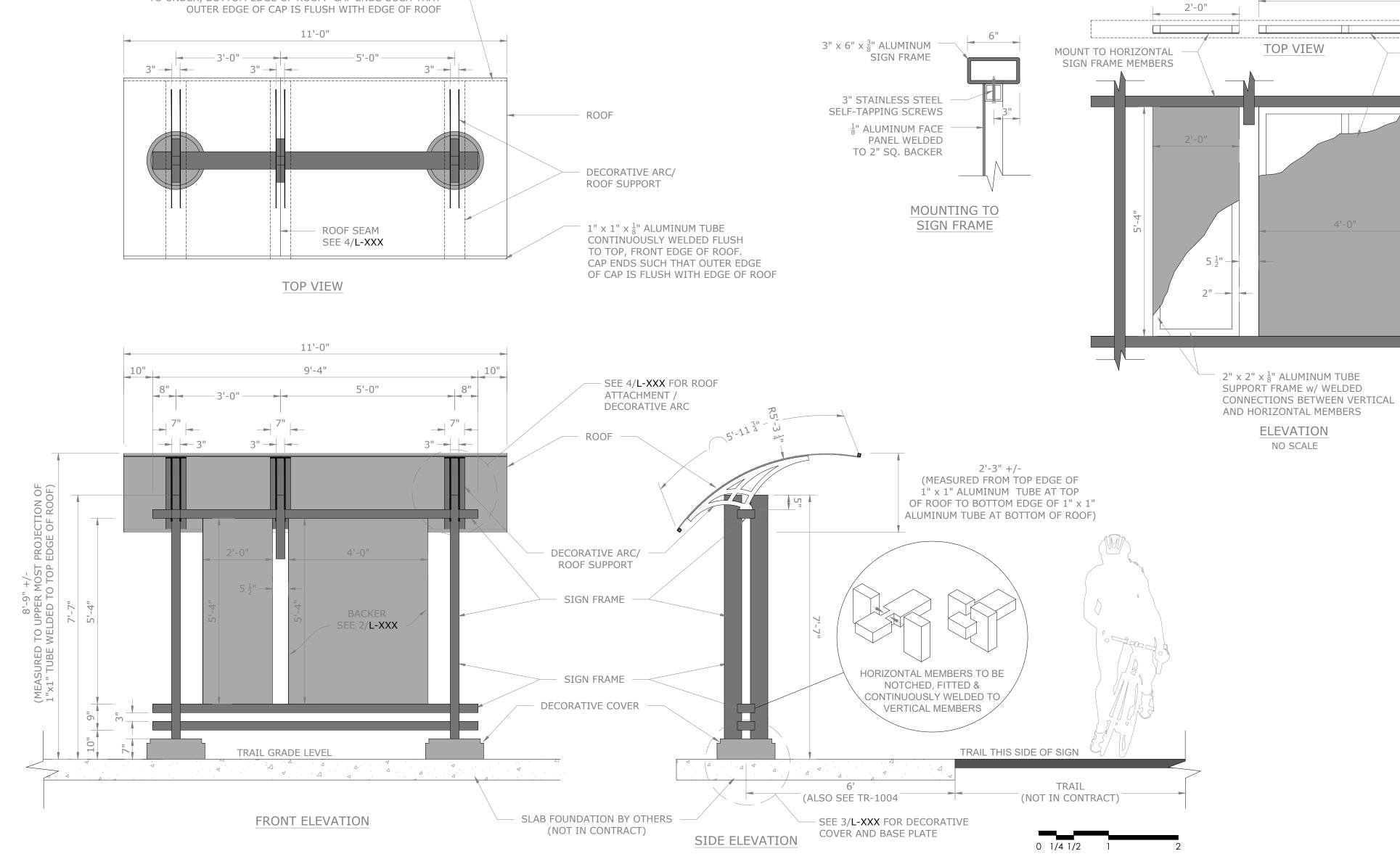
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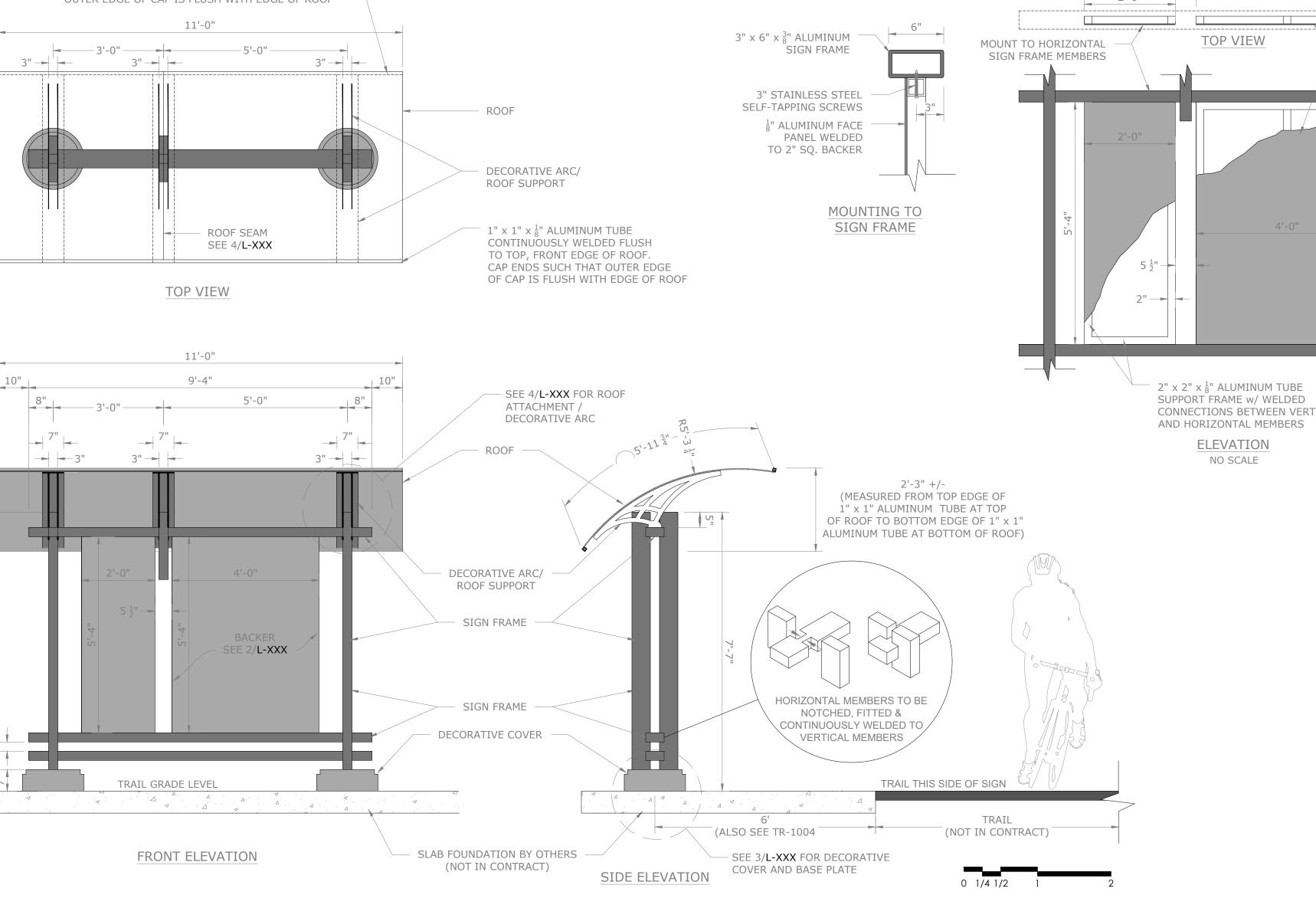
	PROJECT MANAGER	ANDREW F. JUDD	
	·		60% DRAFT SUBMITTAL FOR CLIENT REVIEW
0 02-18-2022 60% DRAFT FOR CLIENT REVIEW			
ISSUE DATE DESCRIPTION	PROJECT NUMBER	10268112	

DETAIL - AM-01 TRAIL KIOSK



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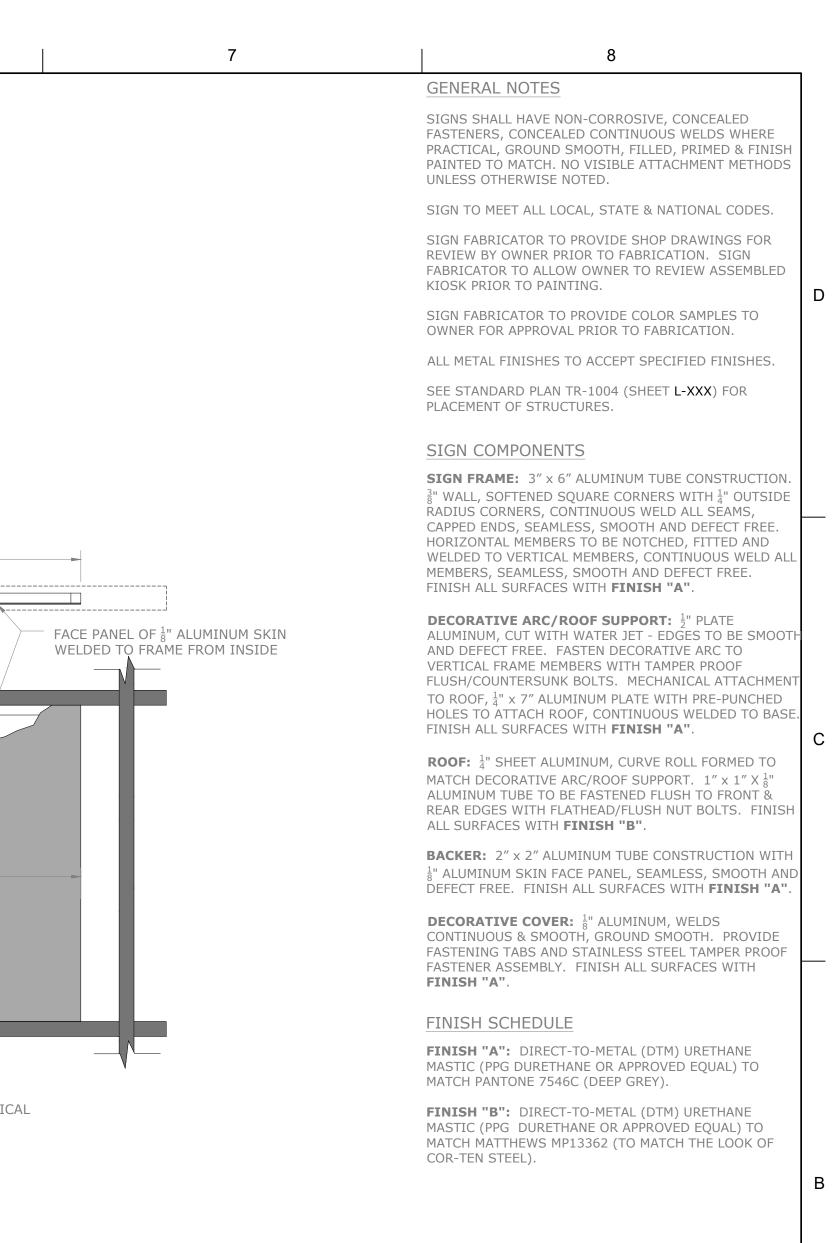
1" x 1" x $\frac{1}{8}$ " ALUMINUM TUBE CONTINUOUSLY WELDED FLUSH TO UNDER, BOTTOM EDGE OF ROOF. CAP ENDS SUCH THAT OUTER EDGE OF CAP IS FLUSH WITH EDGE OF ROOF

1

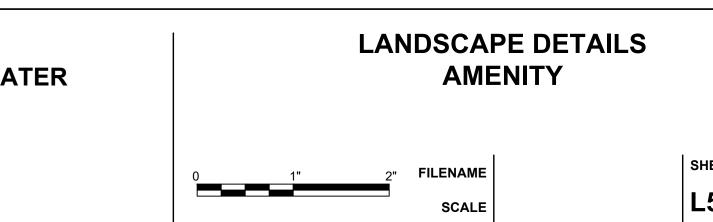
325 BLAKE RD REGIONAL STORMWATER **AND GREENWAY**

4'-0"

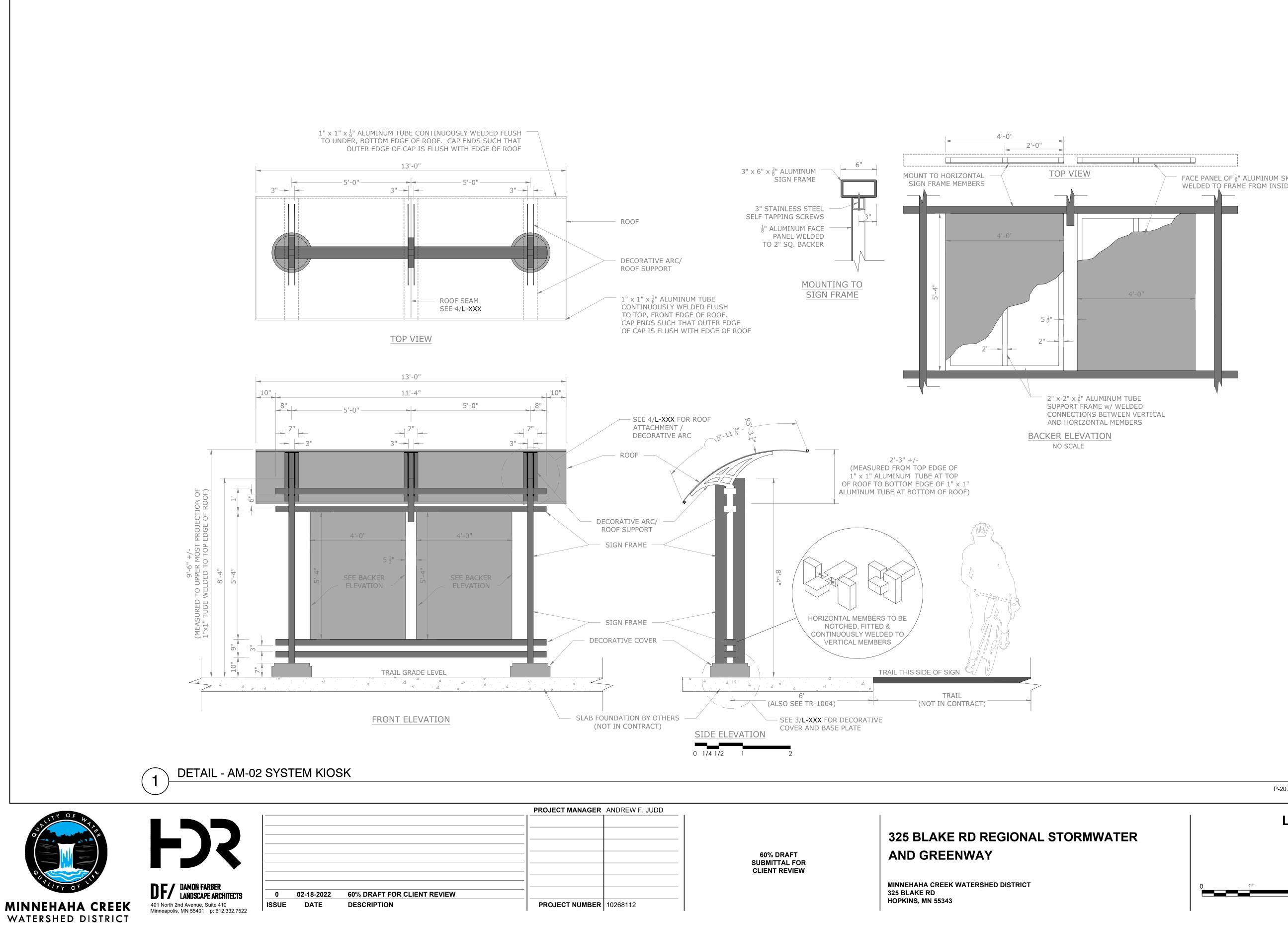
MINNEHAHA CREEK WATERSHED DISTRICT 325 BLAKE RD HOPKINS, MN 55343



P-20.199-119







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PROJECT MANAGER	ANDREW F. JUDD
	10268112

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GENERAL NOTES

SIGNS SHALL HAVE NON-CORROSIVE, CONCEALED FASTENERS, CONCEALED CONTINUOUS WELDS WHERE PRACTICAL, GROUND SMOOTH, FILLED, PRIMED & FINISH PAINTED TO MATCH. NO VISIBLE ATTACHMENT METHODS UNLESS OTHERWISE NOTED.

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SIGN TO MEET ALL LOCAL, STATE & NATIONAL CODES.

SIGN FABRICATOR TO PROVIDE SHOP DRAWINGS FOR REVIEW BY OWNER PRIOR TO FABRICATION. SIGN FABRICATOR TO ALLOW OWNER TO REVIEW ASSEMBLED KIOSK PRIOR TO PAINTING.

SIGN FABRICATOR TO PROVIDE COLOR SAMPLES TO OWNER FOR APPROVAL PRIOR TO FABRICATION.

ALL METAL FINISHES TO ACCEPT SPECIFIED FINISHES.

SEE STANDARD PLAN TR-1004 (SHEET L-XXX) FOR PLACEMENT OF STRUCTURES.

SIGN COMPONENTS

SIGN FRAME: 3" x 6" ALUMINUM TUBE CONSTRUCTION. $\frac{3}{8}$ " WALL, SOFTENED SQUARE CORNERS WITH $\frac{1}{4}$ " OUTSIDE RADIUS CORNERS, CONTINUOUS WELD ALL SEAMS, CAPPED ENDS, SEAMLESS, SMOOTH AND DEFECT FREE. HORIZONTAL MEMBERS TO BE NOTCHED, FITTED AND WELDED TO VERTICAL MEMBERS, CONTINUOUS WELD AL MEMBERS, SEAMLESS, SMOOTH AND DEFECT FREE. FINISH ALL SURFACES WITH FINISH "A".

DECORATIVE ARC/ROOF SUPPORT: ¹/₂" PLATE ALUMINUM, CUT WITH WATER JET - EDGES TO BE SMOOT AND DEFECT FREE. FASTEN DECORATIVE ARC TO VERTICAL FRAME MEMBERS WITH TAMPER PROOF FLUSH/COUNTERSUNK BOLTS. MECHANICAL ATTACHMEN TO ROOF, $\frac{1}{4}$ " x 7" ALUMINUM PLATE WITH PRE-PUNCHED HOLES TO ATTACH ROOF, CONTINUOUS WELDED TO BASE FINISH ALL SURFACES WITH **FINISH "A"**.

ROOF: $\frac{1}{4}$ " SHEET ALUMINUM, CURVE ROLL FORMED TO MATCH DECORATIVE ARC/ROOF SUPPORT. $1'' \times 1'' \times \frac{1}{8}''$ ALUMINUM TUBE TO BE FASTENED FLUSH TO FRONT & REAR EDGES WITH FLATHEAD/FLUSH NUT BOLTS. FINISH ALL SURFACES WITH **FINISH "B"**.

BACKER: 2" x 2" ALUMINUM TUBE CONSTRUCTION WITH ¹/₈" ALUMINUM SKIN FACE PANEL, SEAMLESS, SMOOTH AND DEFECT FREE. FINISH ALL SURFACES WITH FINISH "A".

DECORATIVE COVER: $\frac{1}{8}$ " ALUMINUM, WELDS CONTINUOUS & SMOOTH, GROUND SMOOTH. PROVIDE FASTENING TABS AND STAINLESS STEEL TAMPER PROOF FASTENER ASSEMBLY. FINISH ALL SURFACES WITH FINISH "A".

FINISH SCHEDULE

FINISH "A": DIRECT-TO-METAL (DTM) URETHANE MASTIC (PPG DURETHANE OR APPROVED EQUAL) TO MATCH PANTONE 7546C (DEEP GREY).

FINISH "B": DIRECT-TO-METAL (DTM) URETHANE MASTIC (PPG DURETHANE OR APPROVED EQUAL) TO MATCH MATTHEWS MP13362 (TO MATCH THE LOOK OF COR-TEN STEEL).

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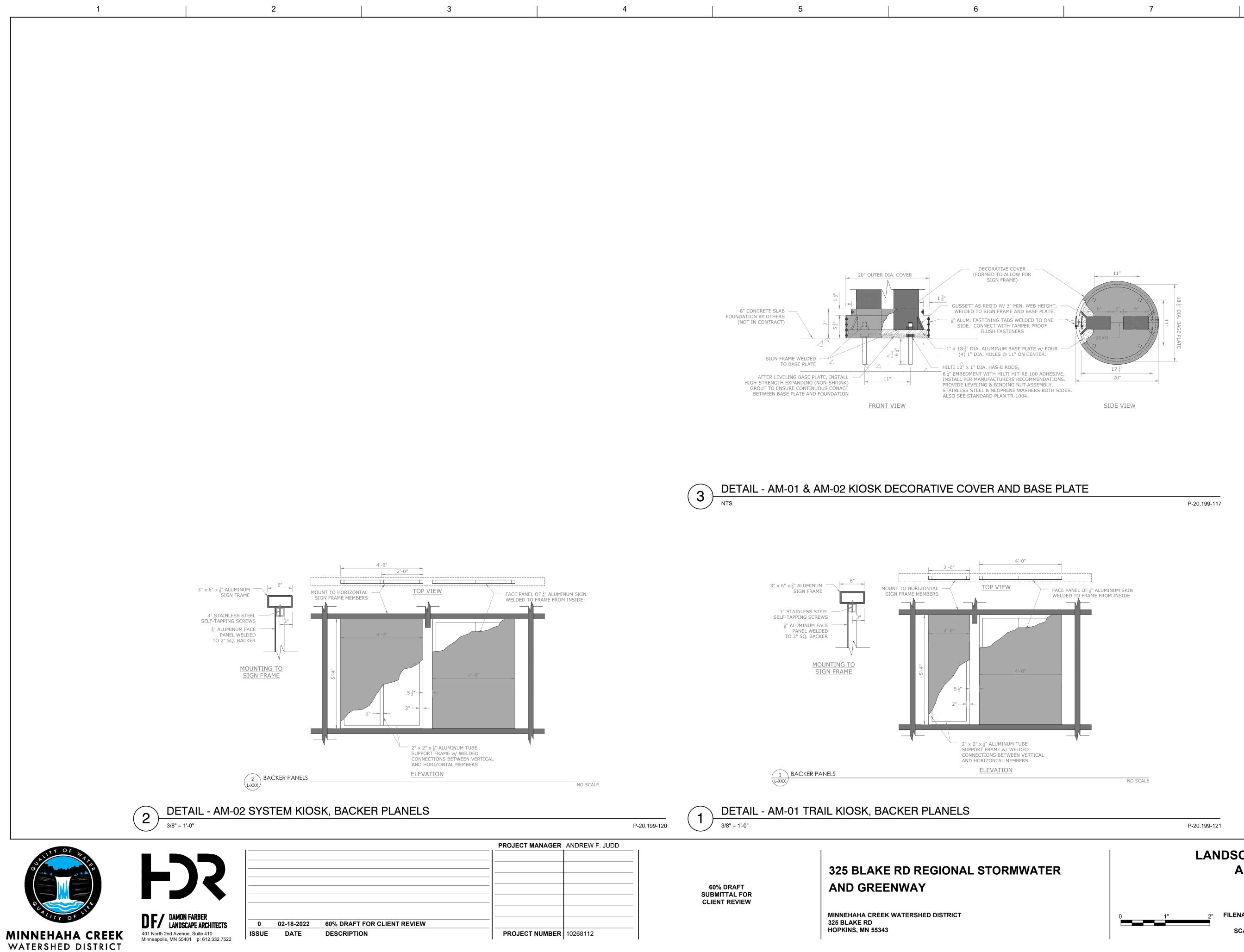


LANDSCAPE DETAILS AMENITY

> FILENAME SCALE

SHEET L581

FACE PANEL OF $\frac{1}{8}$ " ALUMINUM SKIN WELDED TO FRAME FROM INSIDE



LANDSCAPE DETAILS AMENITY

FILENAME SCALE

SHEET L582

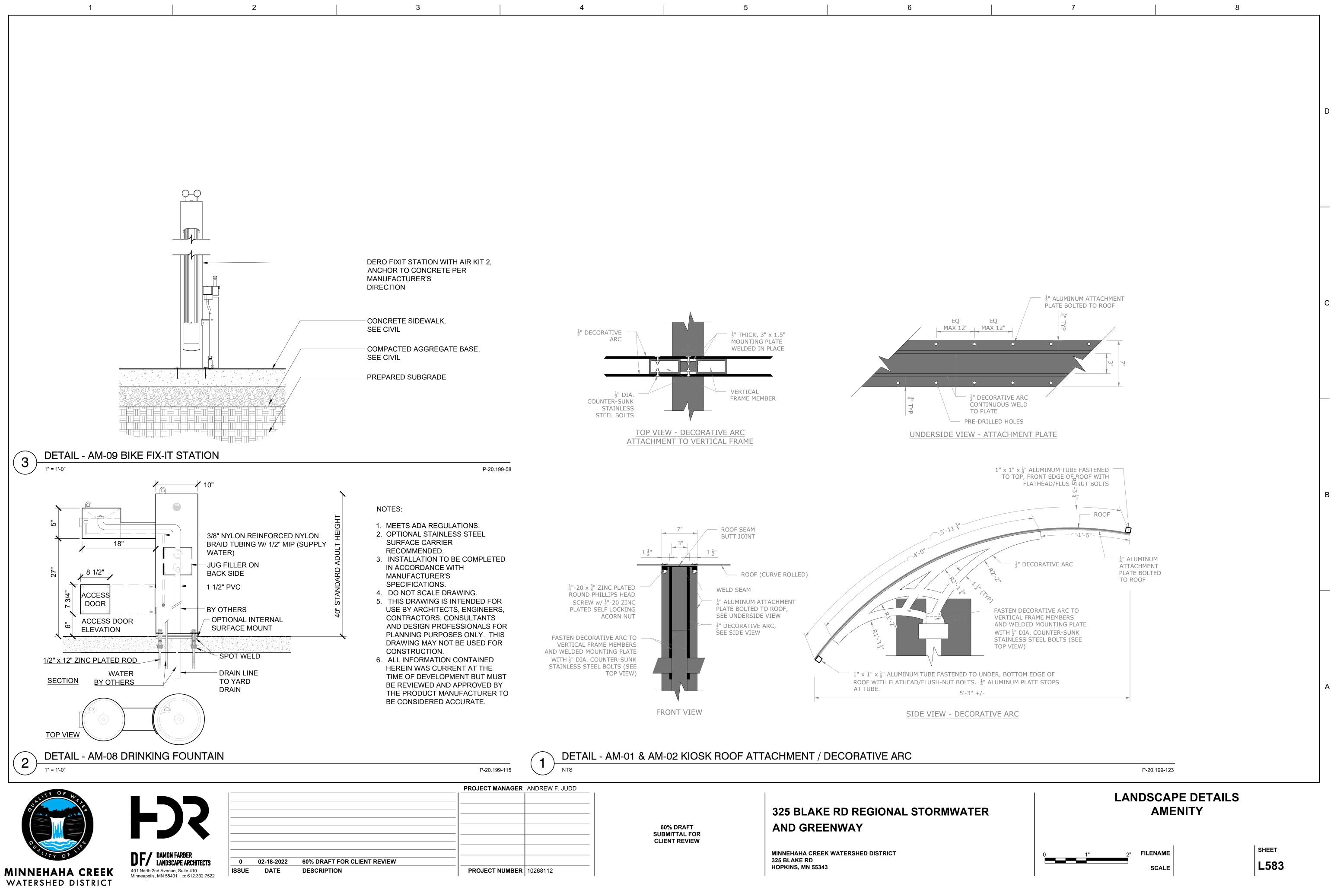
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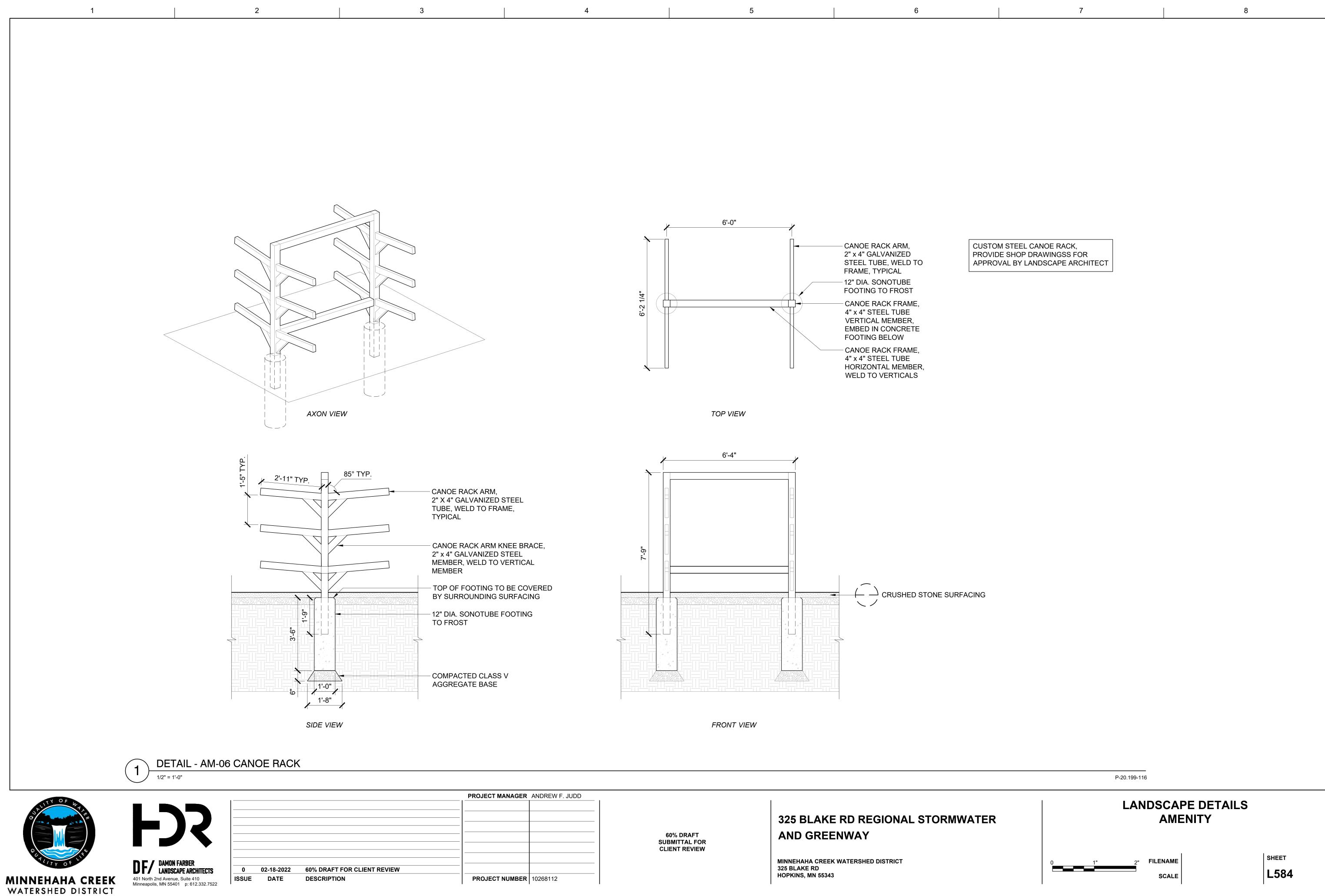
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PROJECT MANAGER	60% DRAFT SUBMITTAL FOR CLIENT REVIEW	AND G		STORMWATE
ONALS FOR ONLY. THIS USED FOR ITAINED AT THE I BUT MUST ROVED BY ACTURER TO RATE. P-20.199-115	ARC TO EMBERS G PLATE R-SUNK	DECORATIVE ARC, EE SIDE VIEW	ROOF WITH FLATHEA AT TUBE.	JM TUBE FASTENED TO UI AD/FLUSH-NUT BOLTS. ¹ / ₄ 5'-3" +/-



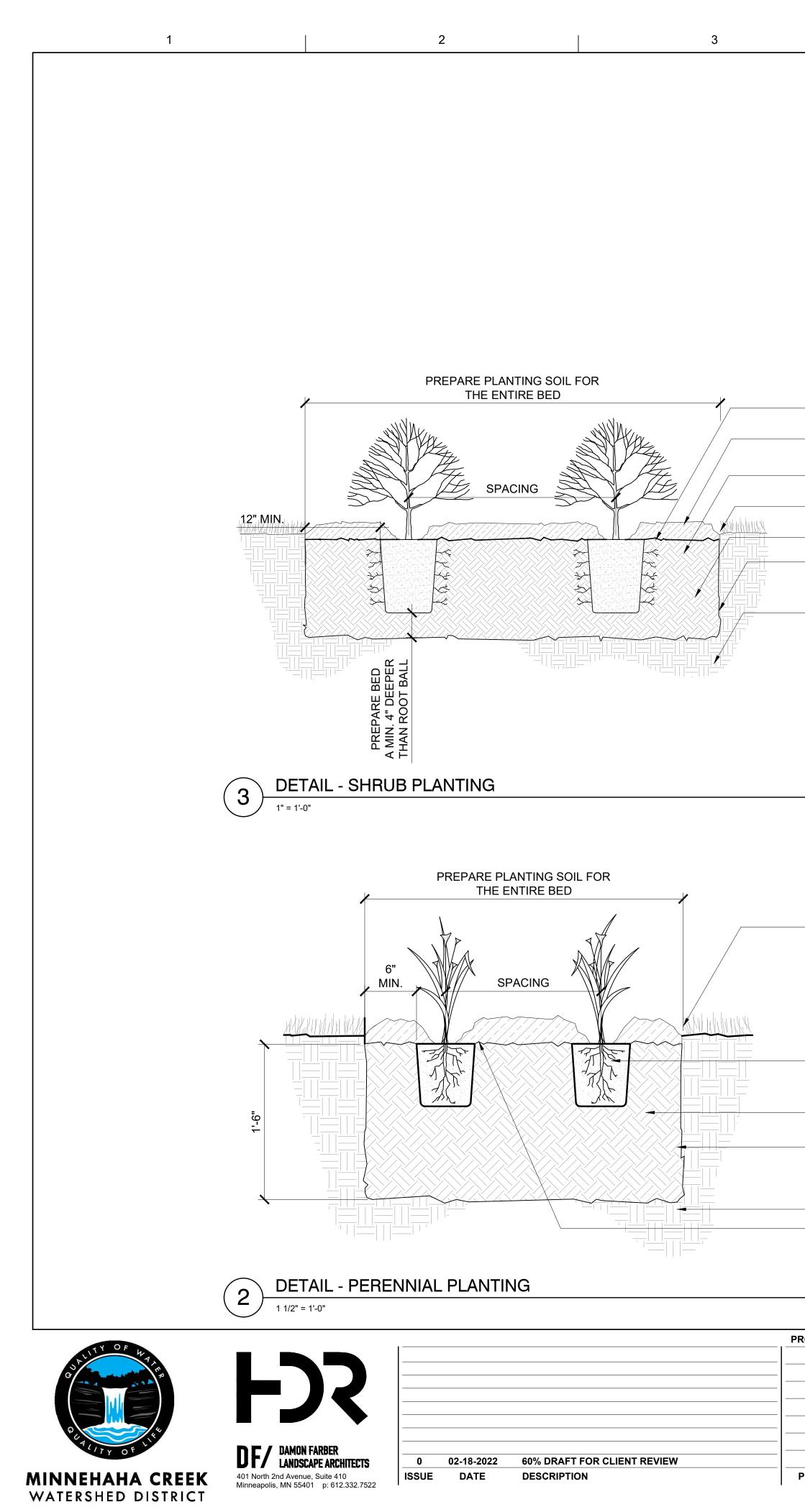
PROJECT MANAGER	ANDREW F. JUDD
PROJECT NUMBER	10268112
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- UNDISTURBED SUBGRADE		HARDWIRE CLOT	TALL RODENT PROTECTION. ¹ /2" TH MESH CYLINDER, 8" DIA. OR HGT; STAKE IN PLACE. PER SPEC	
P-20.199-08		6' DIAMETER MULCH RING	PLANTING PIT TO BE TWO O FIVE TIMES THE DIAMETER OF THE ROOT BALL, SLOPED	
		36" RADIUS		В
- EDGE CONDITION VARIES; REFER TO PLAN			 EDGE CONDITION VARIES; REFER TO PLAN PREPARED PLANTING SOIL PER SPEC SCARIFY SIDES OF TREE PIT WITH SPADE BY HAND TO BIND WITH PREPARED PLANTING SOIL UNDISTURBED SUBGRADE 	
- CONTAINER GROWN MATERIAL SHALL HAVE ROOTSH AND LOOSENED		א דין א BUILT-UP EAF ROOT BALL	RTH SAUCER BEYOND EDGE OF	
- PLANTING SOIL FOR PERENNIALS			DUND ROOT BALL BASE FIRMLY ESSURE SO THAT ROOT BALL T	
- SCARIFY SIDES AND BOTTOM OF ENTIRE BED WITH SPADE BY HAND TO BIND WITH PLANTING SOIL	DIG P		AP, TWINE, ROPE AND WIRE FROM COOT BALL ALL ON UNDISTURBED OR	A
- UNDISTURBED SUBGRADE		COMPACTED SC	OIL	
– 3" MULCH; DO NOT PLACE IN CONTACT WITH PLANT STEM		4" ORGANIC MU CONTACT WITH	JLCH; DO NOT PLACE MULCH IN I TREE TRUNK	
P-20.199-06	1 DETAIL - TREE PLANTING 3/4" = 1'-0"		P-20.199-05	
OJECT MANAGER ANDREW F. JUDD	60% DRAFT SUBMITTAL FOR	LAKE RD REGIONAL STORMWATER GREENWAY	LANDSCAPE DETA PLANTING	NILS
	CLIENT REVIEW MINNEHAH 325 BLAKE	A CREEK WATERSHED DISTRICT	0 <u>1" 2</u> " FILENAME	sнеет L590

APPLICATION OF PRE-EMERGENT HERBICIDE - 3" MULCH; DO NOT PLACE IN

CONTACT WITH SHRUB STEM CONTAINER GROWN MATERIAL

SHALL HAVE ROOTS HAND LOOSENED - EDGE CONDITION VARIES;

REFER TO PLAN

PLANTING SOIL FOR SHRUBS

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THROUGHOUT THE WARRANTY PERIOD. WRAP

MAINTAINING TREES IN A PLUMB POSITION TREE TRUNKS ONLY UPON APPROVAL BY LANDSCAPE ARCHITECT. SEE SPECIFICATION SECTION RELATED TO PLANTS AND SOIL PREPARATION.

NOTE:

EACH TREE SHALL BE PLANTED SUCH THAT THE ROOT FLARE IS VISIBLE AT THE TOP OF THE ROOT BALL. IF THE ROOT FLARE IS NOT VISIBLE,

THE SOIL SHALL BE REMOVED IN A LEVEL

MANNER FROM THE ROOT BALL TO WHERE THE

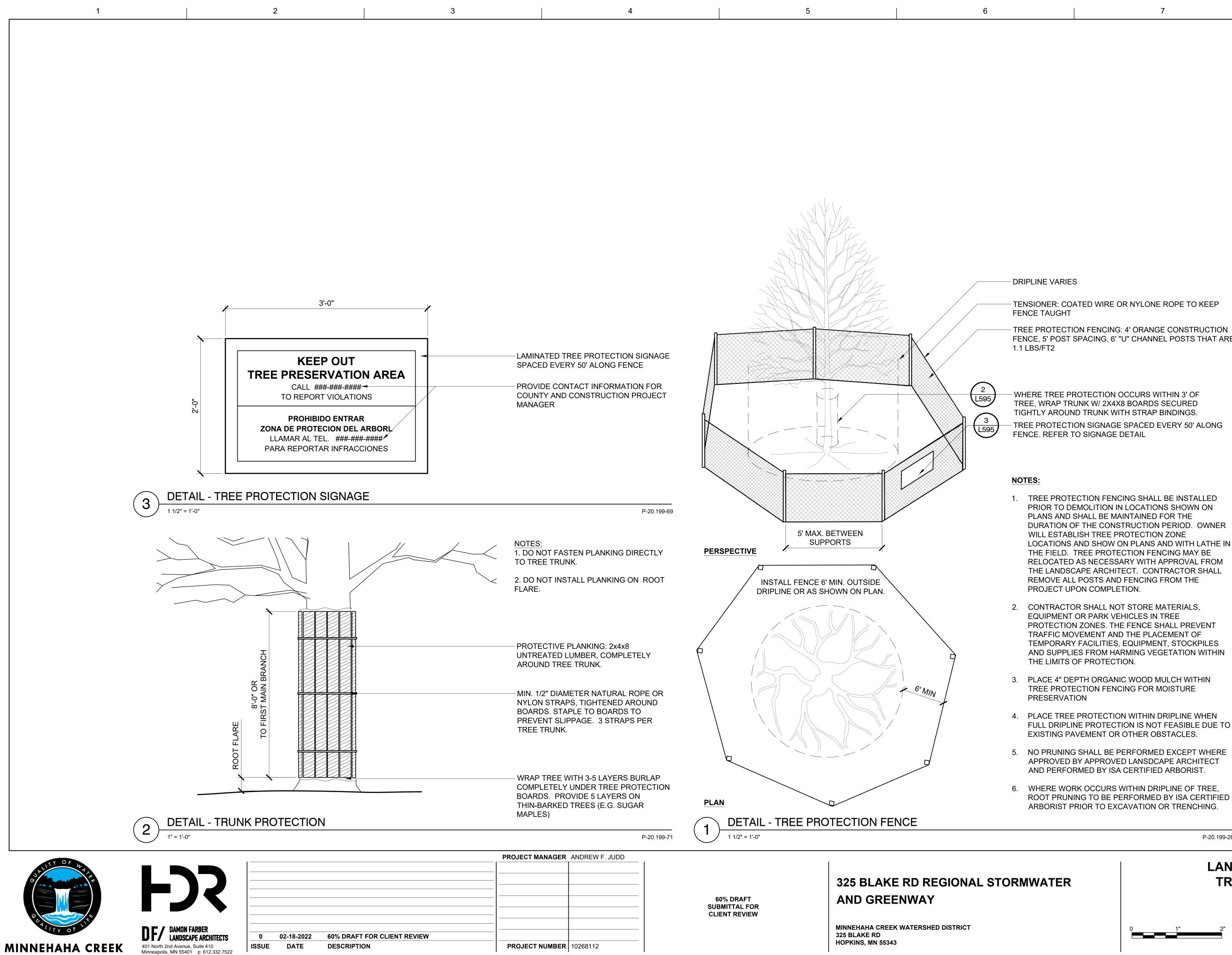
CONTRACTOR SHALL BE RESPONSIBLE FOR

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WATERSHED DISTRICT

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LANDSCAPE DETAILS
TREE PROTECTION

FILENAME

SCALE

P-20.199-28

APPROVED BY APPROVED LANSDCAPE ARCHITECT AND PERFORMED BY ISA CERTIFIED ARBORIST.

EXISTING PAVEMENT OR OTHER OBSTACLES. 5. NO PRUNING SHALL BE PERFORMED EXCEPT WHERE

4. PLACE TREE PROTECTION WITHIN DRIPLINE WHEN FULL DRIPLINE PROTECTION IS NOT FEASIBLE DUE TO

3. PLACE 4" DEPTH ORGANIC WOOD MULCH WITHIN TREE PROTECTION FENCING FOR MOISTURE

TRAFFIC MOVEMENT AND THE PLACEMENT OF TEMPORARY FACILITIES, EQUIPMENT, STOCKPILES AND SUPPLIES FROM HARMING VEGETATION WITHIN THE LIMITS OF PROTECTION.

2. CONTRACTOR SHALL NOT STORE MATERIALS, EQUIPMENT OR PARK VEHICLES IN TREE PROTECTION ZONES. THE FENCE SHALL PREVENT

LOCATIONS AND SHOW ON PLANS AND WITH LATHE IN RELOCATED AS NECESSARY WITH APPROVAL FROM THE LANDSCAPE ARCHITECT. CONTRACTOR SHALL REMOVE ALL POSTS AND FENCING FROM THE PROJECT UPON COMPLETION.

PRIOR TO DEMOLITION IN LOCATIONS SHOWN ON PLANS AND SHALL BE MAINTAINED FOR THE DURATION OF THE CONSTRUCTION PERIOD. OWNER WILL ESTABLISH TREE PROTECTION ZONE THE FIELD. TREE PROTECTION FENCING MAY BE

FENCE. REFER TO SIGNAGE DETAIL 1. TREE PROTECTION FENCING SHALL BE INSTALLED

- WHERE TREE PROTECTION OCCURS WITHIN 3' OF TREE, WRAP TRUNK W/ 2X4X8 BOARDS SECURED

FENCE, 5' POST SPACING, 6' "U" CHANNEL POSTS THAT ARE

TREE PROTECTION FENCING: 4' ORANGE CONSTRUCTION

TENSIONER: COATED WIRE OR NYLONE ROPE TO KEEP

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Draft Operation, Maintenance, and Monitoring Plan

325 Blake Road Restoration and Redevelopment

Regional Stormwater Improvements and Greenway Enhancement

Minnehaha Creek Watershed District February 2022



Table of Contents

1.	Introduction	1
2.	Project Components	2
3.	Site Safety	3
4.	Operation and Maintenance	4
5.	Inspection & Monitoring Program	6

Figures

Figure 1.1: Site Parcels

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Tables

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Table 4.1: Routine Maintenance Activities
Table 5.1: Routine Inspection Activities
Table 5.2: Vegetation Inspection Activities
Table 5.3: Drainage Structure Inspection Activities
Table 5.4: Maintenance and Monitoring Structure Inspection Activities
Table 5.5: Weir Inspection Activities
Table 5.6: Pump Inspection Activities

Appendices

Appendix A: Placeholder – Inspection Report Appendix B: Placeholder – Oldcastle Infrastructure NSBB Operation and Maintenance Manual

1. Introduction

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The 325 Blake Road Regional Stormwater and Greenway Project (the project) consists of the restoration and water-centric redevelopment of a site located adjacent to Minnehaha Creek, premised on a vision of Balanced Urban Ecology. The site is comprised of 4 parcels and one outlot that total 17.81 acres (see *Figure 1.1: Site Parcels*), with the primary parcel (A) being subdivided between the Developer (Alatus) and Minnehaha Creek Watershed District (*the District*). The project is situated in the lower Minnehaha Creek watershed, approximately 7.3 river miles downstream of Grays Bay dam on Lake Minnetonka where the headwaters of Minnehaha Creek are formed, and approximately 11.5 river miles upstream of Lake Hiawatha. Minnehaha Creek's confluence with the Mississippi River is located roughly 13.9 river miles downstream of the project site.

The project includes stormwater management BMPs and recreational facilities situated along Minnehaha Creek and the Cedar Lake LRT Regional Trail, within the Minnehaha Creek Greenway. Stormwater runoff from the Powell Road subwatershed (226 acres) and Lake Street subwatershed (30.3 acres) drains into the project through diversions of the mainline storm sewers. The diversions will fully divert small storms and the first flush of larger storms into the regional stormwater pond. When the diversions reach capacity, the remaining overflow discharges to existing offsite storm sewer outfalls.

This Operations, Maintenance, and Monitoring (OMM) plan outlines specific tasks recommended to maintain the District's regional stormwater treatment system and associated project features .

Cooperative Agreement and Associated Responsibilities

Project development was performed in partnership with Alatus, the developer of the non-District portions of the site. The District and Alatus have entered into a cooperative agreement for long-term operation and maintenance of various project features, including contractually defined responsibilities for various project infrastructure. The primary project parcel at 325 Blake Road North has defined ownership and development boundaries, with MCWD overseeing the public realm (Trailhead and Overlook, Stormwater Ponds, The Landing, Nature-Based Play Area, and the Gateway to Greenway) and Alatus overseeing the mixed-use development located adjacent to the public realm components of the site. Project components and parties responsible for operation, maintenance, and monitoring of said components, are summarized in Section 2. Note that the maintenance responsibilities outlined below may not strictly follow the extents of the site development and subdivision. These cases will be specifically noted in Section 2.

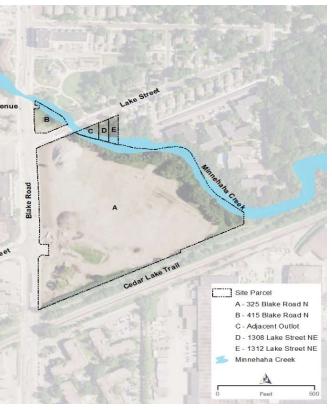


Figure 1.1: Site Parcels.

2. Project Components

The project features several stormwater components that require routine operation, maintenance, and monitoring to achieve the goals set forth by the District. Other site amenities and infrastructure will require ongoing operation and maintenance; however this plan focuses solely on the maintenance of stormwater management components. Refer to Project Drawings for construction information and the Project Design Memo for narrative descriptions of project components. Table 2.1 displays a matrix of the stormwater project components of the overall site relative to required maintenance activities and their frequency.

Table 2.1: Project Components

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			Maintenance Activities*																
Project	Responsible Party –	Weekly	Mor	nthly	- Monthly Sea	Growing son		Annually -	Late Fall					As Needed B	ased on Inspe	ction			
Component	update per agreement	Litter Removal	Drainage Structure Clearing	Flow Path Clearing	Mowing	Weed Control	Maintenance & Monitoring Structure Clearing	Vegetation Harvesting	Pruning	Winterization	Pump Maintenance	Nutrient Separating Baffle Box Maintenance	Drainage Structure Maintenance	Pipe Maintenance	Dredging*	Graffitti Removal	Minor Concrete/ Masonry Repair	Planting	Erosion Repair
Powell Road and Lake Street Diversion Storm Sewers	MCWD	\checkmark	\checkmark	\checkmark			\checkmark	-	-	\checkmark			\checkmark	\checkmark	-	\checkmark	\checkmark		
Nutrient Separating Baffle Boxes (NSBBs)	MCWD	\checkmark	\checkmark							\checkmark		\checkmark				\checkmark	\checkmark		
North Pond	MCWD	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark		\checkmark	\checkmark				\checkmark		\checkmark	\checkmark	\checkmark	\checkmark	\checkmark
South Pond	MCWD	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark		\checkmark	\checkmark				\checkmark		\checkmark	\checkmark	\checkmark	\checkmark	\checkmark
Weir Wall	MCWD	\checkmark														\checkmark	\checkmark		
Outlet Structure	MCWD	\checkmark	\checkmark				\checkmark						\checkmark			\checkmark	\checkmark		\checkmark
Private Development BMPs	Alatus	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark		\checkmark	\checkmark			\checkmark	\checkmark		\checkmark	\checkmark	\checkmark	\checkmark
Private Development Storm Sewer	Alatus	\checkmark	\checkmark	\checkmark			\checkmark			\checkmark			\checkmark	\checkmark		\checkmark	\checkmark		
Cascade and Associated BMPs	Alatus	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark		\checkmark	\checkmark			\checkmark	\checkmark		\checkmark	\checkmark	\checkmark	\checkmark
Boathouse, Pumps, and Associated Piping	Alatus	\checkmark					\checkmark			\checkmark	\checkmark			\checkmark		\checkmark	\checkmark		

*See Table 4.1 for detailed description and recommended frequency of routine maintenance activities.

3. Site Safety and Contacts

Safety precautions should be observed while performing any maintenance, inspection, or monitoring activities associated with the site's stormwater management systems. When potentially hazardous conditions arise, O&M personnel should remove themselves from the situation and secure the site to the maximum extent possible. Any safety concerns that may continue to be present beyond the maintenance, inspection, or monitoring event or potentially impact the safety of the public or other site personnel.

Potential hazards for O&M personnel include but are not limited to:

- Extremely hot or cold weather.
- Heavy equipment and machinery.
- Sloped surfaces
- Confined space
- Insects and wildlife
- Deep water

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Onsite safety meetings to discuss potential safety concerns, shall be performed prior to conducting any O&M activities. All maintenance activities must be performed according to Federal, State, and Local regulations. Entry into confined spaces should only be performed by certified professionals.

To the maximum extent possible vehicle use should be limited to designated path areas. Partial closure of paths, or drive aisles may be required for certain maintenance tasks, specifically those requiring specialized equipment such as vacuum trucks. Use of the pond's maintenance bench should be limited to light-weight vehicles with tight turning radii, such as mowers.

The operation, maintenance, and monitoring of the Blake Road project will include coordination between multiple parties. The following list provides a primary list of points of contact for the project.

Contacts – to be filled in as responsibilities are defined

- Minnehaha Watershed District Site Contact -
- Alatus Site Contact -
- ...

4. Operation and Maintenance

Table 4.1 provides a reference for anticipated maintenance activities and the recommended frequency at which this maintenance should be performed. This table intends to cover the majority of anticipated maintenance tasks, however additional maintenance needs beyond those outlined in the table, such as full replacement of site features, may be necessary. Should this situation occur, maintenance responsibility will be incurred by the party responsible for the site component as defined in Table 2.1.

All maintenance activities should be performed in a manner that reasonably limits impacts to the surrounding natural environment and other site features. Each party is responsible for the in-kind replacement of facilities impacted by maintenance and other activities that they perform.

Each maintenance activity includes an anticipated expense/effort per maintenance event. The following numbers are only estimates, and may vary based on several factors, such as extent of maintenance required and the ability to combine multiple maintenance tasks into a single maintenance event:

- Low Maintenance personnel require minimal specialized training and equipment, expense expected to be less than \$2,000 per event
- Moderate Maintenance personnel require some specialized training and equipment, expense expected to be between \$2,000 and \$10,000 per event
- High Maintenance personnel require significantly specialized training and equipment, expense expected to be between more than \$10,000 per event.

Table 4.1 Routine Maintenance

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Maintenance Activity	Description	Frequency	Expense/Effort
Litter Removal	Removal of trash, debris, and litter from site areas and accessible structures, and accessible pond areas.	Weekly	Low
Drainage Structure Clearing	Clear structures and grates to facilitate proper function of drainage structures.	Monthly	Low
Flow Path Clearing	Remove obstructions and debris to promote proper overland flow.	Monthly	Low
Mowing	Mow lawns, 3-foot wide strip along pedestrian areas, and pond maintenance bench. String trimming permitted in difficult to reach areas.	Monthly during growing season	Low
Weed Control	Remove and/or control of noxious or invasive weeds.	Monthly during growing season	Low
Maintenance & Monitoring Structure Clearing	Locate and clear access promote ease of inspection and monitoring. Remove excessive vegetation and debris.	Annually in late Fall	Low
Vegetation Harvesting	Trim back wetland vegetation to a height of 8 inches.	Annually in late Fall	Low
Pruning	Prune woody vegetation within 5 feet of pedestrian areas for proper structure, removal of dead limbs, and 14-foot vertical clearance.	Annually in late Fall	Moderate
Winterization	Turn off pumps, drain hoses. Spray rusted or likely to freeze appurtenances with lubricant.	Annually in late Fall	Low
Pump Maintenance	Perform routine service to promote proper function.	As needed based on inspection	Moderate
Nutrient Separating Baffle Box Maintenance	Jet/Vac Baffle Box per maintenance requirements to remove sediment and debris.	As needed based on inspection	High
Drainage Structure Maintenance	Jet/Vac sumped Drainage Structures to remove sediment and debris. Dewatering may be necessary.	As needed based on inspection	High
Pipe Maintenance	Jet pipes.	As needed based on inspection	Moderate
Dredging*	Remove submerged sediment and debris from pond bottom to restore original design elevations.	As needed based on inspection	High

Maintenance Activity	Description	Frequency	Expense/Effort
Graffiti Removal	Remove graffiti, repaint surfaces.	As needed based on inspection	Low
Minor Concrete/ Masonry Repair	Repair spalling, cracking, or displaced/loose concrete or masonry site components.	As needed based on inspection	Moderate
Planting	Replant bare areas greater than 1,000 square feet with native plantings based on the original planting plan.	As needed based on inspection	Moderate
Erosion Repair	Remove debris and restore surface flow paths, access paths, and sideslopes to design elevations. Restore undermined structures.	As needed based on inspection	Low

*See Dredging Sub-section below

In addition to routine maintenance tasks, corrective maintenance may be needed as site conditions require. Corrective maintenance requests may result from a formal site inspection, or a simple observation from a site owner, staff, or member of the community. When corrective maintenance is required, it is critical that maintenance personnel be provided with a list of maintenance tasks to be completed from the site owner or inspector prior to performing maintenance. Additional details of inspection requirements are included below.

Dredging

Based on existing knowledge of site groundwater and geotechnical conditions, draining and dewatering of the ponds may be complex and cost-intensive. As such, it is recommended that when the pond(s) require dredging, a "wet dredging" approach is considered.

Wet Dredging may be conducted through a combination of shoreline truck, barge, or the use of geotextile tubes. Because the basin bottom will be submerged during wet dredging, it is critical that rod-measurement of removed sediment be conducted prior to, during, and following the dredging event to understand accurate quantities of sediment removed. Dredged material should be tested for potential contamination prior to removal from the site. Contaminated materials may be subject to special requirements for re-use, disposal, or land application.

The need for dredging will be established through inspection and/or monitoring. Sediment depths should be estimated by a using a measuring rod at several points within the pond to providing an approximate measurement of sediment depth. A Minnesota company called BioBase provides sonar equipment and analysis for a sonar approach as an alternative to rod measurement, but sonar should not be used for measuring dredge quantities during construction.

When the average sediment depth is approaching 3 feet, the District should begin planning for a near-term dredge project. Additionally, if pond outlet monitoring indicates a consistent degradation in water quality, it may be due to sediment resuspending within the pond and the need for dredging should be evaluated.

Records should be kept of any dredging project that is planned, designed, and performed.

5. Inspection & Monitoring Program

Inspection

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Inspection of all site components shall be performed regularly to reduce the risk of hazards and future maintenance costs. Inspections shall follow the same responsible party breakdown as maintenance activities, as indicated in Table 2.1. An inspection report (Appendix B) should be completed during each inspection. This inspection report should be used my maintenance crews to describe corrective maintenance requirements. Documentation, including inspection reports and records of resulting corrective maintenance, will be shared between the District and Alatus, and kept on file for the life of the project.

In addition to inspections occurring at regular time intervals, inspections will also be performed following major storm events. A major storm event is defined as a rainfall event in excess of 1.5 inches in 24 hours, or an event in which intense rainfall, winds, freezing rain, or other natural phenomena could reasonably affect site function.

Inspection activities, recommended frequencies, and suggested corrective maintenance activities to remediate deficiencies are provided in the following tables. Inspections are divided into categories based on similarities in scope and frequency. If inspectors are qualified to perform multiple inspections, they could be conducted simultaneously.

Inspection Activities

Routine inspections shall occur, at minimum, annually, after major storm events, and at the discretion of the owner based on community input or site needs.

Table 5.1 Routine Inspection Activities

Inspection Item	Corrective Maintenance Trigger	Typical Corrective Maintenance Action
Algae	Algae present in more than 25% of pond surface area.	Manage algae via physical removal, or the addir
Animal Burrows	Animal burrows or signs of burrowing present onsite.	Fill animal burrows with acceptable media.
Basin Bottom Depth	Basin bottom level exceeds 50% of the design depth measured from the design basin bottom to the permanent pool outlet elevation (Basin bottom elevation +889 for North Pond, basin bottom elevation +890 for South Pond).	Dredge bottom of affected basin areas.
Concrete	Minor concrete or masonry damage such as spalling, cracking, or displaced/loose concrete or masonry site components is present.	Repair damage with parging, patching, or repla
Erosion	Erosion that exceeds 20 square feet observed along basin slopes, access paths, maintenance bench, or near drainage or operations & maintenance structures.	Repair erosion using acceptable media, erosion
Organic Debris	Excessive organic debris is present within the pond, or near drainage structures, pumps, etc. that may impact site function.	Remove and dispose of organic debris.
Graffiti	Graffiti is present.	Remove graffiti and repaint surfaces as necessa
Woody Debris	Woody debris is accumulated in an area that inhibits site function or poses an aesthetic or safety issue.	Remove and dispose of woody debris.

ldition of additives and chemicals as needed.

lacement of missing components.

on control fabric, and/or additional planting.

sary.

Vegetation inspections shall occur, at minimum, annually during the growing season, and at the discretion of the owner based on community input or site needs.

Table 5.2 Vegetation Inspection Activities

Inspection Item	Corrective Maintenance Trigger	Typical Corrective Maintenance Action
Bare Areas	Vegetation is missing from an area of approximately 1,000 square feet.	Replant bare areas with native plantings based of
Invasive Weeds	Weeds categorized as noxious or invasive are present in planted areas.	Remove noxious or invasive weeds.
Organic Debris	Excessive organic debris present in vegetated areas that may impede the proper growth of desirable vegetation	Remove and dispose of or relocate organic debr

Drainage structure inspections shall occur, at minimum, every other year, after major storm events, and at the discretion of the owner based on community input or site needs. Additional inspections may be required for the outlet structure, especially following storm events that result in discharge through the outlet structure's overflow weir. Should the baffle box, manholes, or other sumped structures, require more frequent maintenance, additional inspections of those structures may be required.

Table 5.3 Drainage Structure Inspection Activities

Inspection Item	Corrective Maintenance Trigger	Typical Corrective Maintenance Action
Nutrient Separating Baffle Box	CCTV Camera or visual inspection reveals baffle box sump is greater than 50% filled with sediment or debris. Or structure inflows/outflows are blocked.	Vacuuming or mechanical removal of sediment
Concrete	Minor concrete or masonry damage such as spalling, cracking, or displaced/loose concrete or masonry site components is present.	Repair damage with parging, patching, or repla
Fasteners	Structure fasteners are rusted or stuck.	Lubricate or replace fasteners to provide access
Other Drainage Structures	CCTV Camera or visual inspection reveals structure sumps are greater than 50% filled with sediment or debris. Or structure inflows/outflows are blocked.	Vacuuming or mechanical removal of sediment
Pipes	CCTV Camera or visual inspection reveals that pipe cross sectional area is more than 30% obstructed by sediment or debris.	Jetting or clearing of pipes.
Railing	Railing atop overflow structure is loose or damaged.	Repair, replace, or tighten railing.

Maintenance and monitoring structure inspections shall occur, at minimum, every other year, and at the discretion of the owner/responsible party.

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Table 5.4 Maintenance and Monitoring Structure Inspection Activities

Inspection Item	Corrective Maintenance Trigger	Typical Corrective Maintenance Action
Conduit	Electrical conduit is exposed to the surface.	Bury conduit to provide protection from mowir
Maintenance Structures	Maintenance structure inaccessible or unable to be located.	Trim vegetation, remove debris, or remove soil
Monitoring Structures	Maintenance structure inaccessible or unable to be located.	Trim vegetation, remove debris, or remove soil
Fasteners	Structure fasteners are rusted or stuck.	Lubricate or replace fasteners to provide access

Weir inspections shall occur, at minimum, every five years, after major storm events, and at the discretion of the owner based on community input or site needs. Weir inspections may require the use of a diver in order to properly understand structural deficiencies of submerged features.

Table 5.5 Weir Inspection Activities

Inspection Item	Corrective Maintenance Trigger	Typical Corrective Maintenance Action
Graffiti	Graffiti is present.	Remove graffiti and repaint surfaces as necessa
Concrete	Minor concrete or masonry damage such as spalling, cracking, or displaced/loose concrete or masonry site components is present.	Repair damage with parging, patching, or replace
Scuppers	Scuppers are damaged or obstructed.	Repair/replace scuppers or clear flow paths, cle
Structural	Signs of structural damage to weir.	Conduct a professional structural analysis of the necessary to dewater the pond.

Pump inspections shall occur, at minimum, every other year, and at the discretion of the owner based on community input or site needs.

Table 5.6 Pump Inspection Activities

Inspection Item Corrective Maintenance Trigger

Typical Corrective Maintenance Action

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lacement of missing components.

clean scuppers if necessary.

the weir. Depending on extent of damage observed it may be

Corrosion	Rusting, cracking or discoloration of pump or associated pipework.	Turn off pump, clean or replace corroded compo
Improper Function	Noise, vibrations, or decreased flow rate observed.	Turn off pump, conduct a professional analysis o
Intake/Outlet	Intake or outlet area are full of debris, sediment, or trash.	Turn off pump, clear intake and outlet.

Monitoring

Permanent monitoring equipment has been installed at various on-site locations. This monitoring equipment shall be used to better understand the efficacy of the stormwater management installation both from a perspective of both quality and quantity. The following monitoring equipment is installed onsite:

- XXXEquipment Name ISCO Sampler measures water quality information such as total nitrogen, total phosphorous, and total suspended solids.
- XXXEquipment Name Flow Rate measures flow rate and velocity of stormwater entering and exiting the site.

All monitoring equipment is installed in a permanent lockable structure. These structures have been designed to be low profile as to not distract from the overall site aesthetic. Electricity is provided to sensors via buried conduit. Approximate locations of all maintenance and monitoring equipment can be found on the map in Appendix A and is summarized below:

- Inflow of each NSBB XXXEquipment Name
- Pond Outlet XXXEquipment Name
- Boat House XXXEquipment Name

Frequent access to these structures will be required for the collection of monitoring data. All structures are accessible from the surface and therefore do not require confined space entry.

Monitoring structures should be inspected whenever accessed (refer to the Inspection above). Should the results of the inspection require corrective maintenance, it should be communicated to the site owner.

The results of monitoring may also indicate the need for maintenance. If observed key site metrics in water quality or quantity are insufficient, corrective maintenance may be required. Specifically, monitoring results should be considered when determining the need for pond dredging. Monitoring results that would trigger the need for corrective maintenance include:

- A 20% decrease in water quality for a duration exceeding 5 days.
- A 50% decrease in water quality in a single event.
- An unexpected increase or decrease of 20% of outflow quantity for a period exceeding 24 hours.

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is of the pump.



Appendix A

Placeholder – Inspection Report





Appendix B

Oldcastle Infrastructure NSBB Operation and Maintenance Manual

OperationManual NSBB WM.pdf (oldcastleinfrastructure.com)



